

## LAMPIRAN



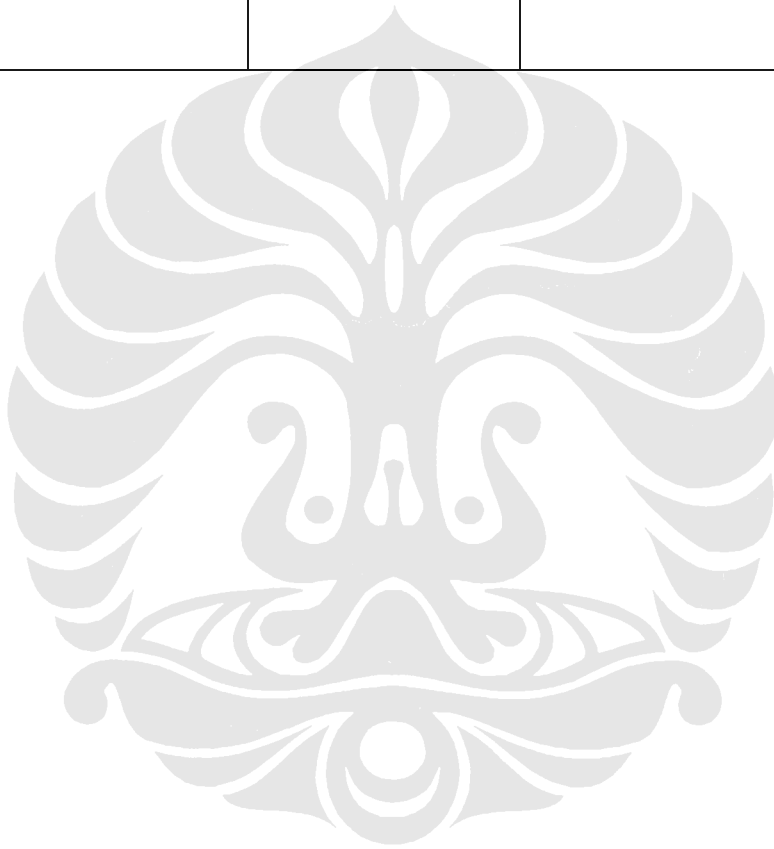
## LAMPIRAN 1

**Tabel sifat-sifat fluida**



Tabel sifat-sifat fluida pada 1 atm dan 20°C (68°F)

Fluida	$\rho$ (kg/m <sup>3</sup> )	$\mu$ (N.s/m <sup>2</sup> )	$\sigma$ (N/m)
Glycerine	1260	1.5	0.063
Castor oil	960	0.976	0.039
SAE 30	890	$1.05 \times 10^{-1}$	0.035



## LAMPIRAN 2

Foto-foto aliran fluida

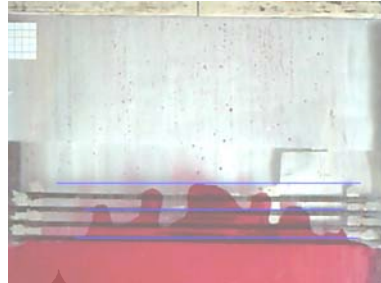


## Gambar perkembangan aliran Glycerin $dT/dx \leq 0$

I.  $b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$



$t = 10 \text{ detik}$



$t = 30 \text{ detik}$



$t = 60 \text{ detik}$

$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -4 \text{ }^\circ\text{C/cm}$



$t = 14 \text{ detik}$

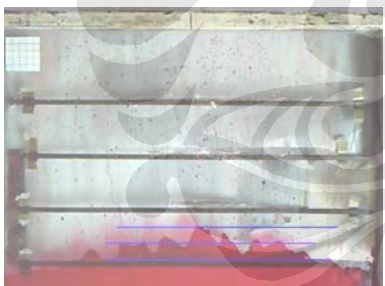


$t = 37 \text{ detik}$



$t = 70 \text{ detik}$

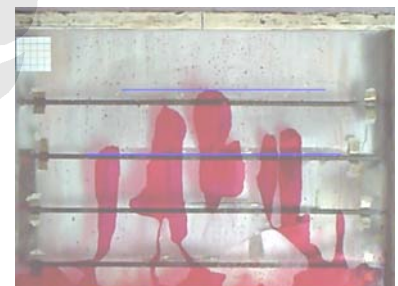
$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -2.5 \text{ }^\circ\text{C/cm}$



$t = 20 \text{ detik}$

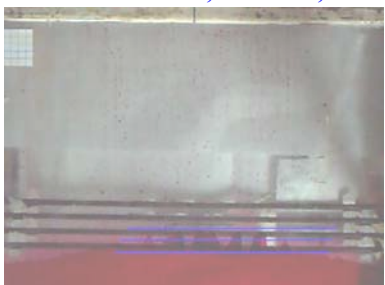


$t = 55 \text{ detik}$



$t = 105 \text{ detik}$

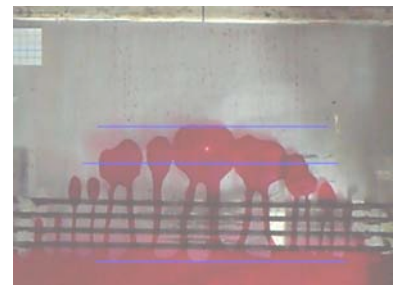
$b = 0.8 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$



$t = 7 \text{ detik}$



$t = 12 \text{ detik}$

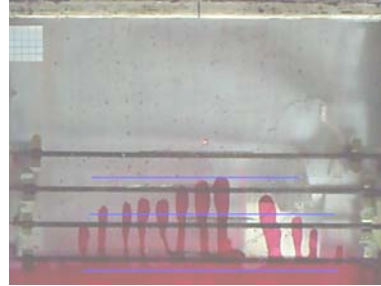


$t = 20 \text{ detik}$

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 10 detik



t = 15 detik

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 16 detik



t = 30 detik

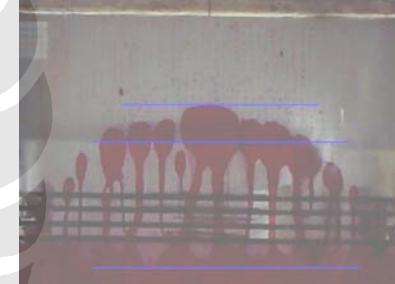
**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 10 detik



t = 15 detik

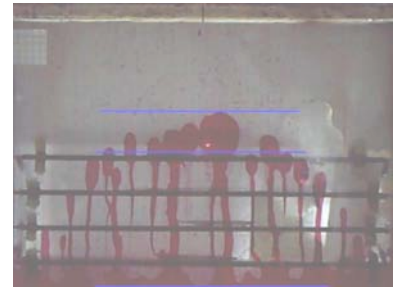
**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 8 detik



t = 12 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 6 detik

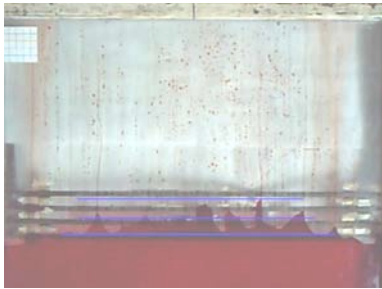


t = 10 detik



t = 17 detik

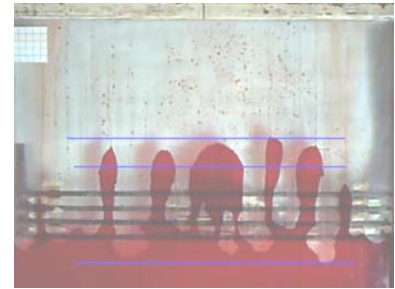
**II.  $b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 15 detik

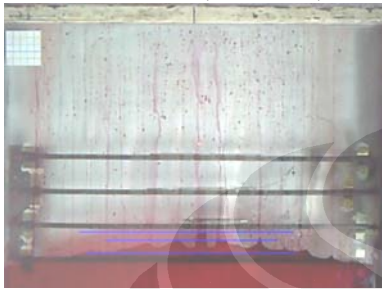


t = 25 detik

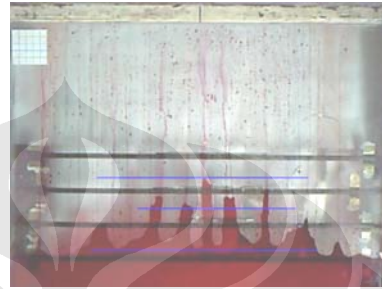


t = 45 detik

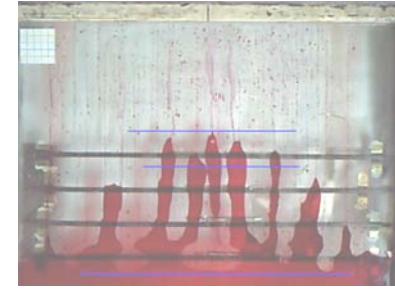
**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 12 detik

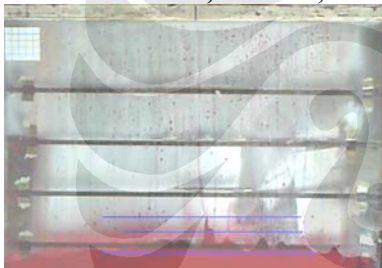


t = 28 detik



t = 50 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 15 detik

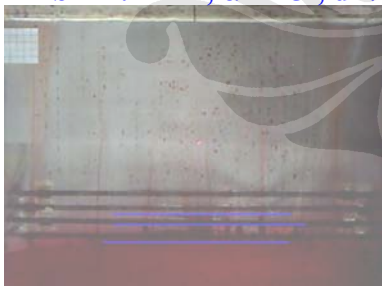


t = 33 detik



t = 70 detik

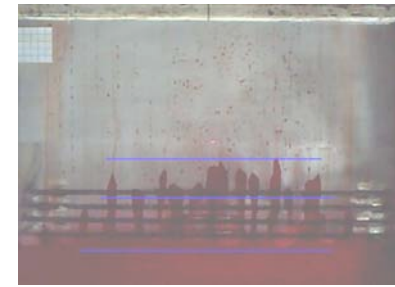
**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 8 detik



t = 10 detik

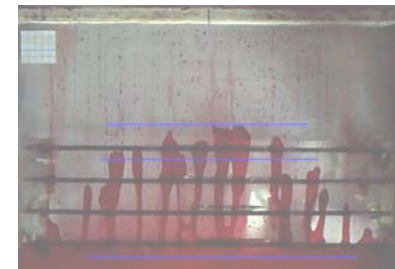
**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 6 detik

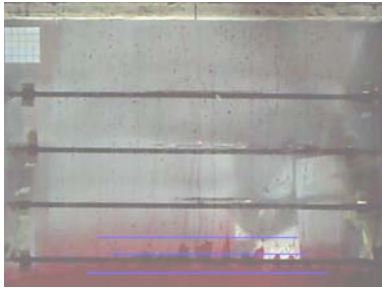


t = 11 detik



t = 15 detik

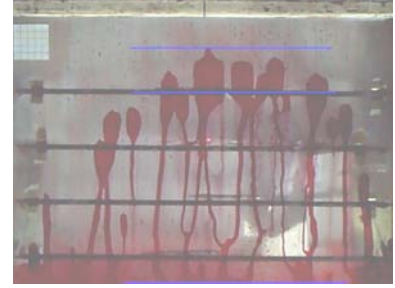
**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 8 detik



t = 17 detik



t = 26 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 8 detik

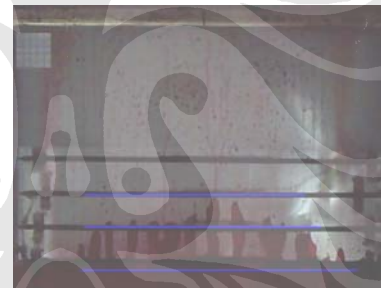


t = 12 detik

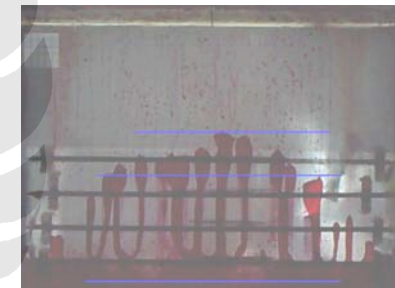
**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 6 detik

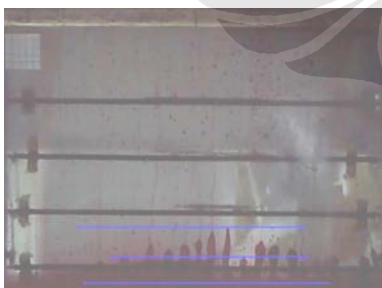


t = 8 detik



t = 12 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 9 detik



t = 14 detik



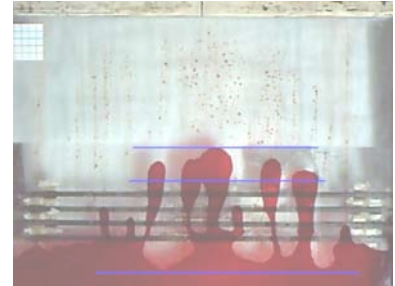
**III.  $b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 15 detik



t = 27 detik



t = 45 detik

**$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 16 detik



t = 32 detik



t = 75 detik

**$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 33 detik



t = 52 detik

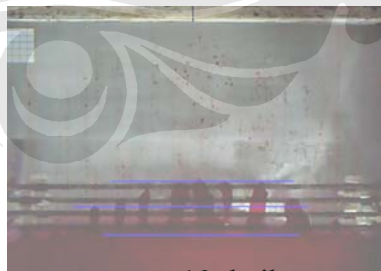


t = 67 detik

**$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 8 detik

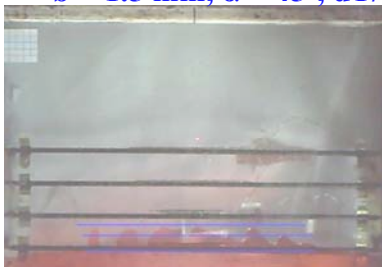


t = 10 detik



t = 15 detik

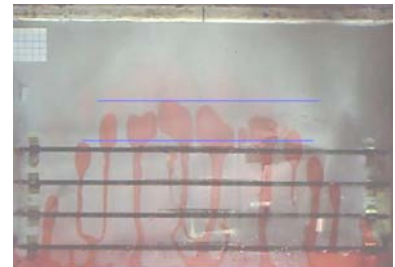
**$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 6 detik

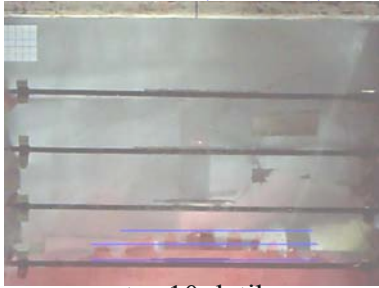


t = 8 detik



t = 13 detik

**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 10 detik

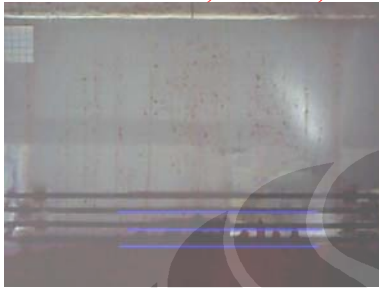


t = 16 detik



t = 22 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 7 detik



t = 10 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 4 detik



t = 6 detik



t = 9 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 5 detik



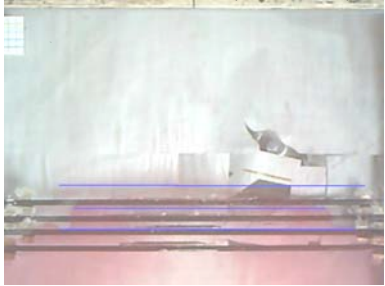
t = 10 detik



t = 17 detik

## Gambar perkembangan aliran Castor oil $dT/dx \leq 0$

**I.  $b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$**



t = 30 detik



t = 50 detik



t = 90 detik

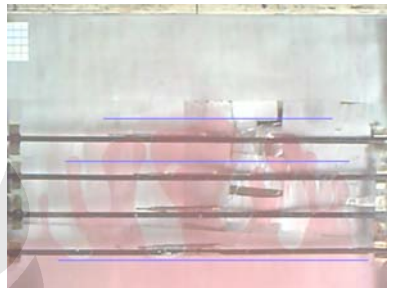
**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -4 \text{ }^\circ\text{C/cm}$**



t = 35 detik



t = 60 detik



t = 100 detik

**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -2.5 \text{ }^\circ\text{C/cm}$**



t = 35 detik



t = 70 detik



t = 165 detik

**$b = 0.8 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$**



t = 8 detik

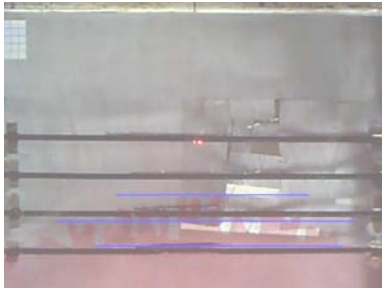


t = 10 detik

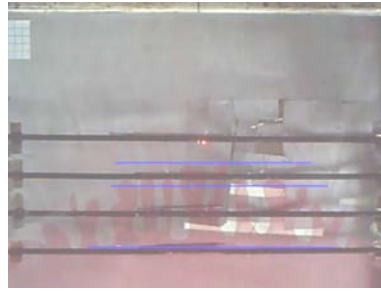


t = 14 detik

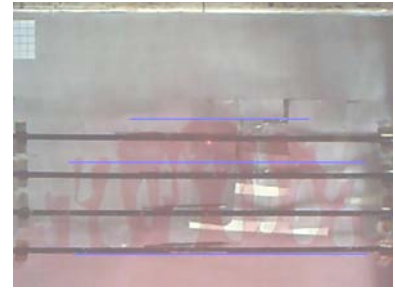
**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 14 detik



t = 22 detik

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 12 detik



t = 23 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 9 detik



t = 15 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 7 detik

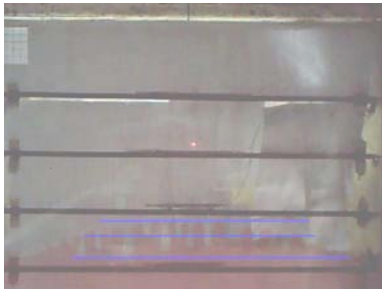


t = 10 detik



t = 20 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 9 detik



t = 16 detik

**II.  $b = 1.2 \text{ mm}, \alpha = 15^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 30 detik



t = 50 detik



t = 70 detik

**$b = 1.2 \text{ mm}, \alpha = 15^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 29 detik



t = 57 detik



t = 105 detik

**$b = 1.2 \text{ mm}, \alpha = 15^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 30 detik

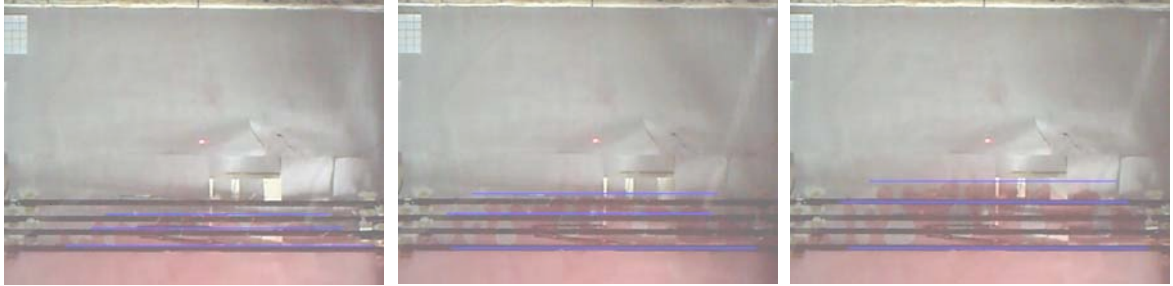


t = 75 detik



t = 180 detik

**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 9 detik

t = 11 detik

t = 13 detik

**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 9 detik

t = 13 detik

t = 22 detik

**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 10 detik

t = 22 detik

t = 33 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 6 detik

t = 10 detik

t = 15 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 7 detik

t = 13 detik

t = 20 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 6 detik

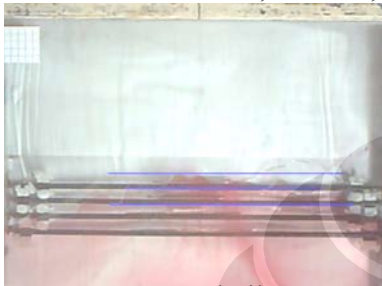


t = 14 detik



t = 23 detik

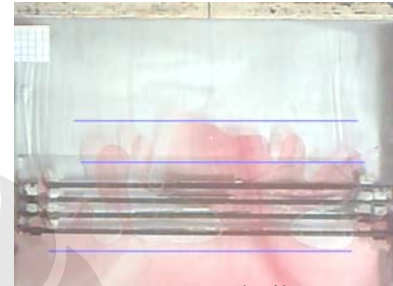
**III.  $b = 1.5 \text{ mm}, \alpha = 15^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 40 detik



t = 70 detik



t = 110 detik

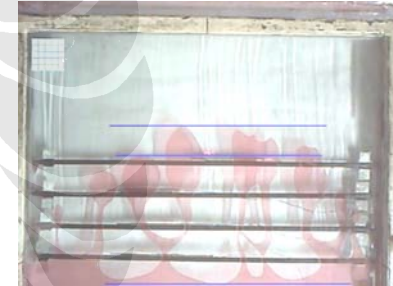
**$b = 1.5 \text{ mm}, \alpha = 15^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 25 detik



t = 60 detik

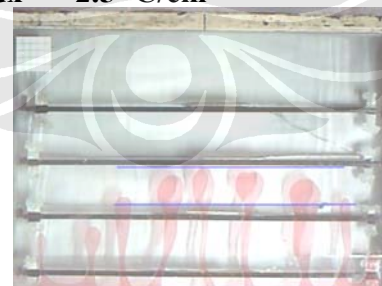


t = 120 detik

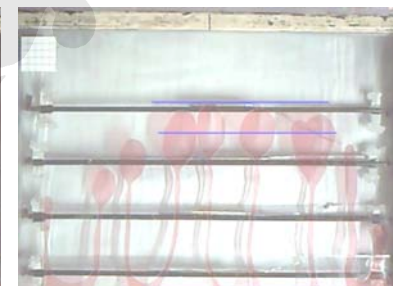
**$b = 1.5 \text{ mm}, \alpha = 15^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 45 detik



t = 125 detik

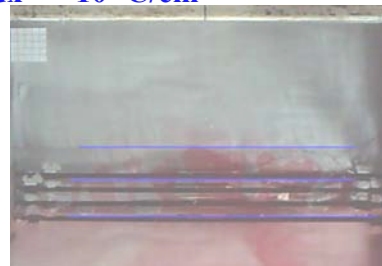


t = 225 detik

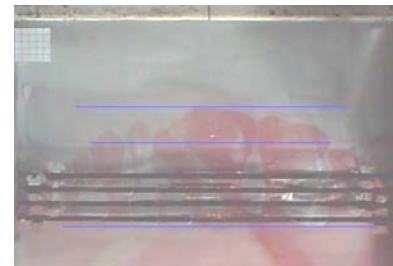
**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 10 detik

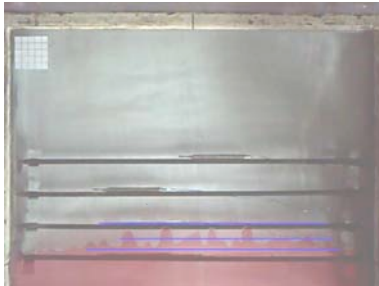


t = 14 detik



t = 20 detik

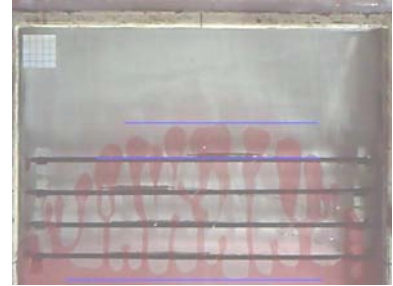
**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 9 detik

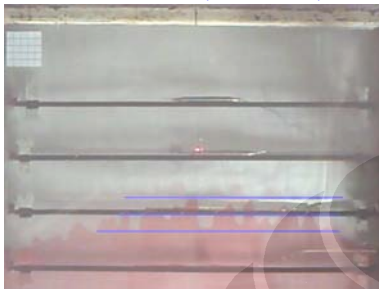


t = 15 detik

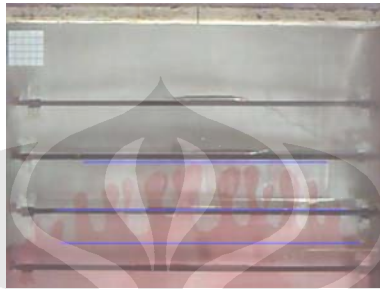


t = 23 detik

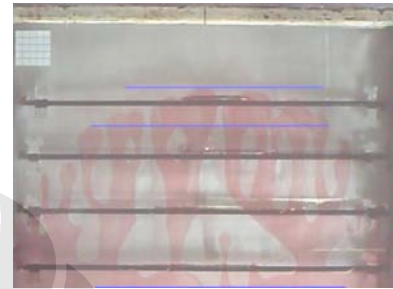
**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 15 detik



t = 30 detik

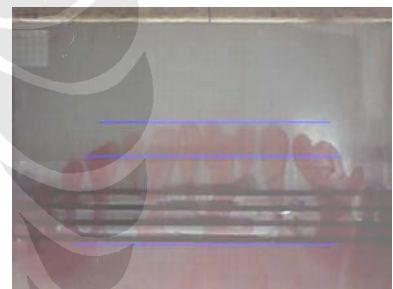
**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 8 detik



t = 13 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 10 detik

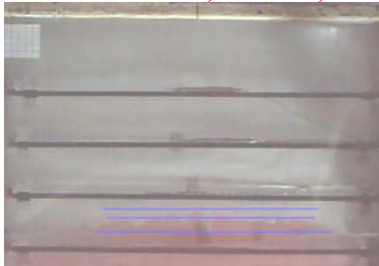


t = 12 detik



t = 15 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 12 detik

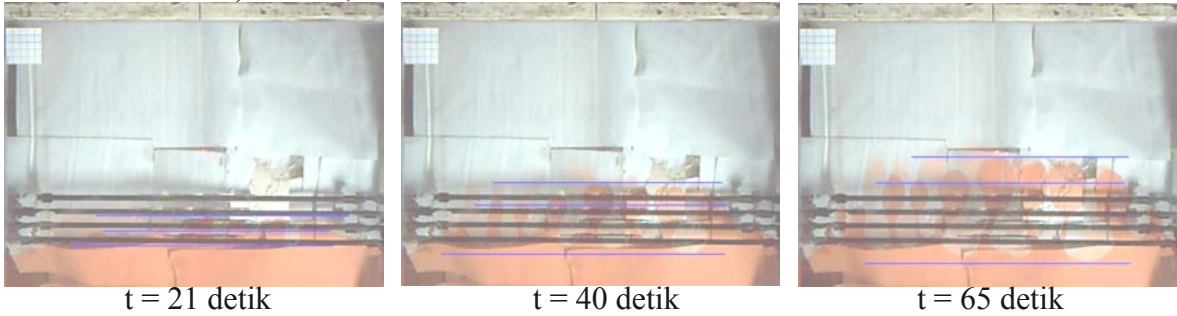


t = 22 detik

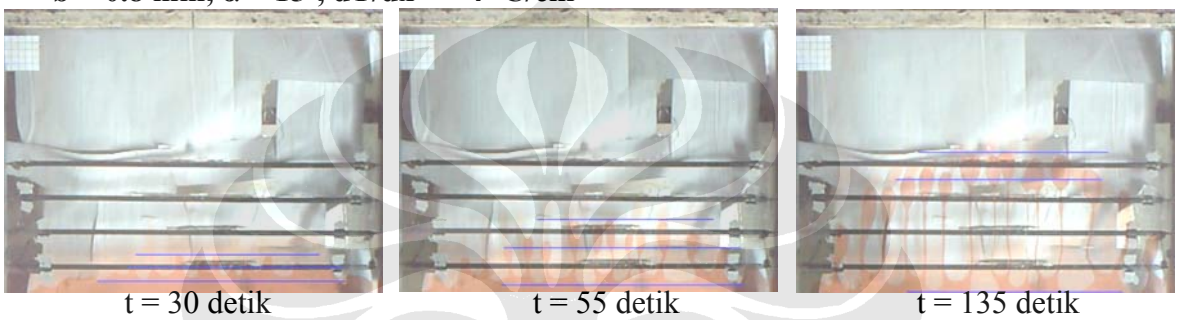


## Gambar perkembangan aliran SAE 30 $dT/dx \leq 0$

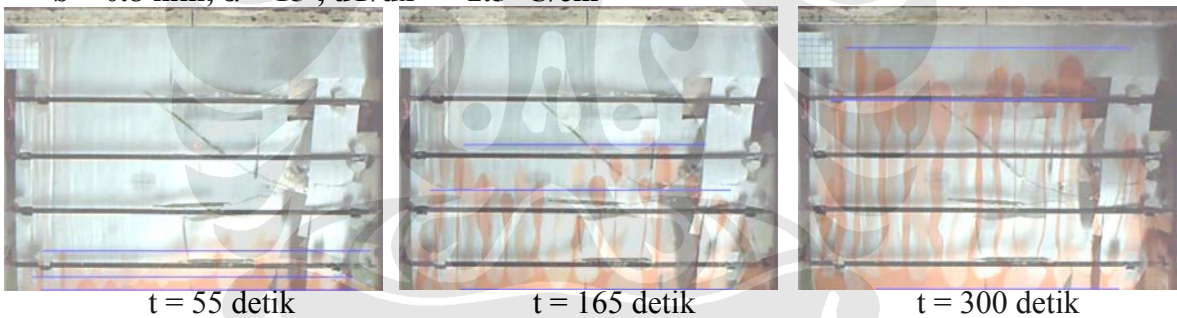
**I.  $b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$**



**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -4 \text{ }^\circ\text{C/cm}$**



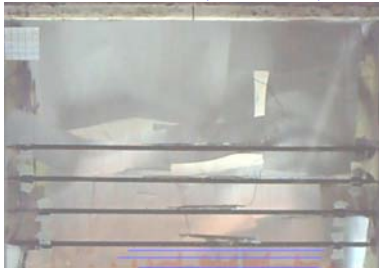
**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -2.5 \text{ }^\circ\text{C/cm}$**



**$b = 0.8 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$**



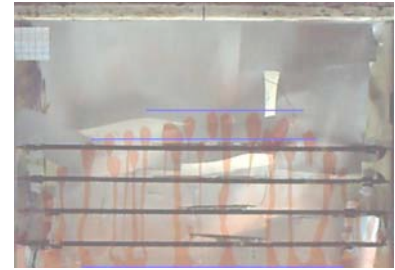
**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 20 detik



t = 40 detik

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 18 detik



t = 31 detik



t = 50 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 9 detik

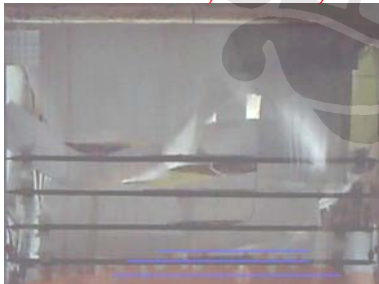


t = 12 detik

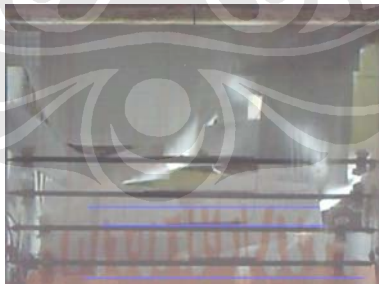


t = 20 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 10 detik



t = 17 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 6 detik

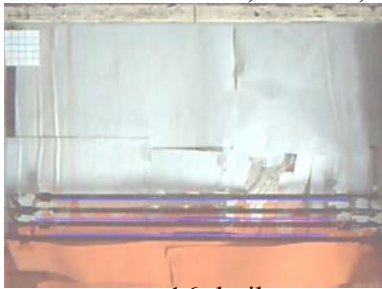


t = 14 detik

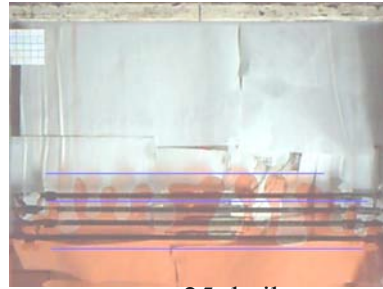


t = 30 detik

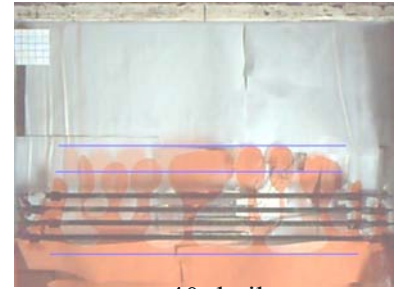
**II.  $b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 16 detik



t = 25 detik



t = 40 detik

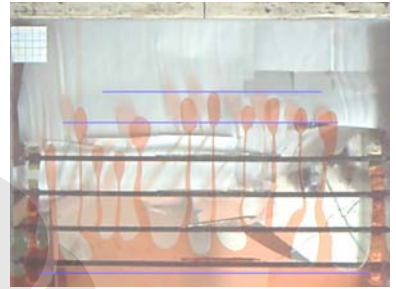
**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 30 detik



t = 50 detik

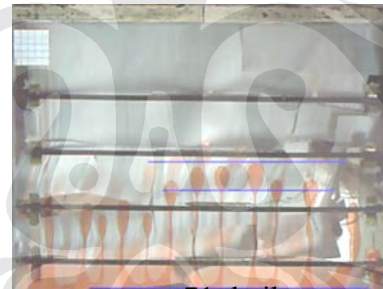


t = 90 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 30 detik



t = 71 detik



t = 130 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 7 detik



t = 10 detik

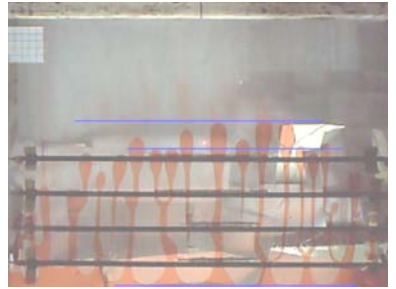
**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 10 detik

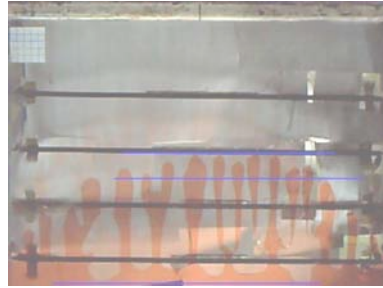


t = 17 detik

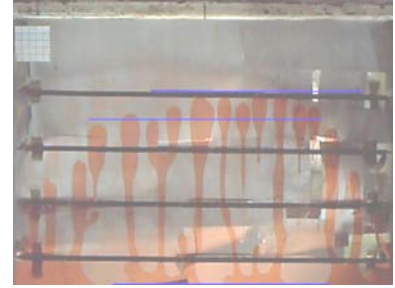
**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 8 detik



t = 12 detik

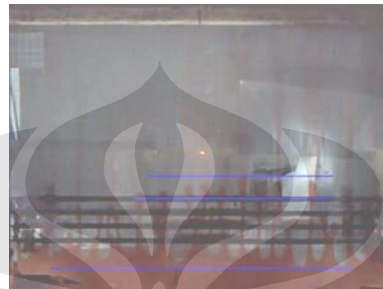


t = 17 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 7 detik



t = 10 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 9 detik



t = 13 detik

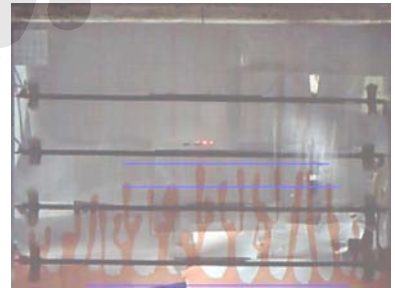
**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 7 detik



t = 9 detik



t = 11 detik



t = 14 detik



t = 17 detik

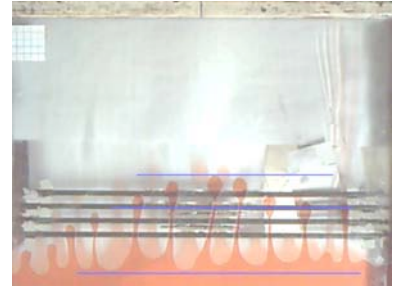
III.  $b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$



$t = 13 \text{ detik}$



$t = 19 \text{ detik}$



$t = 25 \text{ detik}$

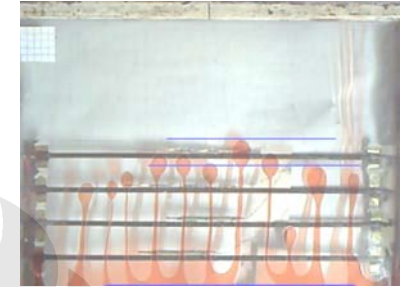
$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -4 \text{ }^\circ\text{C/cm}$



$t = 18 \text{ detik}$



$t = 24 \text{ detik}$



$t = 37 \text{ detik}$

$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = -2.5 \text{ }^\circ\text{C/cm}$



$t = 17 \text{ detik}$

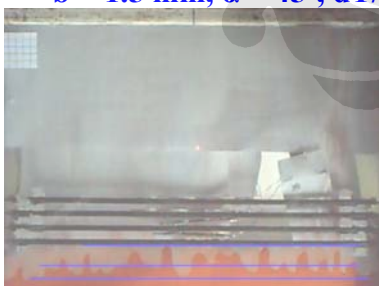


$t = 31 \text{ detik}$



$t = 45 \text{ detik}$

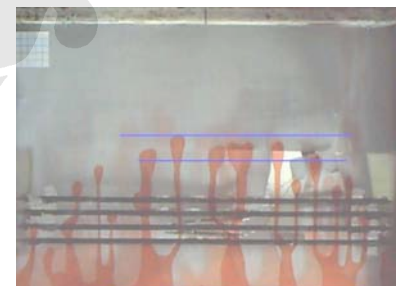
$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = -10 \text{ }^\circ\text{C/cm}$



$t = 5 \text{ detik}$

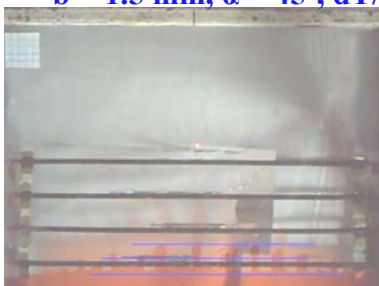


$t = 7 \text{ detik}$

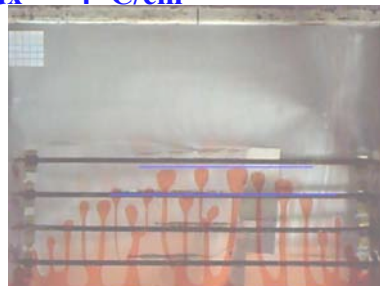


$t = 10 \text{ detik}$

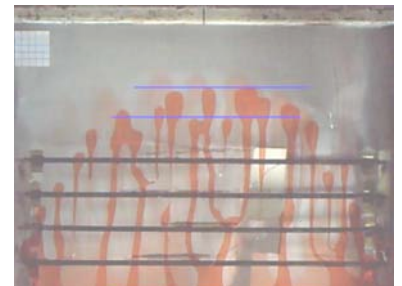
$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = -4 \text{ }^\circ\text{C/cm}$



$t = 5 \text{ detik}$

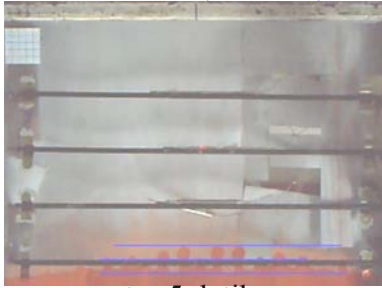


$t = 8 \text{ detik}$



$t = 12 \text{ detik}$

**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 9 detik

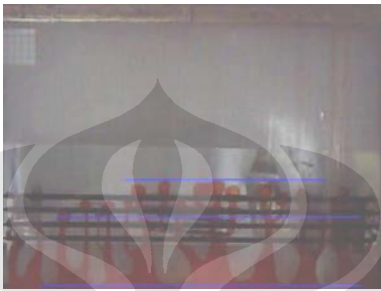


t = 13 detik

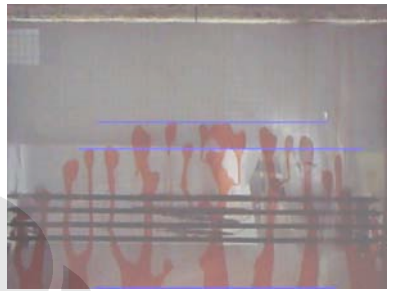
**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 10 \text{ }^\circ\text{C/cm}$**



t = 4 detik



t = 6 detik



t = 8 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 4 \text{ }^\circ\text{C/cm}$**



t = 4 detik



t = 6 detik



t = 8 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = - 2.5 \text{ }^\circ\text{C/cm}$**



t = 3 detik



t = 4 detik



t = 6 detik



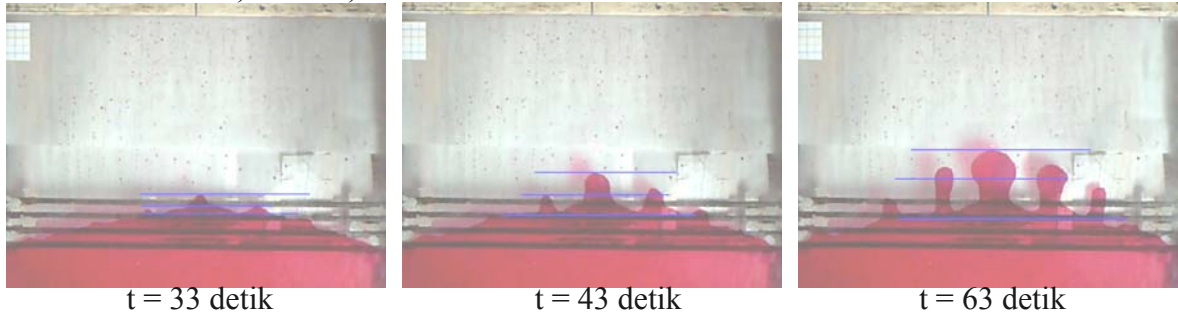
t = 8 detik



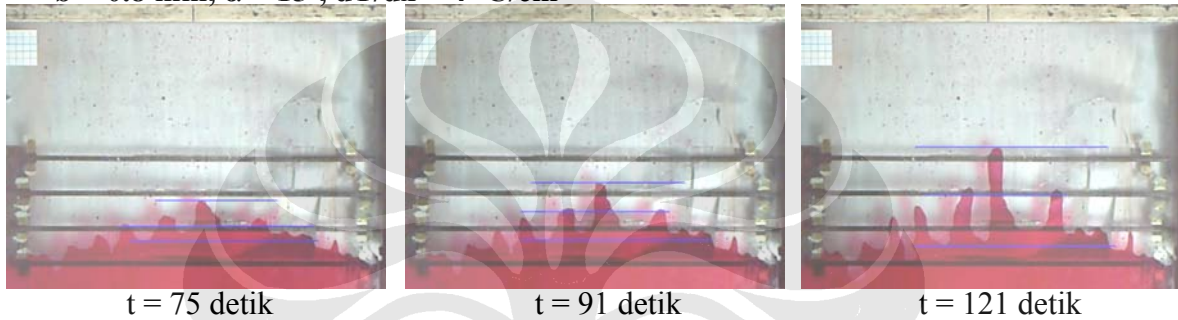
t = 10 detik

## Gambar perkembangan aliran Glycerin $dT/dx \geq 0$

**I.  $b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



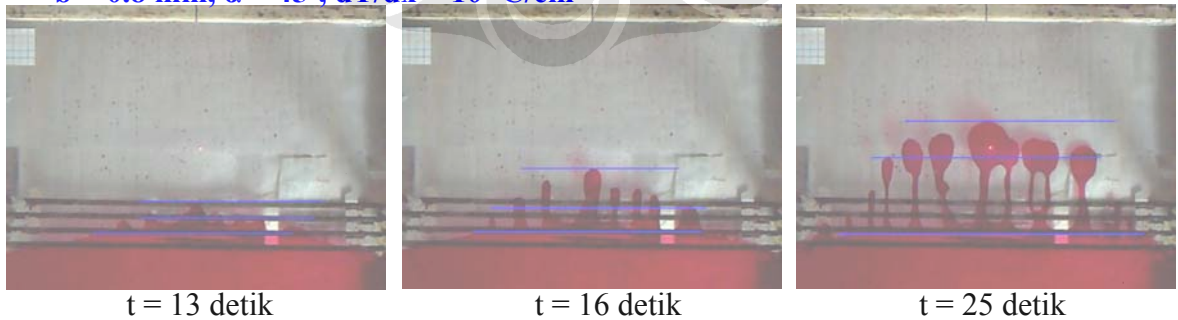
**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



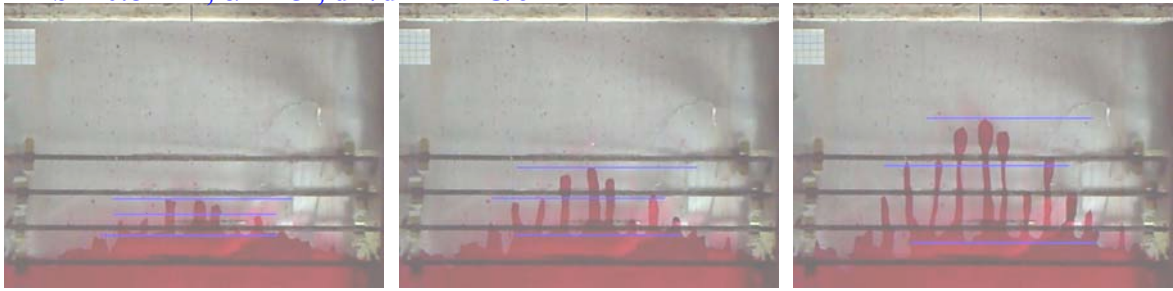
**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



**$b = 0.8 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 23 detik

t = 28 detik

t = 35 detik

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 25 detik

t = 36 detik

t = 44 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 10 detik

t = 13 detik

t = 18 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**

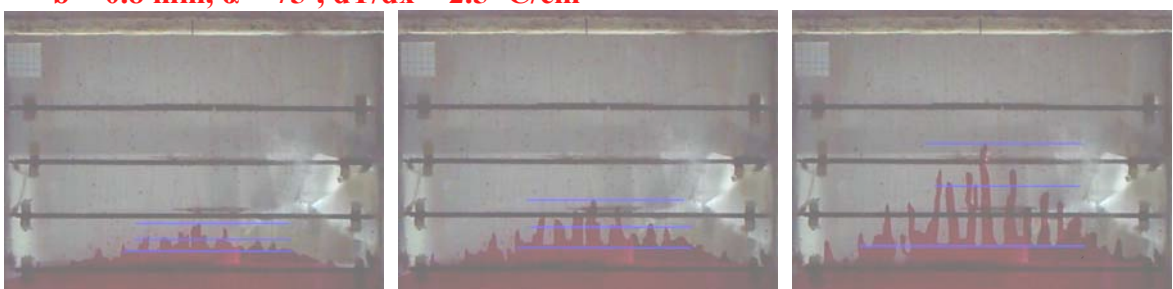


t = 17 detik

t = 21 detik

t = 24 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



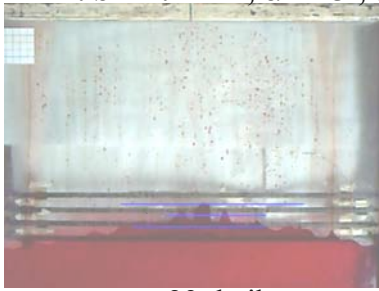
t = 15 detik

t = 19 detik

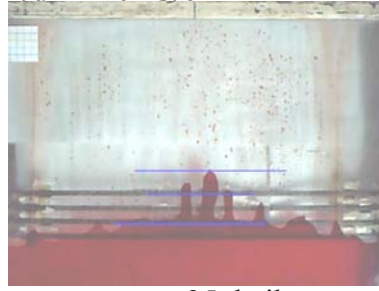
t = 26 detik



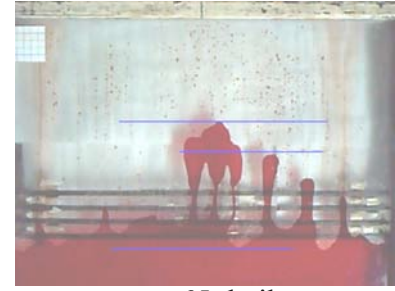
**II.  $b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 23 detik



t = 35 detik



t = 65 detik

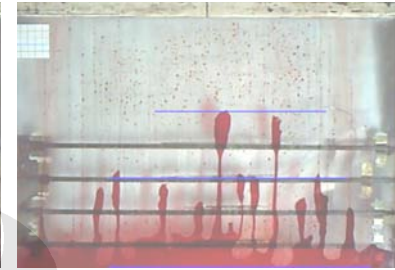
**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 30 detik



t = 70 detik



t = 105 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 50 detik

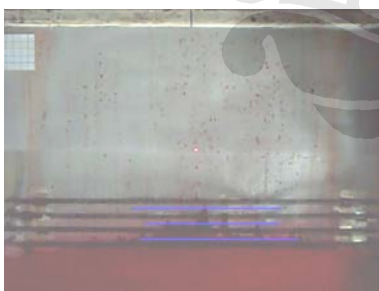


t = 170 detik



t = 245 detik

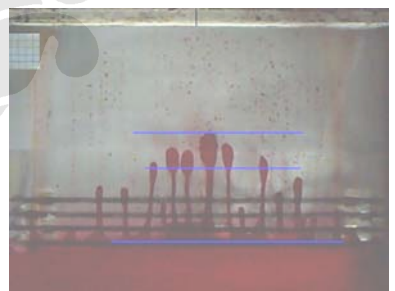
**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 13 detik



t = 17 detik

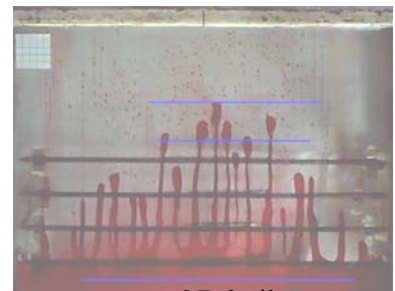
**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 11 detik

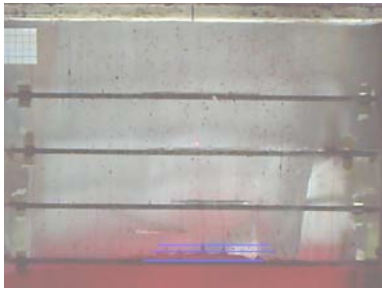


t = 19 detik

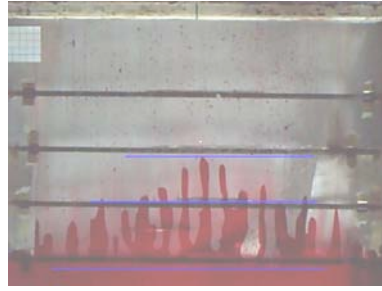


t = 27 detik

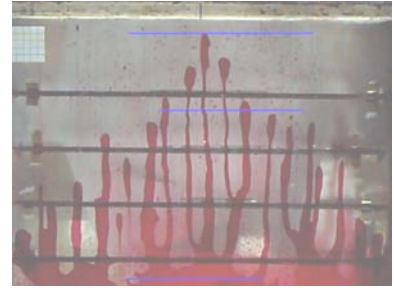
$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$



t = 10 detik



t = 28 detik



t = 42 detik

$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$



t = 8 detik

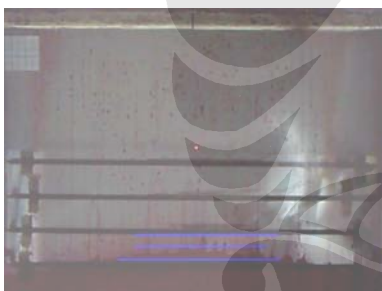


t = 10 detik

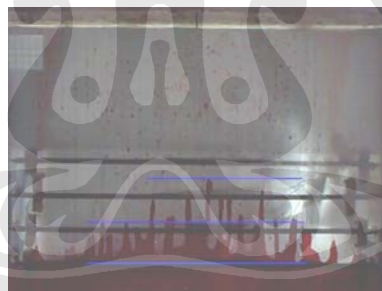


t = 14 detik

$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$



t = 8 detik

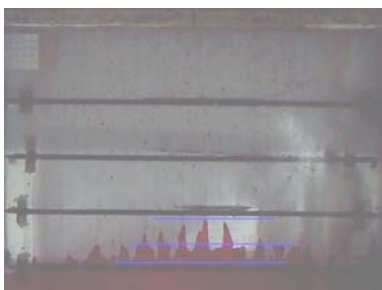


t = 13 detik

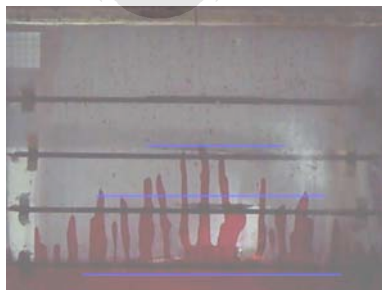


t = 17 detik

$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$



t = 12 detik

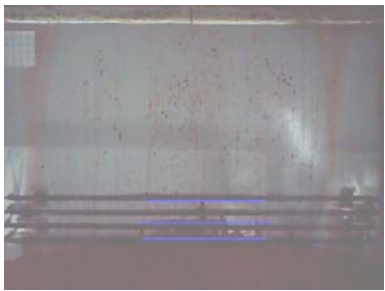


t = 20 detik

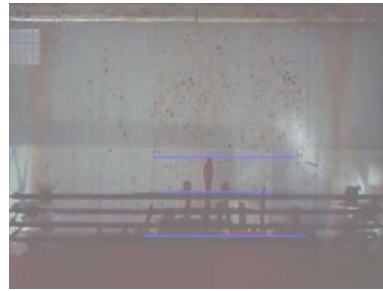


t = 26 detik

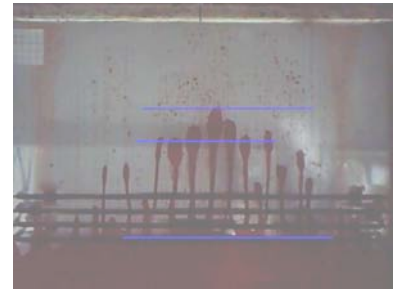
**III.  $b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 8 detik



t = 10 detik



t = 14 detik

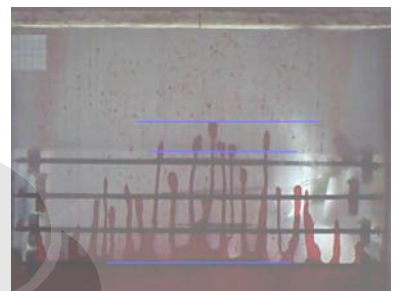
**$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 8 detik

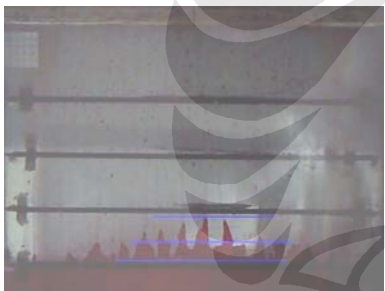


t = 13 detik

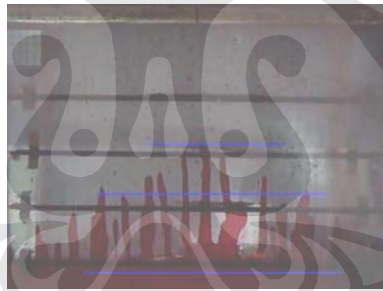


t = 17 detik

**$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 12 detik

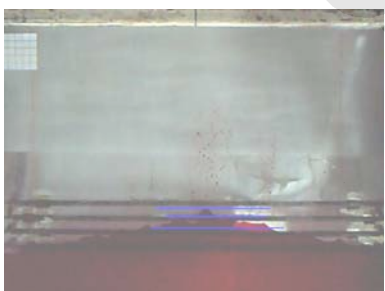


t = 20 detik



t = 26 detik

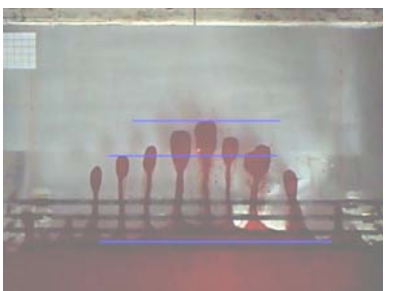
**$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 10 detik

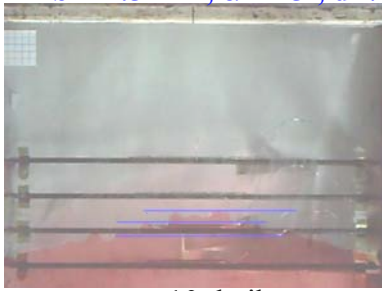


t = 12 detik

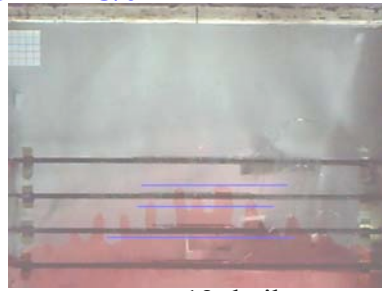


t = 14 detik

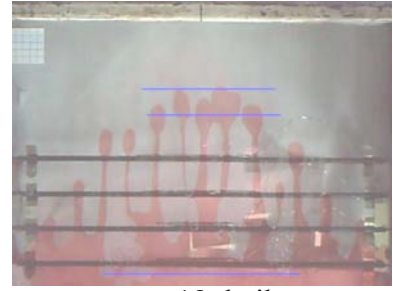
**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 10 detik

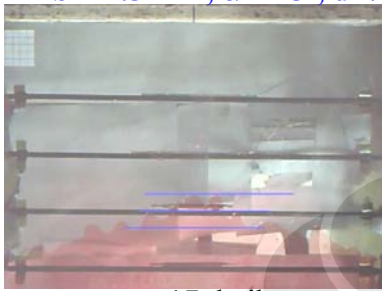


t = 12 detik



t = 18 detik

**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 17 detik



t = 24 detik



t = 30 detik

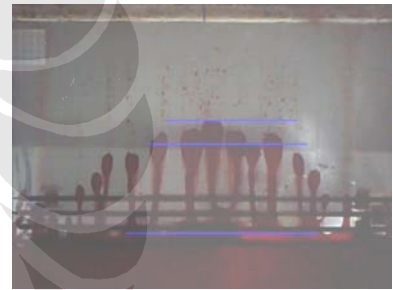
**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 10 detik



t = 12 detik

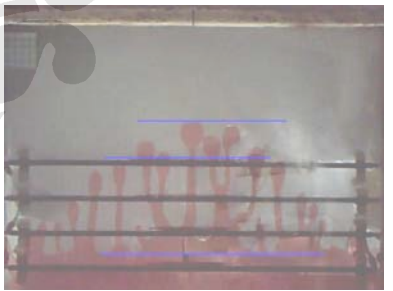
**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 9 detik



t = 11 detik

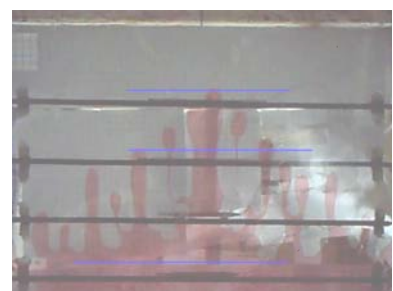
**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 13 detik



t = 17 detik



t = 20 detik

## Gambar perkembangan aliran Castor oil $dT/dx \geq 0$

I.  $b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$



t = 18 detik

t = 30 detik

t = 50 detik

$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$



t = 35 detik

t = 60 detik

t = 80 detik

$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$



t = 45 detik

t = 100 detik

t = 160 detik

$b = 0.8 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$

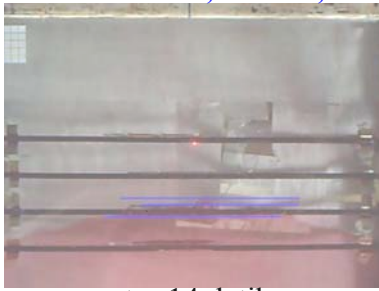


t = 10 detik

t = 14 detik

t = 20 detik

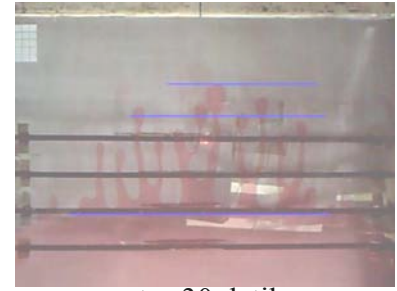
**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 14 detik

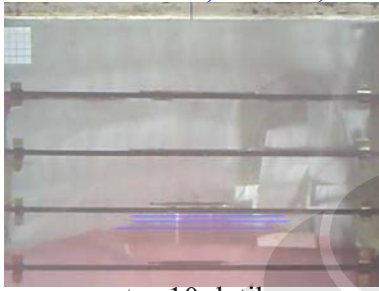


t = 20 detik



t = 30 detik

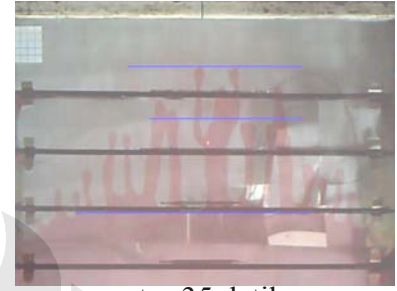
**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 25 detik

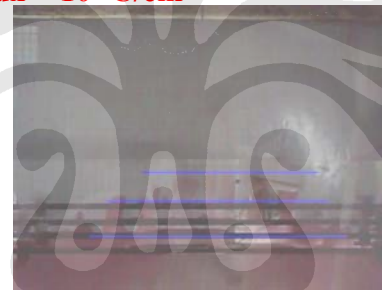


t = 35 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 9 detik

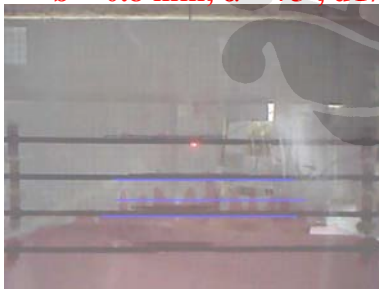


t = 12 detik



t = 17 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 14 detik



t = 18 detik



t = 25 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 12 detik

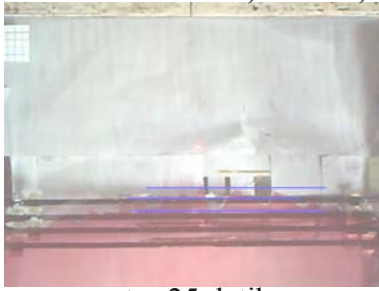


t = 19 detik



t = 26 detik

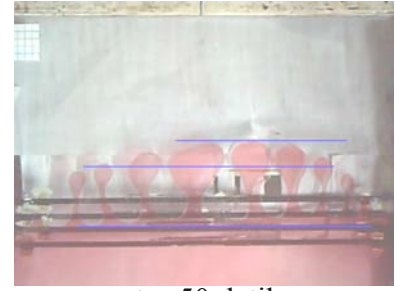
**II.  $b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 25 detik

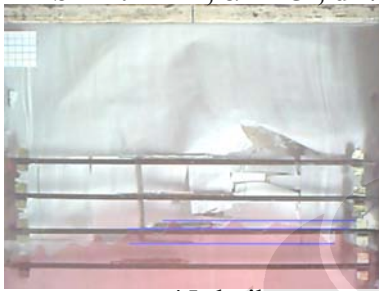


t = 35 detik

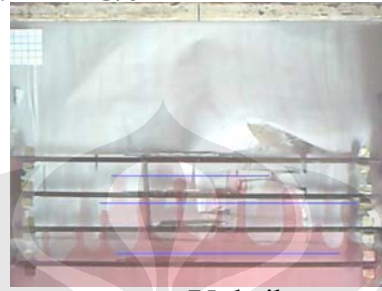


t = 50 detik

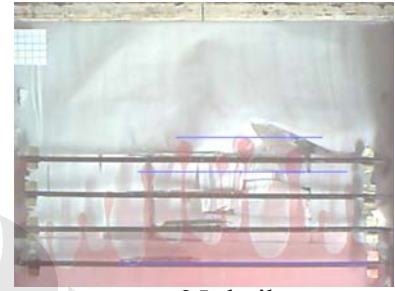
**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 45 detik



t = 75 detik



t = 95 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 85 detik

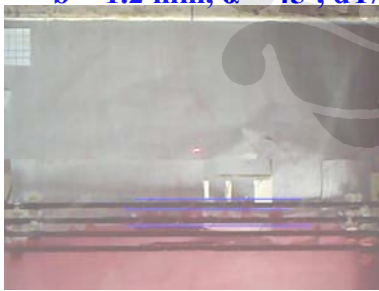


t = 230 detik



t = 305 detik

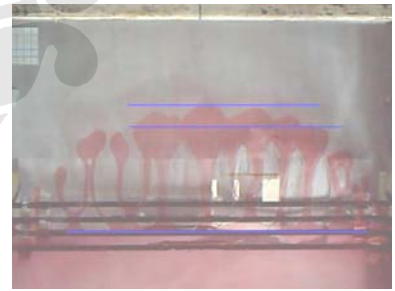
**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 15 detik



t = 25 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 15 detik

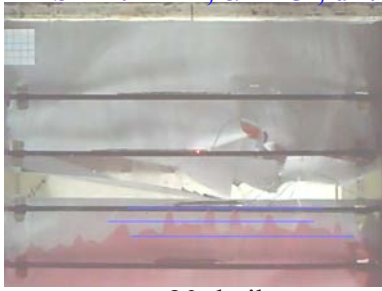


t = 20 detik



t = 25 detik

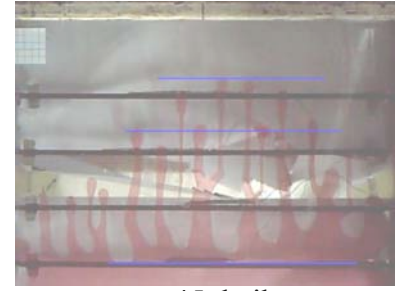
**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 20 detik



t = 35 detik



t = 45 detik

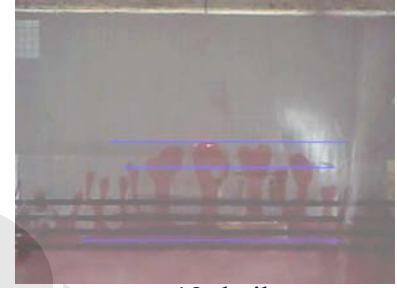
**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 9 detik



t = 12 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 9 detik

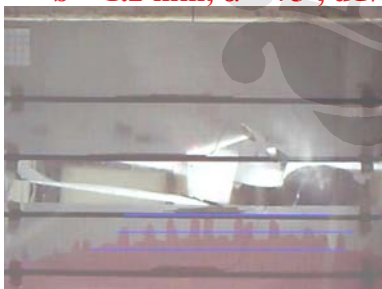


t = 15 detik



t = 20 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 15 detik



t = 26 detik



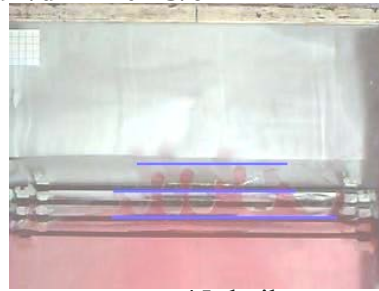
t = 32 detik



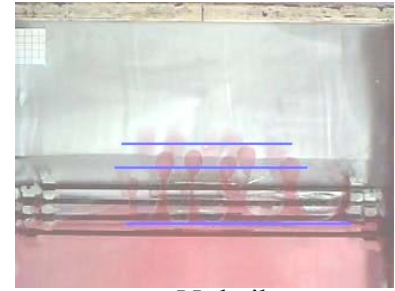
III.  $b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$



t = 35 detik



t = 45 detik



t = 55 detik

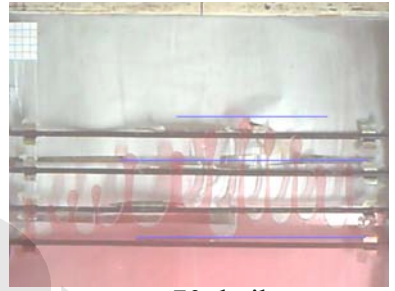
$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$



t = 35 detik



t = 55 detik



t = 70 detik

$b = 1.5 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$



t = 55 detik

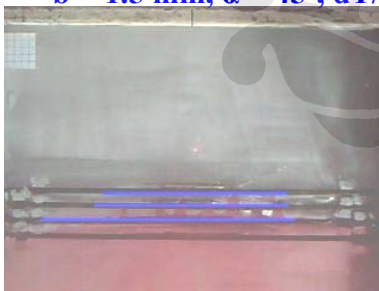


t = 100 detik



t = 155 detik

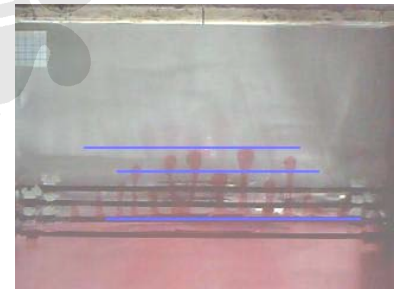
$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$



t = 16 detik

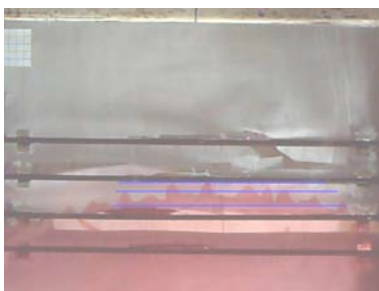


t = 18 detik



t = 20 detik

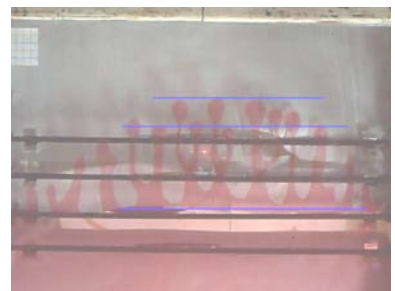
$b = 1.5 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$



t = 14 detik



t = 18 detik



t = 23 detik

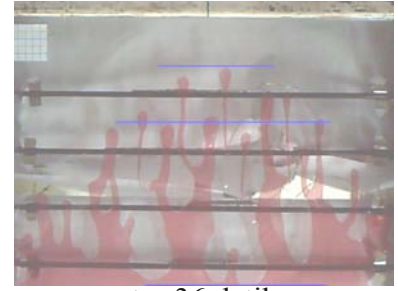
**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 15 detik

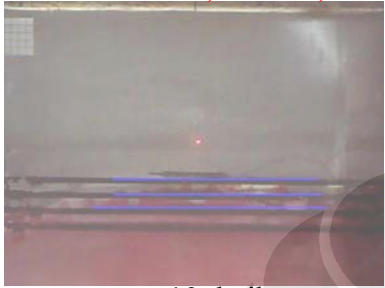


t = 25 detik



t = 36 detik

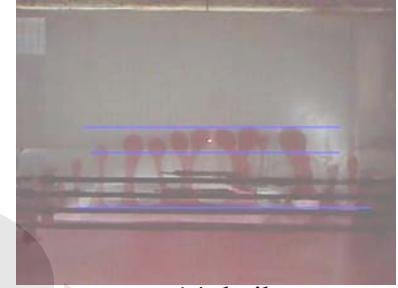
**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 10 detik



t = 12 detik



t = 14 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 11 detik



t = 14 detik



t = 18 detik

**$b = 1.5 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 13 detik



t = 19 detik



t = 25 detik

## Gambar perkembangan aliran SAE 30 $dT/dx \geq 0$

**I.  $b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 25 detik

t = 40 detik

t = 80 detik

**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**

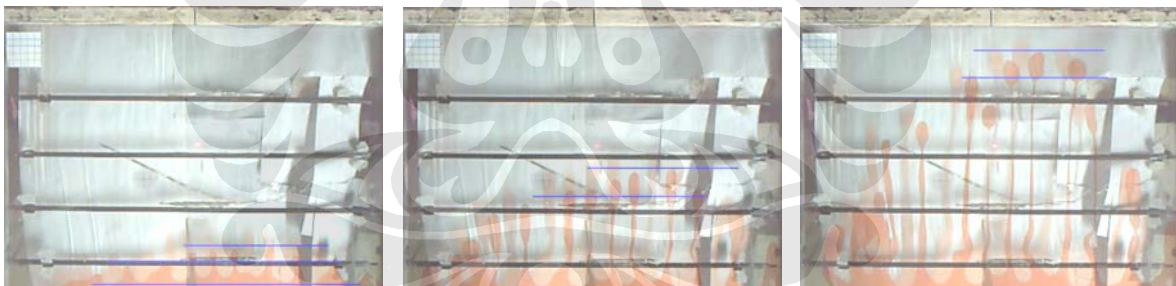


t = 50 detik

t = 77 detik

t = 100 detik

**$b = 0.8 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 65 detik

t = 175 detik

t = 255 detik

**$b = 0.8 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**

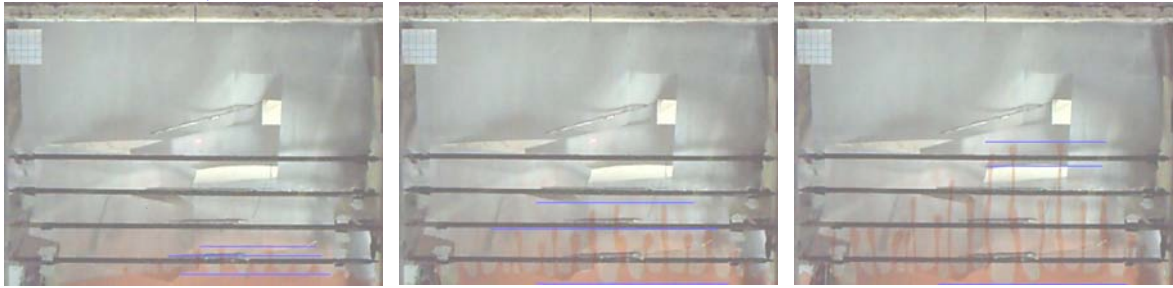


t = 15 detik

t = 21 detik

t = 25 detik

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 15 detik

t = 23 detik

t = 30 detik

**$b = 0.8 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 20 detik

t = 42 detik

t = 52 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 13 detik

t = 17 detik

t = 20 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 9 detik

t = 13 detik

t = 19 detik

**$b = 0.8 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**

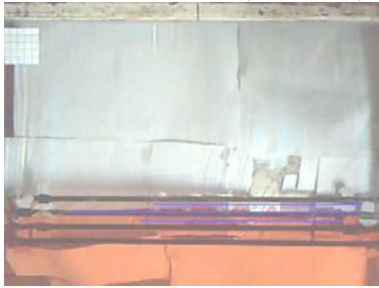


t = 11 detik

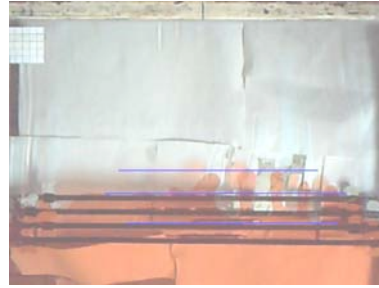
t = 26 detik

t = 33 detik

**II.  $b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 11 detik



t = 20 detik



t = 30 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 42 detik



t = 64 detik



t = 92 detik

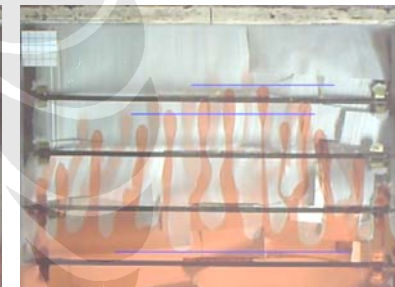
**$b = 1.2 \text{ mm}$ ,  $\alpha = 15^\circ$ ,  $dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 28 detik



t = 50 detik



t = 82 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 7 detik



t = 9 detik



t = 12 detik

**$b = 1.2 \text{ mm}$ ,  $\alpha = 45^\circ$ ,  $dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 10 detik

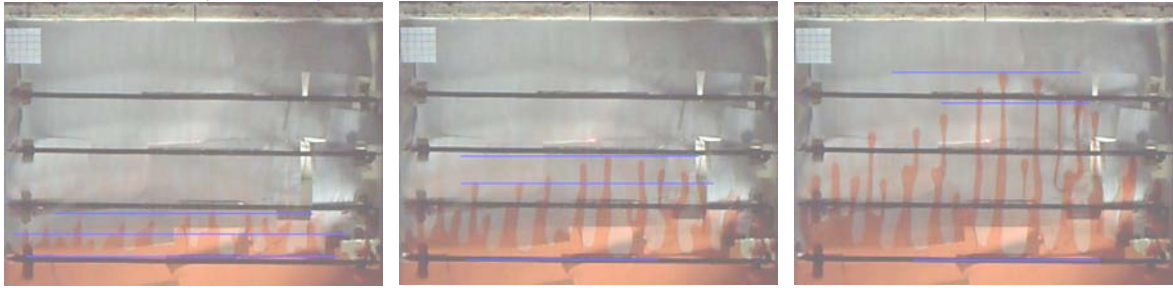


t = 15 detik



t = 21 detik

**$b = 1.2 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**

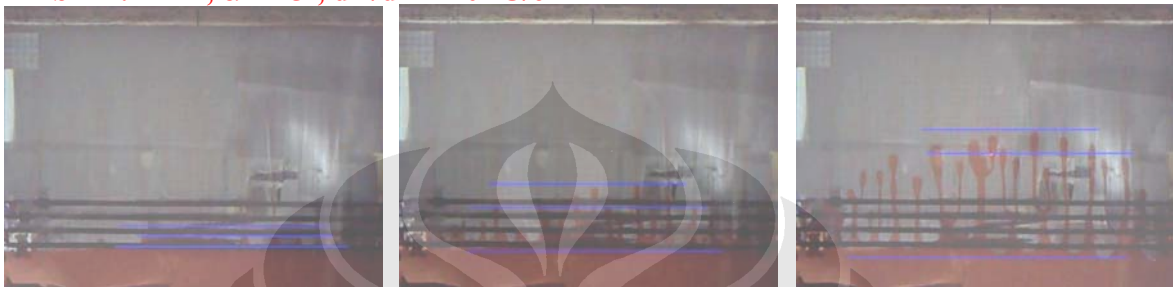


t = 13 detik

t = 19 detik

t = 25 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik

t = 7 detik

t = 10 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 8 detik

t = 12 detik

t = 16 detik

**$b = 1.2 \text{ mm}, \alpha = 75^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 11 detik

t = 16 detik

t = 21 detik

**III.  $b = 1.5 \text{ mm}, \alpha = 15^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**

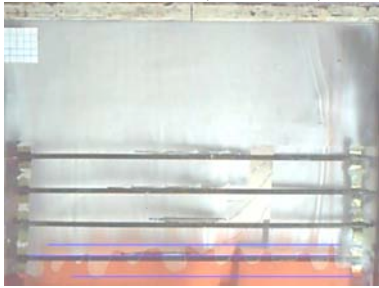


t = 10 detik

t = 14 detik

t = 19 detik

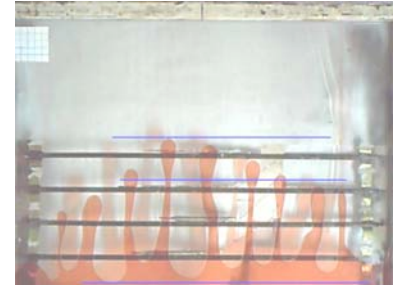
**$b = 1.5 \text{ mm}, \alpha = 15^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 17 detik



t = 28 detik

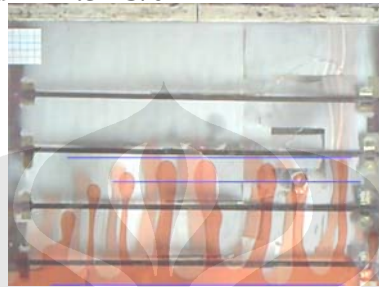


t = 41 detik

**$b = 1.5 \text{ mm}, \alpha = 15^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 25 detik



t = 47 detik



t = 63 detik

**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 7 detik



t = 9 detik

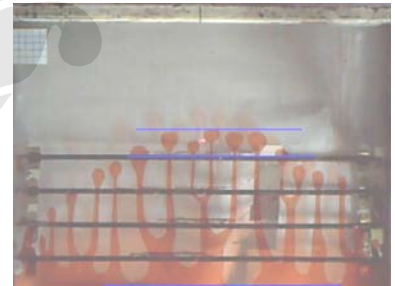
**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 8 detik



t = 11 detik

**$b = 1.5 \text{ mm}, \alpha = 45^\circ, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 8 detik

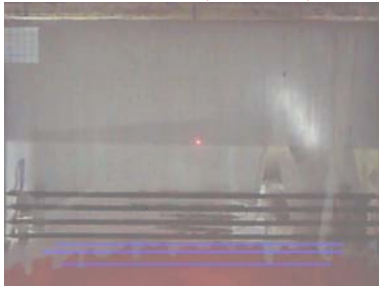


t = 12 detik

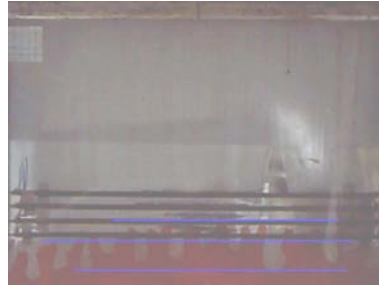


t = 16 detik

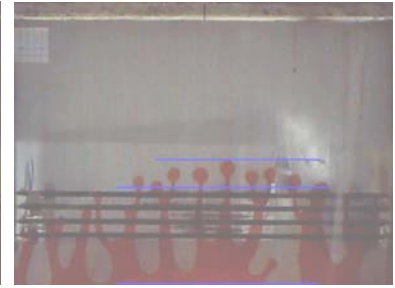
**$b = 1.5 \text{ mm}, \alpha = 75, dT/dx = 10 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 6 detik



t = 8 detik

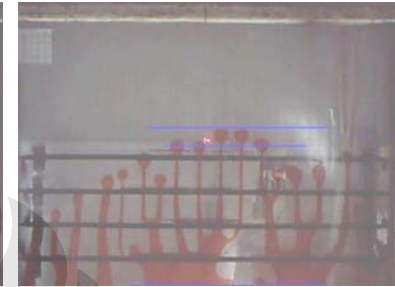
**$b = 1.5 \text{ mm}, \alpha = 75, dT/dx = 4 \text{ }^\circ\text{C/cm}$**



t = 5 detik



t = 7 detik



t = 9 detik

**$b = 1.5 \text{ mm}, \alpha = 75, dT/dx = 2.5 \text{ }^\circ\text{C/cm}$**



t = 6 detik



t = 10 detik

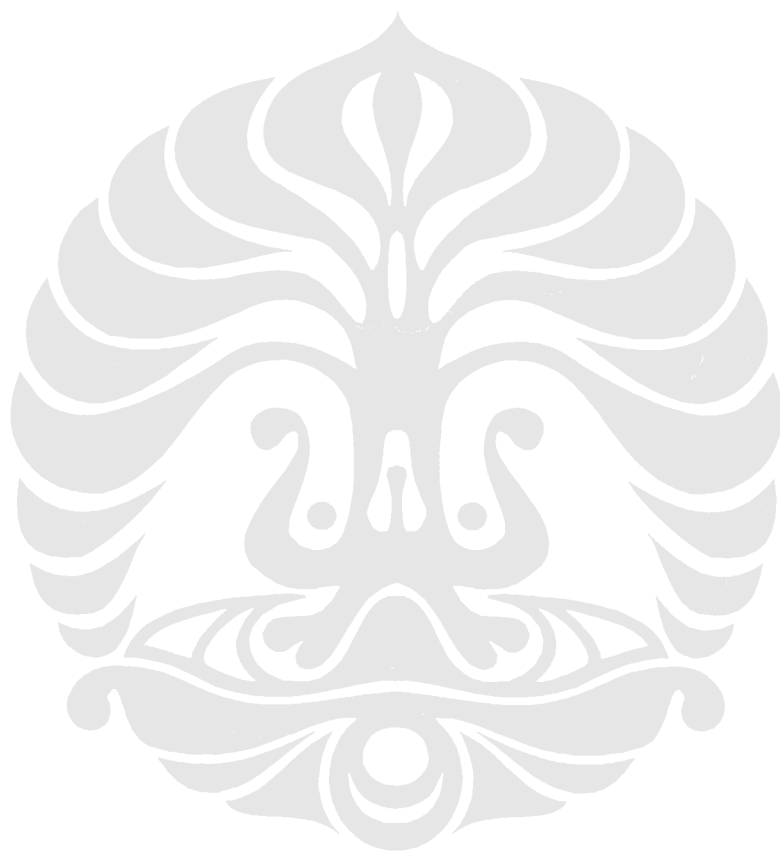


t = 13 detik



### **LAMPIRAN 3**

**Tabel data perubahan bentuk tiap satuan waktu  $dT/dx \leq 0$**



## I. Glycerin

Glycerin,  $b = 0.8\text{mm}$ ,  $\alpha = 15$  derajat

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-10</b> °C/cm	1.	15	425,59	0,048	0	58,78	0	0	0,035	0,000
	2.	20	425,59	0,048	13,24	58,78	1,67	3,43	0,047	0,715
	3.	25	425,59	0,048	12,6	58,78	2,93	5,05	0,059	1,052
	4.	30	425,59	0,048	19,67	58,78	2,09	6,36	0,070	1,325
	5.	35	425,59	0,048	18,04	58,78	5,35	9,37	0,082	1,952
	6.	45	425,59	0,048	22,86	58,78	5,58	11,22	0,106	2,338
	7.	60	425,59	0,048	25,59	58,78	8,64	14,9	0,141	3,104
	8.	70	425,59	0,048	30,38	58,78	10,87	17,65	0,164	3,677
	9.	85	425,59	0,048	28	58,78	11,32	17,27	0,200	3,598
	10.	95	425,59	0,048	30,84	58,78	13,91	20,35	0,223	4,240
dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-4</b> °C/cm	1.	14	425,59	0,048	8,24	58,78	1,28	2,64	0,033	0,550
	2.	18	425,59	0,048	8,42	58,78	2,32	4,54	0,042	0,946
	3.	23	425,59	0,048	8,44	58,78	3,49	6,95	0,054	1,448
	4.	30	425,59	0,048	10,45	58,78	4,01	9,89	0,070	2,060
	5.	37	425,59	0,048	10,29	58,78	6,21	13,80	0,087	2,875
	6.	45	425,59	0,048	14,87	58,78	12,42	19,37	0,106	4,035
	7.	55	425,59	0,048	15,46	58,78	9,61	20,27	0,129	4,223
	8.	70	425,59	0,048	23,53	58,78	14,71	25,51	0,164	5,315
	9.	85	425,59	0,048	24,49	58,78	14,51	25,87	0,200	5,390
	10.	95	425,59	0,048	22,69	58,78	13,39	24,22	0,223	5,046
dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-2.5</b> °C/cm	1.	20	425,59	0,048	15,17	58,78	2,1	4,82	0,047	1,004
	2.	25	425,59	0,048	24,12	58,78	2,41	7,64	0,059	1,592
	3.	35	425,59	0,048	23,20	58,78	3,2	10,15	0,082	2,115
	4.	45	425,59	0,048	18,42	58,78	5,55	13,13	0,106	2,735
	5.	55	425,59	0,048	19,35	58,78	8,14	17,79	0,129	3,706
	6.	65	425,59	0,048	17,57	58,78	10,06	19,73	0,153	4,110
	7.	75	425,59	0,048	21,58	58,78	14,86	25,24	0,176	5,258
	8.	85	425,59	0,048	20,18	58,78	14,71	25,44	0,200	5,300
	9.	105	425,59	0,048	20,97	58,78	18,22	28,89	0,247	6,019
	10.	120	425,59	0,048	18,31	58,78	19,79	29,74	0,282	6,196

**Glycerin, b = 0.8mm,  $\alpha = 45$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-10 °C/cm</b>	1.	7	155,777	0,018	10,94	58,78	1,66	3,08	0,045	1,711
	2.	8	155,777	0,018	12,24	58,78	2,74	5,05	0,051	2,806
	3.	9	155,777	0,018	11,89	58,78	3,79	6,58	0,058	3,656
	4.	10	155,777	0,018	16,67	58,78	5,90	9,05	0,064	5,028
	5.	12	155,777	0,018	20,19	58,78	8,30	12,38	0,077	6,878
	6.	15	155,777	0,018	18,31	58,78	9,48	14,92	0,096	8,289
	7.	20	155,777	0,018	22,25	58,78	11,55	17,06	0,128	9,478
	8.	25	155,777	0,018	29,28	58,78	16,38	22,59	0,160	12,550
	9.	30	155,777	0,018	26,69	58,78	16,74	22,77	0,193	12,650
dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-4 °C/cm</b>	1.	4	155,777	0,018	0	58,78	0	0	0,026	0,000
	2.	6	155,777	0,018	6,29	58,78	2,13	4,02	0,039	2,233
	3.	8	155,777	0,018	11,36	58,78	3,57	7,32	0,051	4,067
	4.	10	155,777	0,018	13,32	58,78	8,28	12,69	0,064	7,050
	5.	13	155,777	0,018	13,75	58,78	13,58	18,77	0,083	10,428
	6.	15	155,777	0,018	16,95	58,78	14,12	19,73	0,096	10,961
	7.	20	155,777	0,018	24,44	58,78	19,37	26,39	0,128	14,661
	8.	25	155,777	0,018	25,78	58,78	24,71	30,99	0,160	17,217
dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-2.5 °C/cm</b>	1.	5	155,777	0,018	0	58,78	0	0	0,032	0,000
	2.	7	155,777	0,018	7,61	58,78	2,61	4,49	0,045	2,494
	3.	9	155,777	0,018	11,35	58,78	5,55	8,56	0,058	4,756
	4.	11	155,777	0,018	17,83	58,78	8,24	26,28	0,071	14,600
	5.	14	155,777	0,018	13,58	58,78	13,27	18,08	0,090	10,044
	6.	16	155,777	0,018	14,13	58,78	14,05	20,29	0,103	11,272
	7.	20	155,777	0,018	15,99	58,78	21,70	27,42	0,128	15,233
	8.	23	155,777	0,018	19,62	58,78	25,18	30,73	0,148	17,072
	9.	26	155,777	0,018	19,41	58,78	26,34	31,11	0,167	17,283

**Glycerin, b = 0.8mm,  $\alpha = 75$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
<b>-4 °C/cm</b>	1.	3	114,036	0,013	0	58,78	0	0	0,026	0,000
	2.	5	114,036	0,013	6,36	58,78	3,09	4,19	0,044	3,223
	3.	6	114,036	0,013	9,49	58,78	6,19	8,56	0,053	6,585
	4.	8	114,036	0,013	14,17	58,78	10,57	15,76	0,070	12,123
	5.	10	114,036	0,013	12,55	58,78	18,94	21,71	0,088	16,700
	6.	12	114,036	0,013	15,85	58,78	20,43	24,21	0,105	18,623
	7.	15	114,036	0,013	18,79	58,78	24,64	29,97	0,132	23,054
	8.	18	114,036	0,013	20,06	58,78	26,38	31,98	0,158	24,600
	9.	21	114,036	0,013	27,83	58,78	28,24	36,27	0,184	27,900

**Glycerin, b = 1.2mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	12	283,727	0,048	2,31	58,78	1,43	2,36	0,042	0,492
	2.	16	283,727	0,048	9,02	58,78	1,94	4,68	0,056	0,975
	3.	22	283,727	0,048	8,29	58,78	3,27	7,15	0,078	1,490
	4.	28	283,727	0,048	8,2	58,78	4,94	11,09	0,099	2,310
	5.	35	283,727	0,048	7,77	58,78	9,61	14,35	0,123	2,990
	6.	43	283,727	0,048	8,67	58,78	13,58	18,88	0,152	3,933
	7.	50	283,727	0,048	11,46	58,78	15,81	20,65	0,176	4,302
	8.	60	283,727	0,048	14,23	58,78	17,79	22,68	0,211	4,725
	9.	75	283,727	0,048	16,98	58,78	20,68	25,48	0,264	5,308

**Glycerin, b = 1.5mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	12	226,981	0,048	4,49	58,78	1,89	2,87	0,053	0,598
	2.	16	226,981	0,048	5,09	58,78	4,98	7,49	0,070	1,560
	3.	19	226,981	0,048	6,31	58,78	5,17	8,67	0,084	1,806
	4.	23	226,981	0,048	9,75	58,78	9,04	13,62	0,101	2,838
	5.	26	226,981	0,048	11,69	58,78	12,98	18,06	0,115	3,763
	6.	32	226,981	0,048	14,74	58,78	13,58	18,7	0,141	3,896
	7.	40	226,981	0,048	20,65	58,78	17,91	24,22	0,176	5,046
	8.	50	226,981	0,048	21,49	58,78	19,13	24,45	0,220	5,094
	9.	60	226,981	0,048	22,98	58,78	20,27	26,05	0,264	5,427
	10.	75	226,981	0,048	25,11	58,78	25,59	31,63	0,330	6,590

**II. CASTOR OIL**

**castor, 0.8mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-10 °C/cm	1.	30	327,282	0,044	43,33	58,78	1,22	7,28	0,092	1,655
	2.	35	327,282	0,044	36	58,78	1	6,66	0,107	1,514
	3.	40	327,282	0,044	38,89	58,78	1,33	7,7	0,122	1,750
	4.	45	327,282	0,044	39,02	58,78	1,85	8,81	0,137	2,002
	5.	50	327,282	0,044	34,34	58,78	1,84	8,74	0,153	1,986
	6.	60	327,282	0,044	37,36	58,78	3,69	11,31	0,183	2,571
	7.	75	327,282	0,044	36,29	58,78	6,13	13,9	0,229	3,159
	8.	90	327,282	0,044	37,94	58,78	7,73	16,6	0,275	3,773
	9.	105	327,282	0,044	38,57	58,78	9,29	18,66	0,321	4,241
	10.	120	327,282	0,044	41,96	58,78	10,89	21,87	0,367	4,971
	11.	135	327,282	0,044	38,09	58,78	10,53	21,07	0,412	4,789
	12.	150	327,282	0,044	43,52	58,78	13,04	24,71	0,458	5,616

**castor, 0.8mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	15	327,282	0,044	9,01	58,78	1,36	1,92	0,046	0,436
	2.	25	327,282	0,044	14,25	58,78	1,69	3,84	0,076	0,873
	3.	35	327,282	0,044	17,27	58,78	1,91	4,92	0,107	1,118
	4.	50	327,282	0,044	24,89	58,78	1,54	7,96	0,153	1,809
	5.	60	327,282	0,044	22,54	58,78	3,01	10,02	0,183	2,277
	6.	85	327,282	0,044	21,49	58,78	6,25	16,82	0,260	3,823
	7.	100	327,282	0,044	20,3	58,78	8,32	19,69	0,306	4,475
	8.	115	327,282	0,044	19,1	58,78	8,45	19,18	0,351	4,359
	9.	130	327,282	0,044	21,58	58,78	11,3	23,39	0,397	5,316
	10.	145	327,282	0,044	23,07	58,78	12,72	26,11	0,443	5,934

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-2.5 °C/cm	1.	10	327,282	0,044	0	58,78	0	0	0,031	0,000
	2.	15	327,282	0,044	17,59	58,78	0,3	1,51	0,046	0,343
	3.	25	327,282	0,044	13,81	58,78	1,04	3,09	0,076	0,702
	4.	35	327,282	0,044	14,99	58,78	1,91	5,54	0,107	1,259
	5.	45	327,282	0,044	19,19	58,78	2,62	8,45	0,137	1,921
	6.	70	327,282	0,044	15,37	58,78	2,31	11,54	0,214	2,623
	7.	80	327,282	0,044	13,65	58,78	2,27	12,8	0,244	2,909
	8.	95	327,282	0,044	13,22	58,78	3,77	15,68	0,290	3,564
	9.	110	327,282	0,044	14,2	58,78	2,87	17,29	0,336	3,930
	10.	135	327,282	0,044	15,84	58,78	4,03	17,55	0,412	3,989

**castor, 0.8mm,  $\alpha = 45$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	3	119,794	0,026	0	58,78	0	0	0,025	0,000
	2.	6	119,794	0,026	15,65	58,78	1,04	2,64	0,050	1,015
	3.	7	119,794	0,026	19,47	58,78	0,83	2,76	0,058	1,062
	4.	10	119,794	0,026	21,55	58,78	1,59	6,13	0,083	2,358
	5.	11	119,794	0,026	24,59	58,78	2,19	8,06	0,092	3,100
	6.	14	119,794	0,026	20,19	58,78	2,15	9,25	0,117	3,558
	7.	16	119,794	0,026	20,81	58,78	3,48	13,04	0,134	5,015
	8.	22	119,794	0,026	16,3	58,78	4,27	15,53	0,184	5,973
	9.	25	119,794	0,026	16,95	58,78	5,14	18,39	0,209	7,073
	10.	30	119,794	0,026	16,71	58,78	4,25	19,71	0,250	7,581

**castor, 0.8mm,  $\alpha = 75$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	4	87,695	0,019	0	58,78	0	0	0,046	0,000
	2.	7	87,695	0,019	13,41	58,78	1,27	2,85	0,080	1,500
	3.	10	87,695	0,019	25,34	58,78	1,84	7,80	0,114	4,105
	4.	13	87,695	0,019	18,81	58,78	2,81	10,90	0,148	5,737
	5.	17	87,695	0,019	18,08	58,78	4,6	17,78	0,194	9,358
	6.	20	87,695	0,019	21,29	58,78	4,58	20,67	0,228	10,879
	7.	25	87,695	0,019	22,25	58,78	6,14	25,89	0,285	13,626
	8.	30	87,695	0,019	15,70	58,78	8,13	26,78	0,342	14,095

**castor, b = 1.2mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	15	218,188	0,044	19,62	58,78	0,48	1,29	0,069	0,293
	2.	22	218,188	0,044	24,69	58,78	0,87	2,57	0,101	0,584
	3.	29	218,188	0,044	26,9	58,78	1,09	4,55	0,133	1,034
	4.	36	218,188	0,044	23,64	58,78	1,88	6,71	0,165	1,525
	5.	43	218,188	0,044	20,53	58,78	3,06	8,56	0,197	1,945
	6.	50	218,188	0,044	19,37	58,78	3,74	9,84	0,229	2,236
	7.	57	218,188	0,044	17,66	58,78	3,47	11,01	0,261	2,502
	8.	64	218,188	0,044	16,56	58,78	4,29	14,63	0,293	3,325
	9.	71	218,188	0,044	13,46	58,78	4,51	14,81	0,325	3,366
	10.	78	218,188	0,044	13,3	58,78	5,26	16,21	0,357	3,684

**castor, b = 1.5mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	15	174,55	0,044	8,26	58,78	0,81	1,45	0,086	0,330
	2.	25	174,55	0,044	7,42	58,78	2,76	4,26	0,143	0,968
	3.	35	174,55	0,044	9,91	58,78	5,23	7,98	0,201	1,814
	4.	45	174,55	0,044	12,03	58,78	7	10,34	0,258	2,350
	5.	60	174,55	0,044	14,66	58,78	10,20	14,30	0,344	3,250
	6.	70	174,55	0,044	14,04	58,78	12,67	16,03	0,401	3,643
	7.	85	174,55	0,044	19,81	58,78	15,97	20,91	0,487	4,752
	8.	100	174,55	0,044	15,85	58,78	16,61	21,11	0,573	4,798
	9.	120	174,55	0,044	16,73	58,78	21,07	25,17	0,687	5,720
	10.	140	174,55	0,044	17,65	58,78	23,29	26,98	0,802	6,132

### III. SAE 30

SAE 30, 0.8mm,  $\alpha = 15$  derajat

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-10 °C/cm	1.	10	29,902	0,043	0	58,78	0	0	0,334	0,000
	2.	15	29,902	0,043	0	58,78	0	0	0,502	0,000
	3.	21	29,902	0,043	14,82	58,78	2,74	4,73	0,702	1,100
	4.	27	29,902	0,043	15,16	58,78	3,90	6,26	0,903	1,456
	5.	40	29,902	0,043	19,67	58,78	5,82	9,04	1,338	2,102
	6.	50	29,902	0,043	22,26	58,78	7,79	11,01	1,672	2,561
	7.	65	29,902	0,043	23,14	58,78	10,26	13,57	2,174	3,156
	8.	85	29,902	0,043	23,57	58,78	10,86	14,39	2,843	3,347
	9.	110	29,902	0,043	32,38	58,78	14,73	20,67	3,679	4,807

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	15	29,902	0,043	0	58,78	0	0	0,502	0,000
	2.	30	29,902	0,043	4,62	58,78	1,53	2,39	1,003	0,556
	3.	40	29,902	0,043	7,44	58,78	3,69	4,93	1,338	1,147
	4.	55	29,902	0,043	10,82	58,78	7,49	10,19	1,839	2,370
	5.	65	29,902	0,043	9,83	58,78	8,41	10,85	2,174	2,523
	6.	85	29,902	0,043	10,03	58,78	10,58	12,93	2,843	3,007
	7.	100	29,902	0,043	10,15	58,78	13,71	16,21	3,344	3,770
	8.	135	29,902	0,043	15,18	58,78	16,47	18,71	4,515	4,351
	9.	150	29,902	0,043	12,49	58,78	18,01	20,54	5,016	4,777
	10.	170	29,902	0,043	16,89	58,78	20,58	23,51	5,685	5,467

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-2.5 °C/cm	1.	25	29,902	0,043	0	58,78	0	0	0,836	0,000
	2.	55	29,902	0,043	2,89	58,78	4,36	5,1	1,839	1,186
	3.	90	29,902	0,043	6,68	58,78	7,77	9,59	3,010	2,230
	4.	105	29,902	0,043	5,47	58,78	9,25	11,78	3,511	2,740
	5.	145	29,902	0,043	6,27	58,78	15,57	18,02	4,849	4,191
	6.	165	29,902	0,043	4,63	58,78	17,26	20,03	5,518	4,658
	7.	210	29,902	0,043	6,95	58,78	22,41	24,78	7,023	5,763
	8.	245	29,902	0,043	10,8	58,78	28,07	31,11	8,193	7,235
	9.	270	29,902	0,043	13,73	58,78	31,97	36,56	9,029	8,502
	10.	300	29,902	0,043	9,87	58,78	32,86	36,74	10,033	8,544

**SAE 30, 0.8mm,  $\alpha = 45$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	10	10,945	0,016	0	58,78	0	0	0,914	0,000
	2.	15	10,945	0,016	3,72	58,78	6,24	7,27	1,370	4,544
	3.	20	10,945	0,016	4,44	58,78	11,17	12,34	1,827	7,713
	4.	26	10,945	0,016	6,55	58,78	16,52	17,83	2,376	11,144
	5.	40	10,945	0,016	10,23	58,78	23,44	25,21	3,655	15,756
	6.	50	10,945	0,016	14,34	58,78	27,26	29,92	4,568	18,700
	7.	60	10,945	0,016	13,42	58,78	30,08	32,17	5,482	20,106

**SAE 30, b = 0.8mm,  $\alpha = 75$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	4	8,012	0,012	0	58,78	0	0	0,499	0,000
	2.	6	8,012	0,012	16,63	58,78	2,31	3,98	0,749	3,317
	3.	7	8,012	0,012	15,80	58,78	3,68	5,68	0,874	4,733
	4.	9	8,012	0,012	15,36	58,78	5,64	9,09	1,123	7,575
	5.	10	8,012	0,012	16,44	58,78	7,95	11,34	1,248	9,450
	6.	12	8,012	0,012	16,42	58,78	11,09	15,34	1,498	12,783
	7.	13	8,012	0,012	14,11	58,78	13,44	17,01	1,623	14,175
	8.	17	8,012	0,012	18,58	58,78	18,05	21,44	2,122	17,867
	9.	20	8,012	0,012	22,09	58,78	21,09	24,70	2,496	20,583
	10.	25	8,012	0,012	24,88	58,78	22,16	26,27	3,120	21,892

**SAE 30, b = 1.2mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
-4 °C/cm	1.	4	19,935	0,043	0	58,78	0	0	0,201	0,000
	2.	8	19,935	0,043	0	58,78	0	0	0,401	0,000
	3.	20	19,935	0,043	9,26	58,78	2,78	3,61	1,003	0,840
	4.	30	19,935	0,043	7,73	58,78	3,82	5,33	1,505	1,240
	5.	40	19,935	0,043	9,27	58,78	7,56	9,54	2,007	2,219
	6.	50	19,935	0,043	12,87	58,78	8,23	13,09	2,508	3,044
	7.	56	19,935	0,043	9,12	58,78	12,88	15,85	2,809	3,686
	8.	65	19,935	0,043	9,06	58,78	15,44	19,49	3,261	4,533
	9.	75	19,935	0,043	11,15	58,78	18,81	22,88	3,762	5,321
	10.	90	19,935	0,043	11,82	58,78	19,74	22,33	4,515	5,193



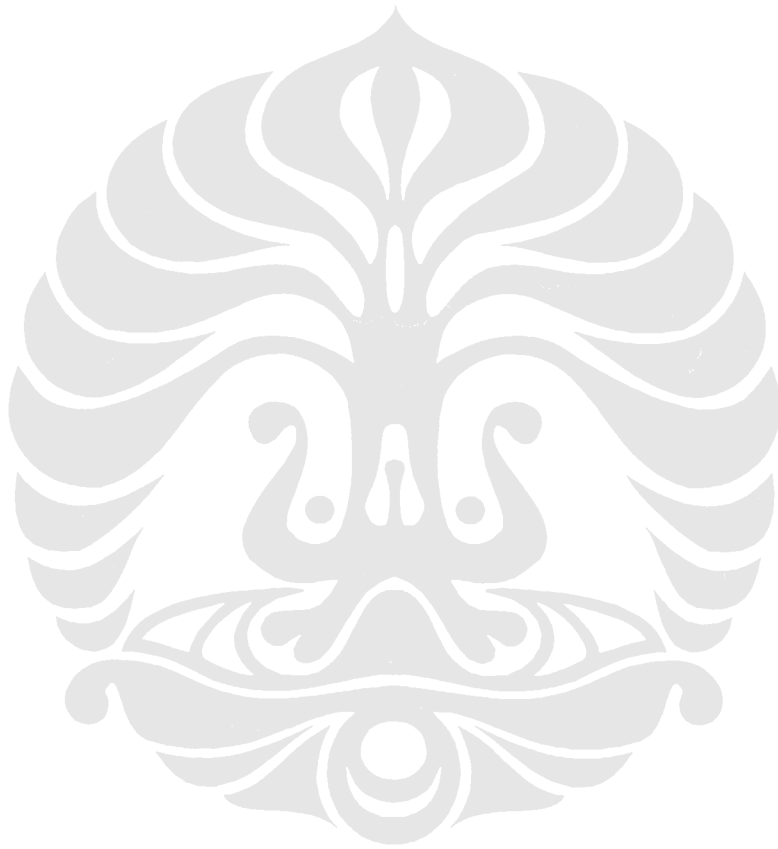
**SAE 30, b = 1.5mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
-4 °C/cm	1.	13	15,948	0,043	4,92	58,78	2,03	4,58	0,815	1,065
	2.	18	15,948	0,043	9,94	58,78	3,15	6,75	1,129	1,570
	3.	20	15,948	0,043	10,01	58,78	4,70	8,28	1,254	1,926
	4.	24	15,948	0,043	10,20	58,78	7,20	11,02	1,505	2,563
	5.	26	15,948	0,043	10,72	58,78	9,42	13,23	1,630	3,077
	6.	29	15,948	0,043	16,62	58,78	10,67	15,43	1,818	3,588
	7.	32	15,948	0,043	10,07	58,78	12,95	16,97	2,007	3,947
	8.	37	15,948	0,043	11,06	58,78	15,63	20,23	2,320	4,705
	9.	45	15,948	0,043	13,59	58,78	18,79	23,12	2,822	5,377
	10.	60	15,948	0,043	17,68	58,78	24,69	29,47	3,762	6,853



**LAMPIRAN 4**

**Tabel data perubahan bentuk tiap satuan waktu  $dT/dx \geq 0$**



## I. Glycerin

glycerin,  $b = 0.8 \text{ mm}$ ,  $\alpha = 15 \text{ derajat}$

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
10 °C/cm	1.	27	425,59	0,048	0	58,78	0	0	0,063	0,000
	2.	33	425,59	0,048	2,51	58,78	1,37	2,60	0,078	0,542
	3.	38	425,59	0,048	3,25	58,78	2,87	4,91	0,089	1,023
	4.	43	425,59	0,048	5,88	58,78	3,65	6,54	0,101	1,363
	5.	53	425,59	0,048	9,45	58,78	5,32	8,37	0,125	1,744
	6.	63	425,59	0,048	11,9	58,78	6,83	9,69	0,148	2,019
	7.	78	425,59	0,048	15,83	58,78	8,64	11,84	0,183	2,467
	8.	93	425,59	0,048	18,84	58,78	9,85	13,99	0,219	2,915
	9.	108	425,59	0,048	24,58	58,78	12,05	17,23	0,254	3,590
	10.	123	425,59	0,048	26,17	58,78	12,54	18,25	0,289	3,802

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	32	425,59	0,048	0	58,78	0	0	0,075	0,000
	2.	51	425,59	0,048	2,18	58,78	2,29	3,14	0,120	0,654
	3.	75	425,59	0,048	5,63	58,78	2,86	5,27	0,176	1,098
	4.	91	425,59	0,048	7,25	58,78	3,75	8,35	0,214	1,740
	5.	106	425,59	0,048	6,96	58,78	7,17	13,75	0,249	2,865
	6.	121	425,59	0,048	6,97	58,78	7,07	14,57	0,284	3,035
	7.	140	425,59	0,048	7,79	58,78	8,59	19,28	0,329	4,017
	8.	160	425,59	0,048	7,35	58,78	12,36	22,69	0,376	4,727
	9.	200	425,59	0,048	10,72	58,78	21,16	25,93	0,470	5,402
	10.	220	425,59	0,048	13,33	58,78	22,27	27,94	0,517	5,821

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
2.5 °C/cm	1.	7	425,59	0,048	0	58,78	0	0	0,016	0,000
	2.	16	425,59	0,048	0	58,78	0	0	0,038	0,000
	3.	46	425,59	0,048	1,99	58,78	4,76	5,66	0,108	1,179
	4.	72	425,59	0,048	6,75	58,78	4,86	8,35	0,169	1,740
	5.	115	425,59	0,048	4	58,78	8,94	13,03	0,270	2,715
	6.	133	425,59	0,048	4,09	58,78	12,28	19,4	0,313	4,042
	7.	168	425,59	0,048	3,87	58,78	16,74	26,07	0,395	5,431
	8.	183	425,59	0,048	3,62	58,78	19,01	30,32	0,430	6,317
	9.	200	425,59	0,048	3,87	58,78	23,32	35,70	0,470	7,438
	10.	225	425,59	0,048	4,59	58,78	24,43	36,49	0,529	7,602

**glycerin, b = 0.8 mm,  $\alpha = 45$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	10	155,777	0,018	0	58,78	0	0	0,064	0,000
	2.	15	155,777	0,018	5,47	58,78	1,34	2,54	0,096	1,411
	3.	20	155,777	0,018	4,29	58,78	3,71	5,17	0,128	2,872
	4.	23	155,777	0,018	5,82	58,78	4,41	6,95	0,148	3,861
	5.	26	155,777	0,018	5,41	58,78	6,02	9,66	0,167	5,367
	6.	28	155,777	0,018	6,23	58,78	7,84	12,48	0,180	6,933
	7.	31	155,777	0,018	5,14	58,78	10,22	15,33	0,199	8,517
	8.	35	155,777	0,018	3,93	58,78	13,76	19,14	0,225	10,633
	9.	40	155,777	0,018	9,09	58,78	21,47	26,65	0,257	14,806

**glycerin, b = 0.8 mm,  $\alpha = 75$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	5	114,036	0,013	0	58,78	0	0	0,044	0,000
	2.	10	114,036	0,013	0	58,78	0	0	0,088	0,000
	3.	12	114,036	0,013	0	58,78	0	0	0,105	0,000
	4.	17	114,036	0,013	4,09	58,78	2,83	3,87	0,149	2,977
	5.	19	114,036	0,013	5,35	58,78	3,81	6,15	0,167	4,731
	6.	21	114,036	0,013	7,85	58,78	4,81	8,91	0,184	6,854
	7.	22	114,036	0,013	4,73	58,78	5,72	9,41	0,193	7,238
	8.	24	114,036	0,013	4,32	58,78	10,64	15,52	0,210	11,938
	9.	30	114,036	0,013	7,35	58,78	16,61	21,98	0,263	16,908
	10.	35	114,036	0,013	14,05	58,78	21,15	26,5	0,307	20,385

**glycerin, b = 1.2 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	20	283,727	0,048	8,76	58,78	2,2	3,03	0,070	0,631
	2.	30	283,727	0,048	8,43	58,78	3,52	4,85	0,106	1,010
	3.	45	283,727	0,048	5,69	58,78	4,28	7,03	0,159	1,465
	4.	6	283,727	0,048	6,69	58,78	5,59	9,89	0,021	2,060
	5.	70	283,727	0,048	8,72	58,78	7	13,06	0,247	2,721
	6.	81	283,727	0,048	5,97	58,78	8,32	15,92	0,285	3,317
	7.	91	283,727	0,048	4,09	58,78	10,07	18,16	0,321	3,783
	8.	105	283,727	0,048	5,32	58,78	12,94	22,57	0,370	4,702
	9.	115	283,727	0,048	6,27	58,78	14,99	25,73	0,405	5,360
	10.	130	283,727	0,048	5,47	58,78	18,48	28,24	0,458	5,883

**glycerin, b = 1.5 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	4	226,981	0,048	0	58,78	0	0	0,018	0,000
	2.	8	226,981	0,048	0	58,78	0	0	0,035	0,000
	3.	17	226,981	0,048	0	58,78	0	0	0,075	0,000
	4.	26	226,981	0,048	7,06	58,78	2,02	4,57	0,115	0,952
	5.	30	226,981	0,048	5,49	58,78	4,16	7,47	0,132	1,556
	6.	34	226,981	0,048	7,27	58,78	5,11	12,35	0,150	2,573
	7.	38	226,981	0,048	6,27	58,78	5,66	14,58	0,167	3,038
	8.	46	226,981	0,048	6,99	58,78	7,56	21,66	0,203	4,513
	9.	55	226,981	0,048	6,49	58,78	12,45	27,05	0,242	5,635
	10.	65	226,981	0,048	8,44	58,78	17,85	33,53	0,286	6,985

**II. Castor oil**

**Castor oil, 0.8 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
10 °C/cm	1.	18	327,282	0,044	11,52	58,78	0,83	1,52	0,055	0,346
	2.	25	327,282	0,044	14,57	58,78	1,75	4,35	0,076	0,989
	3.	30	327,282	0,044	14,21	58,78	3,21	6,23	0,092	1,416
	4.	35	327,282	0,044	18,69	58,78	4,11	7,82	0,107	1,777
	5.	40	327,282	0,044	20,72	58,78	5,28	9,26	0,122	2,105
	6.	50	327,282	0,044	56,04	58,78	6,72	10,28	0,153	2,336
	7.	60	327,282	0,044	28,33	58,78	8,10	12,11	0,183	2,752
	8.	70	327,282	0,044	28,20	58,78	8,18	12,72	0,214	2,891
	9.	80	327,282	0,044	32,91	58,78	11,14	16,27	0,244	3,698

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	30	327,282	0,044	0	58,78	0	0	0,092	0,000
	2.	35	327,282	0,044	4,76	58,78	1,78	2,50	0,107	0,568
	3.	40	327,282	0,044	10,36	58,78	1,99	3,56	0,122	0,809
	4.	50	327,282	0,044	15,19	58,78	2,21	5,80	0,153	1,318
	5.	60	327,282	0,044	13,67	58,78	4,03	9,41	0,183	2,139
	6.	70	327,282	0,044	9,05	58,78	6,24	12,26	0,214	2,786
	7.	80	327,282	0,044	8,79	58,78	9,30	15,98	0,244	3,632
	8.	90	327,282	0,044	7,87	58,78	13,31	19,32	0,275	4,391
	9.	100	327,282	0,044	10,76	58,78	16,32	21,19	0,306	4,816
	10.	120	327,282	0,044	17,72	58,78	18,56	23,03	0,367	5,234

**Castor oil, b = 0.8 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
2.5 °C/cm	1.	30	327,282	0,044	12,45	58,78	1,19	2,46	0,092	0,559
	2.	45	327,282	0,044	14,04	58,78	2,03	4,26	0,137	0,968
	3.	60	327,282	0,044	17,44	58,78	2,36	6,44	0,183	1,464
	4.	80	327,282	0,044	16,85	58,78	3,01	10,16	0,244	2,309
	5.	100	327,282	0,044	15,54	58,78	6,87	14,26	0,306	3,241
	6.	120	327,282	0,044	16,75	58,78	8,63	19,64	0,367	4,464
	7.	140	327,282	0,044	13,66	58,78	11,52	23,59	0,428	5,361
	8.	160	327,282	0,044	13,75	58,78	13,7	25,79	0,489	5,861
	9.	180	327,282	0,044	13,84	58,78	16,02	28,02	0,550	6,368
	10.	195	327,282	0,044	15,86	58,78	21,06	33,90	0,596	7,705

**Castor oil, b = 0.8 mm,  $\alpha = 45$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
4 °C/cm	1.	10	119,794	0,026	0	58,78	0	0	0,083	0,000
	2.	14	119,794	0,026	4,53	58,78	1,40	2,65	0,117	1,019
	3.	17	119,794	0,026	4,33	58,78	2	4,33	0,142	1,665
	4.	20	119,794	0,026	4,36	58,78	4,14	6,92	0,167	2,662
	5.	25	119,794	0,026	4,61	58,78	7,17	11,5	0,209	4,423
	6.	30	119,794	0,026	6,56	58,78	12,13	17,72	0,250	6,815
	7.	35	119,794	0,026	11,84	58,78	14,95	19,49	0,292	7,496
	8.	40	119,794	0,026	18,21	58,78	17,89	23,03	0,334	8,858

**Castor oil, b = 0.8 mm,  $\alpha = 75$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
4 °C/cm	1.	7	87,695	0,019	0	58,78	0	0	0,080	0,000
	2.	9	87,695	0,019	0	58,78	0	0	0,103	0,000
	3.	12	87,695	0,019	4,42	58,78	2,39	3,55	0,137	1,868
	4.	14	87,695	0,019	5,45	58,78	3,79	5,75	0,160	3,026
	5.	16	87,695	0,019	3,82	58,78	6,29	8,42	0,182	4,432
	6.	18	87,695	0,019	4,83	58,78	10,56	13,95	0,205	7,342
	7.	20	87,695	0,019	4,43	58,78	12,48	15,23	0,228	8,016
	8.	25	87,695	0,019	10,68	58,78	18,15	20,95	0,285	11,026
	9.	30	87,695	0,019	16,8	58,78	20,29	23,5	0,342	12,368

**Castor oil, b = 1.2 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
4 °C/cm	1.	20	218,188	0,044	0	58,78	0	0	0,092	0,000
	2.	45	218,188	0,044	3,14	58,78	2,99	3,57	0,206	0,811
	3.	55	218,188	0,044	10,94	58,78	3,78	5,62	0,252	1,277
	4.	65	218,188	0,044	8,53	58,78	6,24	8,49	0,298	1,930
	5.	75	218,188	0,044	9,77	58,78	8,31	12,33	0,344	2,802
	6.	85	218,188	0,044	7,32	58,78	11,72	14,8	0,390	3,364
	7.	95	218,188	0,044	7,01	58,78	14,48	17,17	0,435	3,902
	8.	115	218,188	0,044	13,41	58,78	19,72	22,59	0,527	5,134
	9.	130	218,188	0,044	15,38	58,78	23,70	25,83	0,596	5,870
	10.	150	218,188	0,044	27	58,78	24,58	27,66	0,687	6,286

**Castor oil, b = 1.5 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
4 °C/cm	1.	35	174,55	0,044	9,84	58,78	2,04	3	0,201	0,682
	2.	45	174,55	0,044	7,52	58,78	3,48	4,97	0,258	1,130
	3.	55	174,55	0,044	10,38	58,78	5,41	8,6	0,315	1,955
	4.	60	174,55	0,044	7,14	58,78	8,16	12,44	0,344	2,827
	5.	63	174,55	0,044	6,73	58,78	8,50	12,66	0,361	2,877
	6.	70	174,55	0,044	5,79	58,78	12,52	16,21	0,401	3,684
	7.	80	174,55	0,044	8,36	58,78	16,93	19,24	0,458	4,373
	8.	100	174,55	0,044	14,35	58,78	20,37	24,10	0,573	5,477
	9.	120	174,55	0,044	20,48	58,78	24,26	27,61	0,687	6,275
	10.	135	174,55	0,044	20,25	58,78	24,19	27,41	0,773	6,230

**III. SAE 30**

**SAE 30, b = 0.8 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$\ell^*$	$\sum \ell_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/\ell^*$
10 °C/cm	1.	7	29,902	0,043	0	58,78	0	0	0,234	0,000
	2.	13	29,902	0,043	0	58,78	0	0	0,435	0,000
	3.	20	29,902	0,043	2,54	58,78	1,09	2,43	0,669	0,552
	4.	25	29,902	0,043	3,16	58,78	2,11	3,85	0,836	0,875
	5.	31	29,902	0,043	4,08	58,78	2,88	5,82	1,037	1,323
	6.	40	29,902	0,043	9,02	58,78	4,79	9,51	1,338	2,161
	7.	45	29,902	0,043	10,02	58,78	5,59	10,10	1,505	2,296
	8.	60	29,902	0,043	16,20	58,78	8,36	13,41	2,007	3,048
	9.	80	29,902	0,043	19,53	58,78	10,12	24	2,675	5,455
	10.	100	29,902	0,043	22,48	58,78	13,09	18,31	3,344	4,161

**SAE 30, b = 0.8 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	5	29,902	0,043	0	58,78	0	0	0,167	0,000
	2.	15	29,902	0,043	0	58,78	0	0	0,502	0,000
	3.	28	29,902	0,043	0	58,78	0	0	0,936	0,000
	4.	50	29,902	0,043	6,77	58,78	2,60	4,34	1,672	0,986
	5.	60	29,902	0,043	6,35	58,78	3,88	6,86	2,007	1,559
	6.	77	29,902	0,043	7,43	58,78	4,89	10,17	2,575	2,311
	7.	85	29,902	0,043	8,09	58,78	5,33	10,99	2,843	2,498
	8.	100	29,902	0,043	6,77	58,78	7,96	15,14	3,344	3,441
	9.	120	29,902	0,043	8,22	58,78	11,08	18,21	4,013	4,139
	10.	140	29,902	0,043	8,94	58,78	14,94	21,34	4,682	4,850

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
2.5 °C/cm	1.	30	29,902	0,043	0	58,78	0	0	1,003	0,000
	2.	65	29,902	0,043	8,61	58,78	3,02	5,97	2,174	1,357
	3.	105	29,902	0,043	12,66	58,78	6,94	10,28	3,511	2,336
	4.	145	29,902	0,043	13,20	58,78	8,49	13,96	4,849	3,173
	5.	175	29,902	0,043	9,98	58,78	10,44	16,49	5,852	3,748
	6.	195	29,902	0,043	9,41	58,78	12,95	20,63	6,521	4,689
	7.	215	29,902	0,043	8,19	58,78	16,10	26,19	7,190	5,952
	8.	230	29,902	0,043	6,84	58,78	22,01	30,15	7,692	6,852
	9.	255	29,902	0,043	6,66	58,78	29,96	33,64	8,528	7,646

**SAE 30, b = 0.8 mm,  $\alpha = 45$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	10	10,945	0,016	2,42	58,78	1,45	1,89	0,914	1,181
	2.	15	10,945	0,016	4,29	58,78	2,46	4,59	1,370	2,869
	3.	17	10,945	0,016	4,68	58,78	3,93	6,38	1,553	3,988
	4.	21	10,945	0,016	6,36	58,78	6,25	10,09	1,919	6,306
	5.	23	10,945	0,016	4,72	58,78	7,89	11,38	2,101	7,113
	6.	26	10,945	0,016	7,63	58,78	9,43	15,93	2,376	9,956
	7.	27	10,945	0,016	5,31	58,78	10,88	16,14	2,467	10,088
	8.	30	10,945	0,016	2,60	58,78	13,95	19,59	2,741	12,244
	9.	35	10,945	0,016	3,07	58,78	19,93	23,79	3,198	14,869



**SAE 30, b = 0.8 mm,  $\alpha = 75$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	6	8,012	0,012	0	58,78	0	0	0,749	0,000
	2.	9	8,012	0,012	10,23	58,78	3,14	4,63	1,123	3,858
	3.	11	8,012	0,012	6,88	58,78	5,27	7,16	1,373	5,967
	4.	13	8,012	0,012	12,85	58,78	6,83	9,89	1,623	8,242
	5.	15	8,012	0,012	9,54	58,78	8,71	12,90	1,872	10,750
	6.	16	8,012	0,012	13,76	58,78	9,71	14,52	1,997	12,100
	7.	18	8,012	0,012	8,31	58,78	13,62	18,88	2,247	15,733
	8.	19	8,012	0,012	4,96	58,78	17,91	21,17	2,371	17,642
	9.	21	8,012	0,012	5,55	58,78	20,74	23,17	2,621	19,308
	10.	25	8,012	0,012	7,31	58,78	25,95	28,59	3,120	23,825

**SAE 30, b = 1.2 mm,  $\alpha = 15$  derajat**

dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	35	19,935	0,043	10,23	58,78	1,34	2,52	1,756	0,586
	2.	42	19,935	0,043	7,84	58,78	2,09	4,61	2,107	1,072
	3.	50	19,935	0,043	8,48	58,78	5,74	7,62	2,508	1,772
	4.	56	19,935	0,043	7,81	58,78	6,69	9,01	2,809	2,095
	5.	64	19,935	0,043	10,78	58,78	11,06	14,03	3,210	3,263
	6.	72	19,935	0,043	10,93	58,78	12,43	15,38	3,612	3,577
	7.	82	19,935	0,043	11,82	58,78	15,72	18,72	4,113	4,353
	8.	92	19,935	0,043	12,68	58,78	17,06	20,43	4,615	4,751
	9.	100	19,935	0,043	14,14	58,78	19,83	23,38	5,016	5,437
	10.	120	19,935	0,043	16,48	58,78	22,92	27,24	6,020	6,335

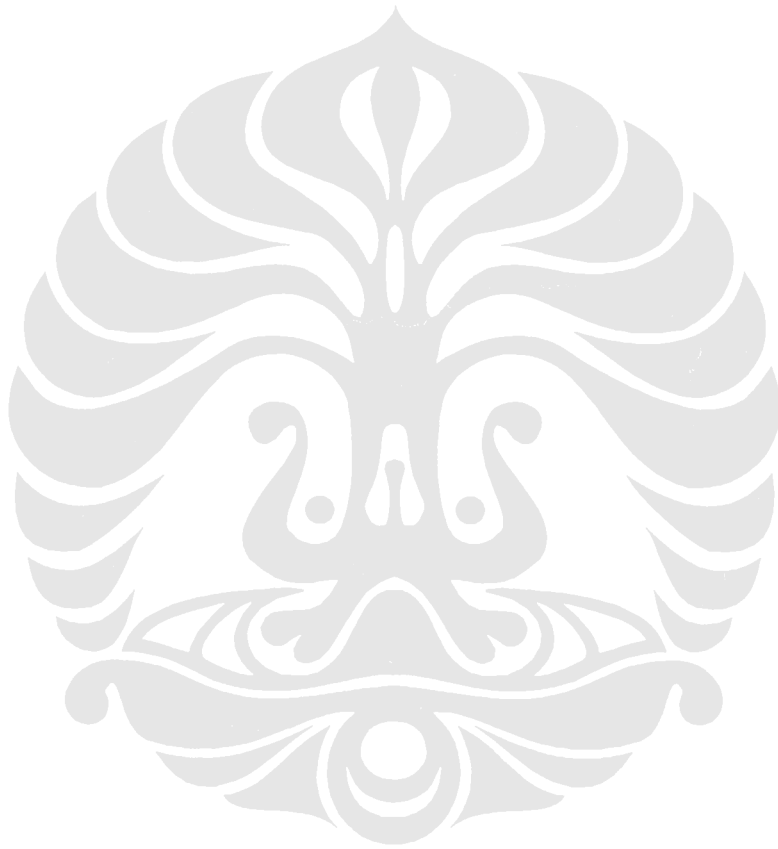
**SAE 30, b = 1.5 mm,  $\alpha = 15$  derajat**

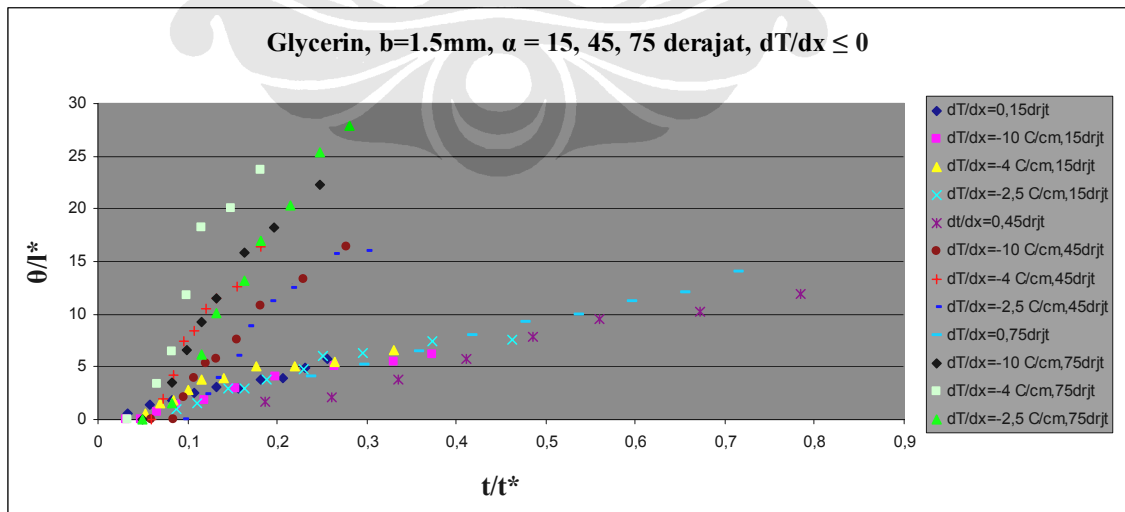
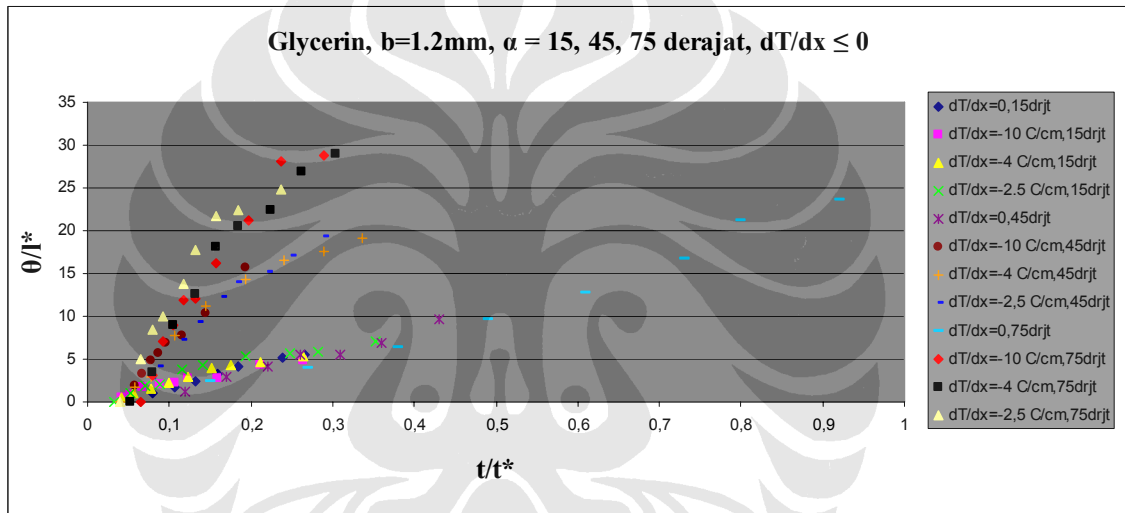
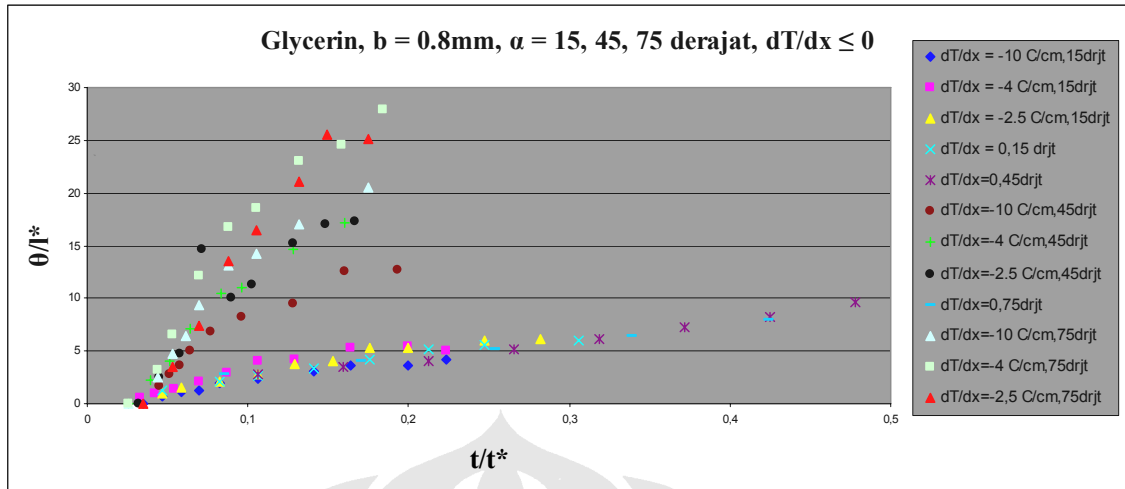
dT/dx	No.	t	t*	$l^*$	$\sum l_i$	W	y	$\hat{\theta}$	t/t*	$\hat{\theta}/l^*$
4 °C/cm	1.	17	15,948	0,043	20,71	58,78	3,51	5,37	1,066	1,249
	2.	23	15,948	0,043	17,10	58,78	5,94	8,26	1,442	1,921
	3.	28	15,948	0,043	15,92	58,78	7,83	11,57	1,756	2,691
	4.	31	15,948	0,043	13,39	58,78	8,06	12,56	1,944	2,921
	5.	35	15,948	0,043	13,21	58,78	11,09	16,43	2,195	3,821
	6.	37	15,948	0,043	8,80	58,78	13,09	17,93	2,320	4,170
	7.	41	15,948	0,043	7,29	58,78	16,47	21,64	2,571	5,033
	8.	45	15,948	0,043	6,51	58,78	18,76	23,85	2,822	5,547
	9.	50	15,948	0,043	12,05	58,78	22,96	28,01	3,135	6,514
	10.	60	15,948	0,043	15,51	58,78	25,44	29,57	3,762	6,877

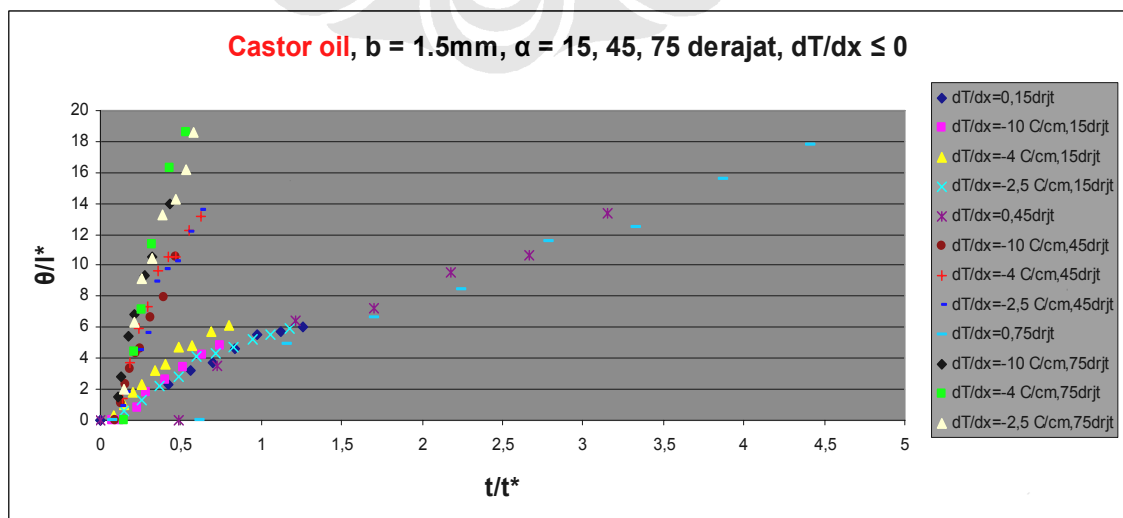
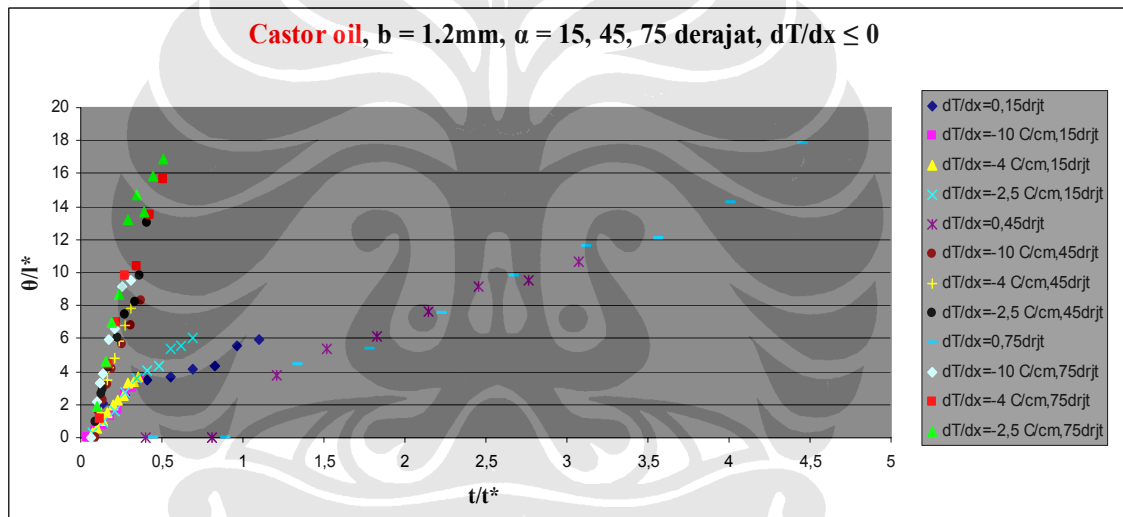
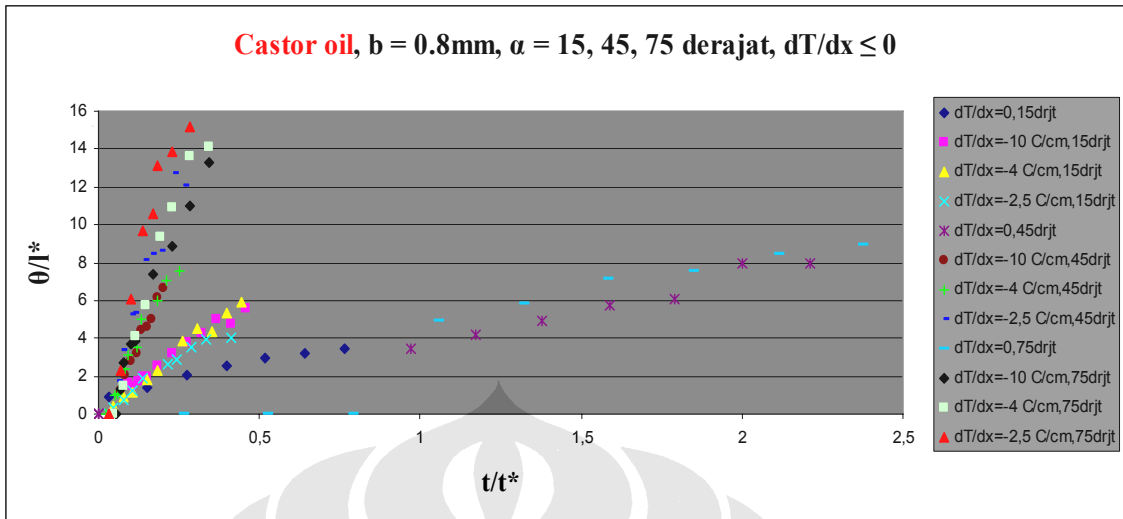
## LAMPIRAN 5

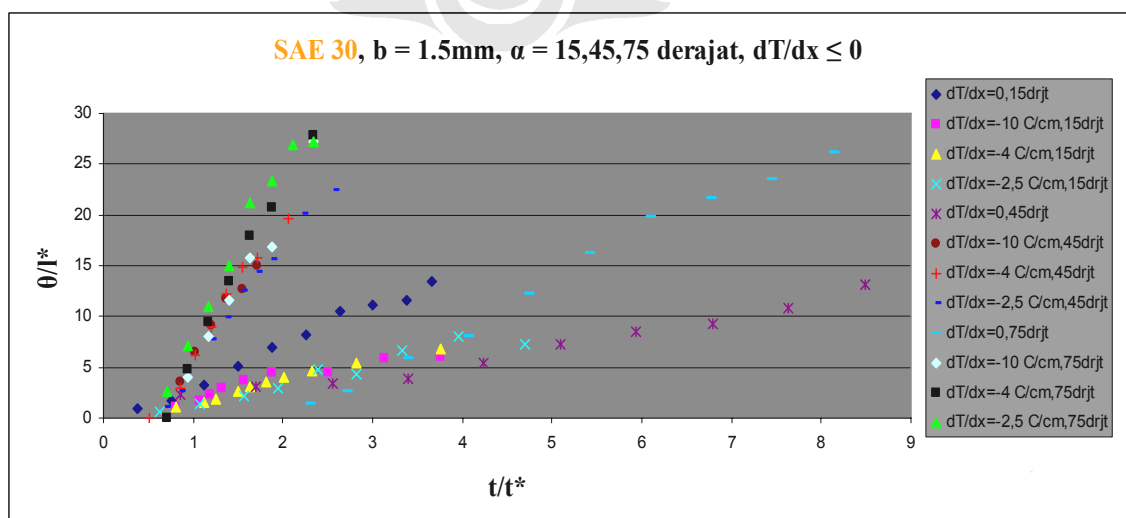
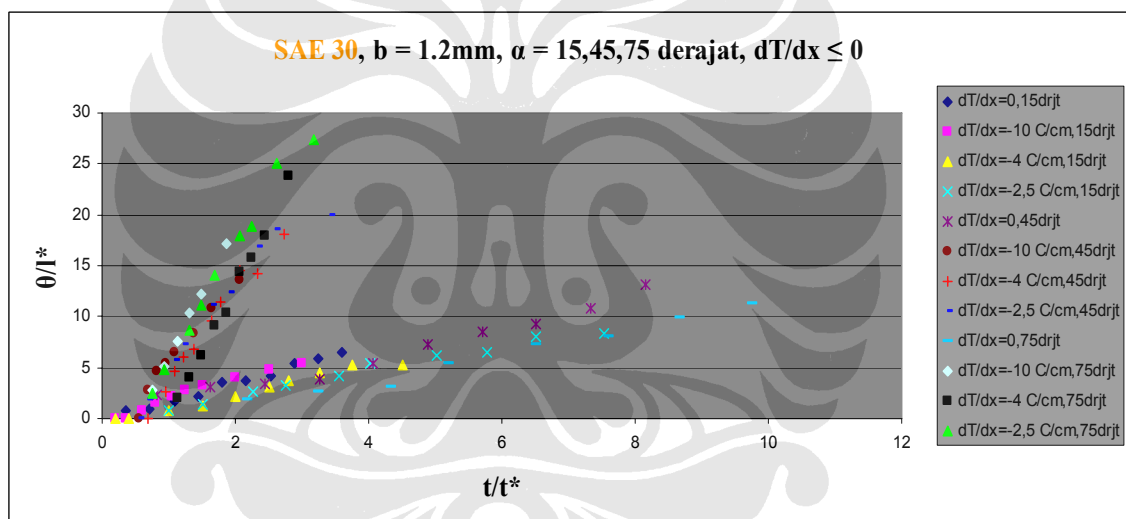
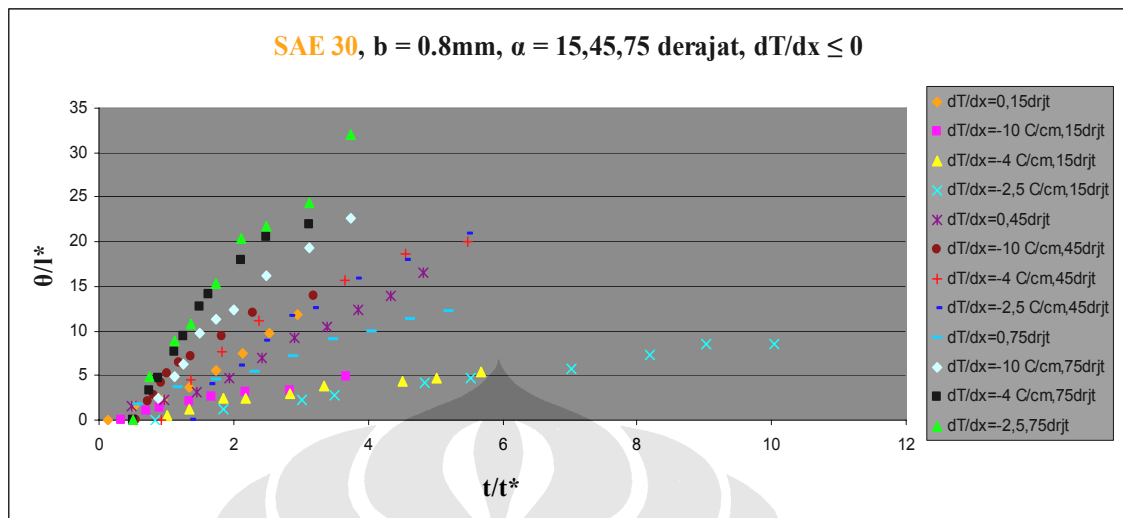
**Grafik hubungan antara skala panjang ( $\Theta/l^*$ ) dan skala waktu ( $t/t^*$ )**

$$dT/dx \leq 0$$









## LAMPIRAN 6

**Grafik hubungan antara skala panjang ( $\Theta/l^*$ ) dan skala waktu ( $t/t^*$ )**

$$dT/dx \geq 0$$

