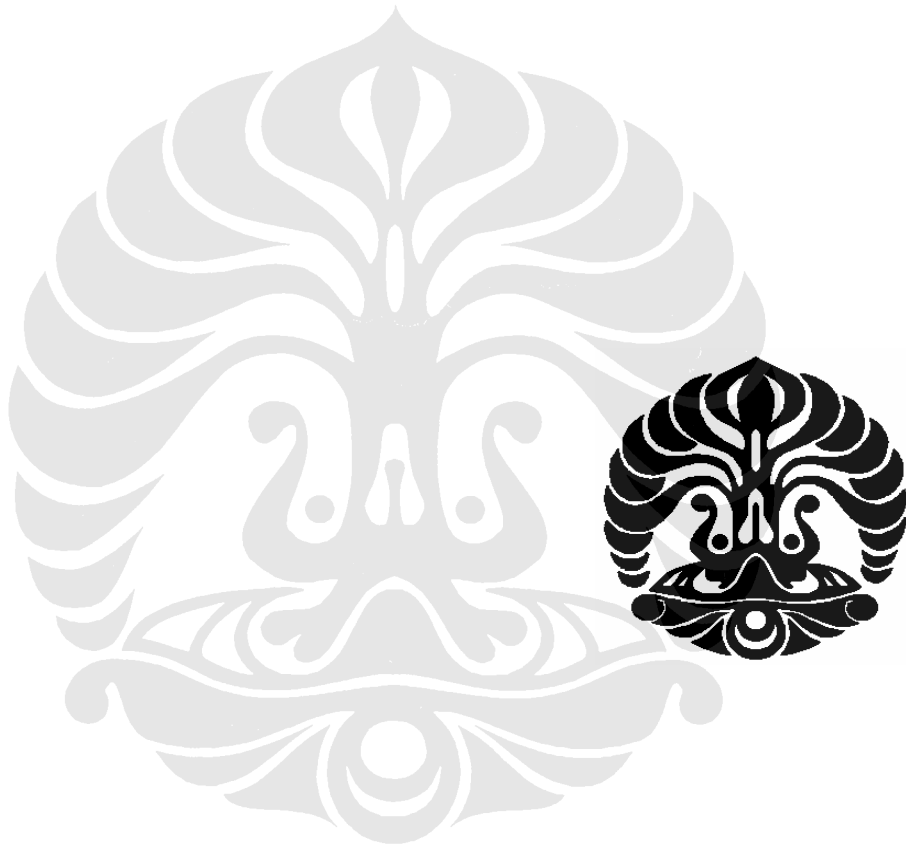


LAMPIRAN A1

Perhitungan Struktur Atap Rumah Tinggal Dengan Program SAP 2000



Beban Mati**Gording** 0.05 kN/m²

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.017	0.034	0.034	0.017
Gording 2	0.011	0.021	0.021	0.011
Gording 3	0.011	0.021	0.021	0.011
Gording 4	0.011	0.021	0.021	0.011

Penutup Atap**Genteng tanah liat** 0.25 kN/m²

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.541	1.083	1.083	0.541
Gording 2	0.541	1.083	1.083	0.541
Gording 3	0.496	0.992	0.992	0.496
Gording 4	0.225	0.451	0.451	0.225

Beban Mati Total

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.558	1.117	1.117	0.558
Gording 2	0.552	1.104	1.104	0.552
Gording 3	0.507	1.013	1.013	0.507
Gording 4	0.236	0.472	0.472	0.236

Beban Hidup**Beban Pekerja** 1 kN/m²

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	1	1	1	1
Gording 2	1	1	1	1
Gording 3	1	1	1	1
Gording 4	0.5	0.5	0.5	0.5

Beban Angin kiri**Muka Angin** 0.25 kN/m² Koefisien 0.2

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.054	0.108	0.108	0.054
Gording 2	0.108	0.217	0.217	0.108
Gording 3	0.099	0.198	0.198	0.099
Gording 4	0.045	0.090	0.090	0.045

Angin belakang 0.25 kN/m² Koefisien 0.4

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.108	0.217	0.217	0.108
Gording 2	0.217	0.433	0.433	0.217
Gording 3	0.198	0.397	0.397	0.198
Gording 4	0.090	0.180	0.180	0.090

Beban Angin kanan

Muka Angin **0.25 kN/m²** **Koefisien** **0.2**

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.054	0.108	0.108	0.054
Gording 2	0.108	0.217	0.217	0.108
Gording 3	0.099	0.198	0.198	0.099
Gording 4	0.045	0.090	0.090	0.045

Angin belakang **0.25 kN/m²** **Koefisien** **0.4**

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.108	0.217	0.217	0.108
Gording 2	0.217	0.433	0.433	0.217
Gording 3	0.198	0.397	0.397	0.198
Gording 4	0.090	0.180	0.180	0.090

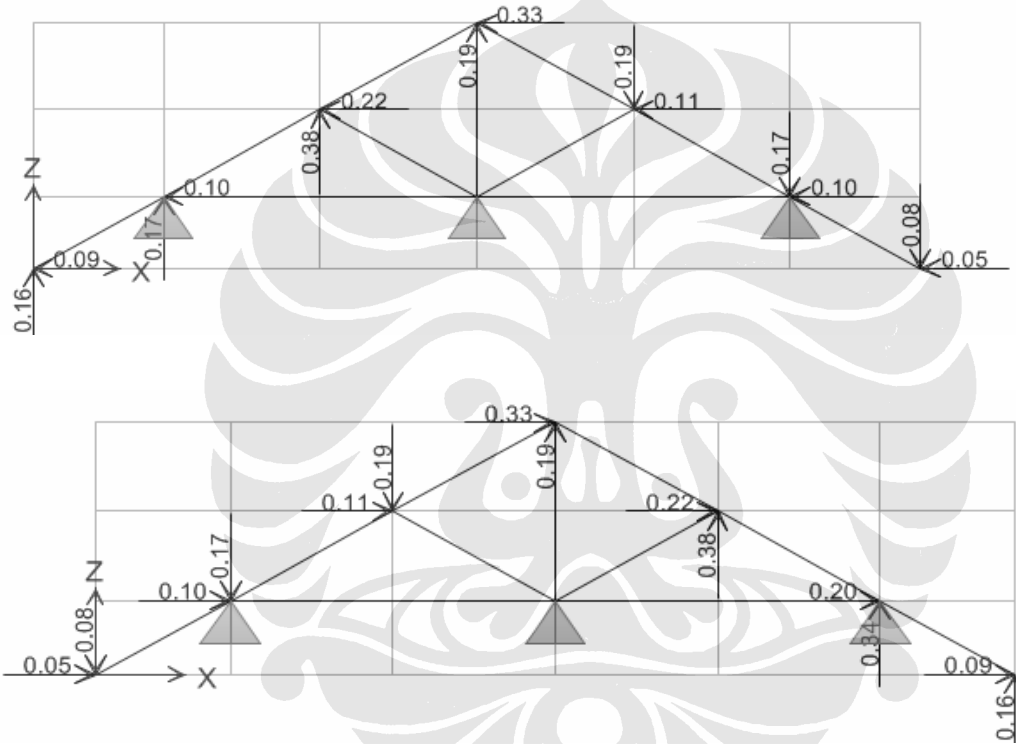


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	1.572
4	0	0	3.033
7	0	0	1.572

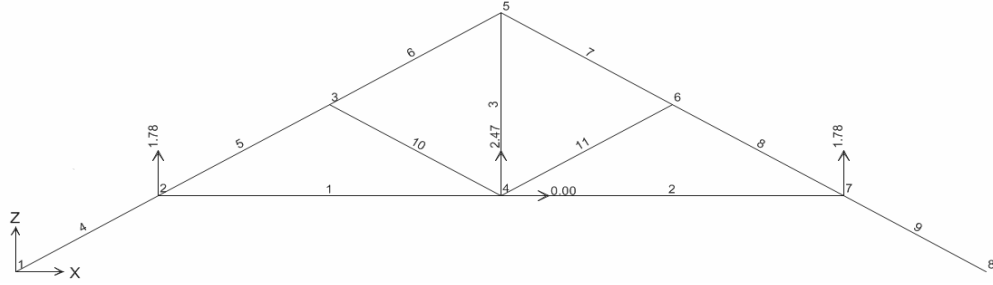


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	1.568
4	0	0	2.671
7	0	0	1.568

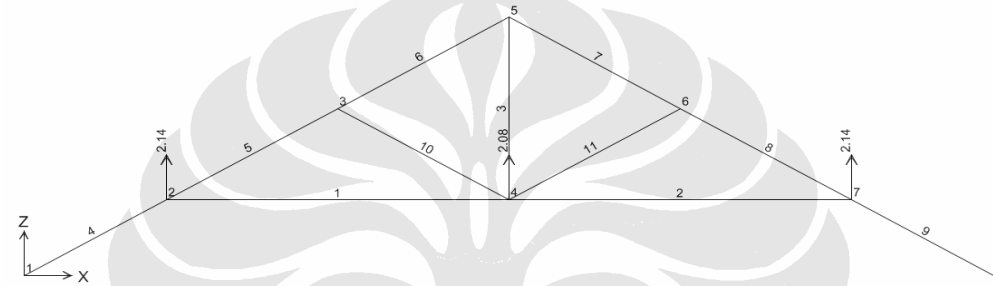


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	0.251
4	-0.607	0	-0.236
7	0	0	-0.615

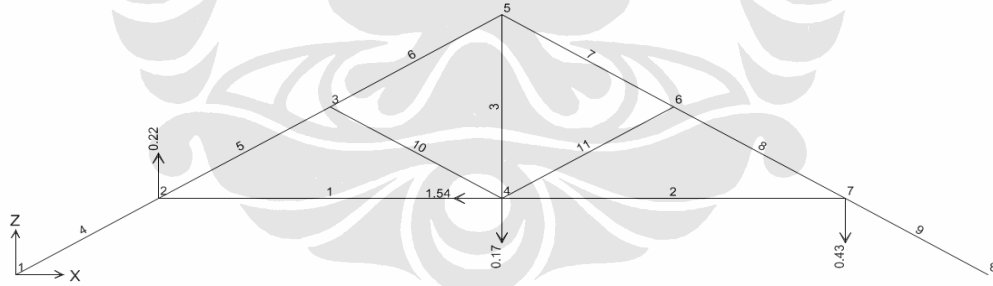
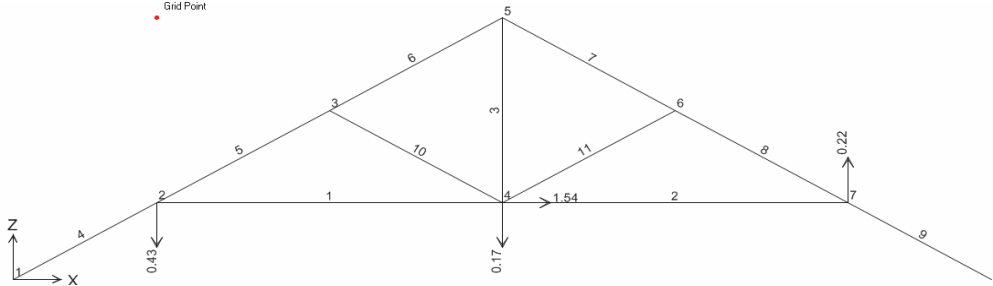


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	-0.615
4	0.607	0	-0.236
7	0	0	0.251

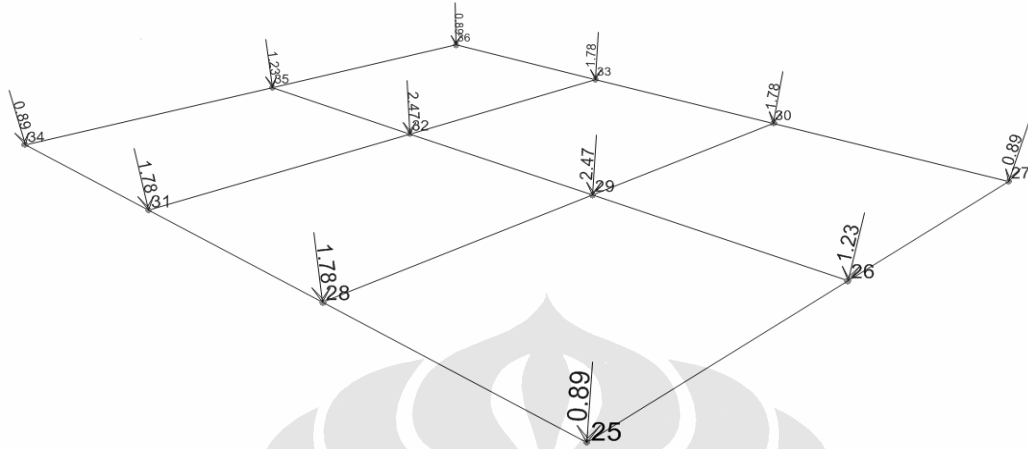


Beban Atap

Reaksi Perletakan Atap

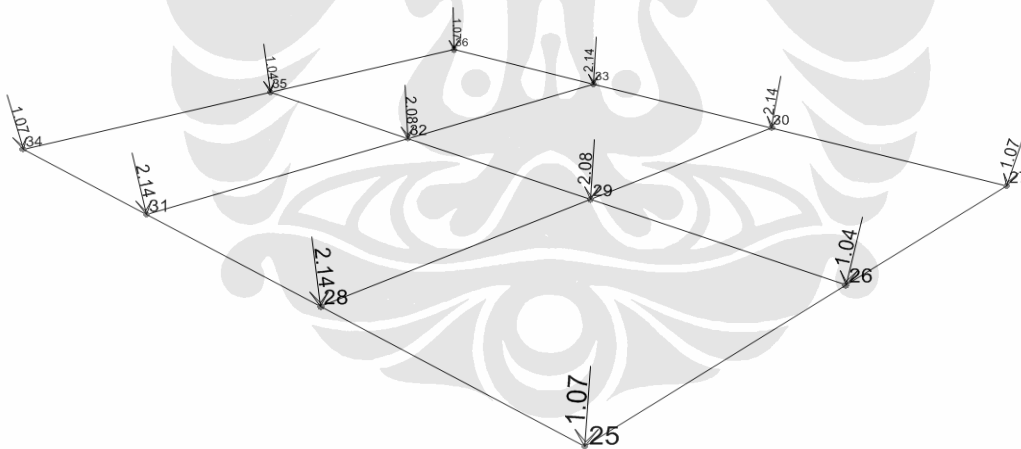
Beban Mati

	1	2	3	4
A	-0.786	-1.572	-1.572	-0.786
B	-1.517	-3.033	-3.033	-1.517
C	-0.786	-1.572	-1.572	-0.786



Beban Hidup

	1	2	3	4
A	-0.784	-1.568	-1.568	-0.784
B	-1.336	-2.671	-2.671	-1.336
C	-0.784	-1.568	-1.568	-0.784



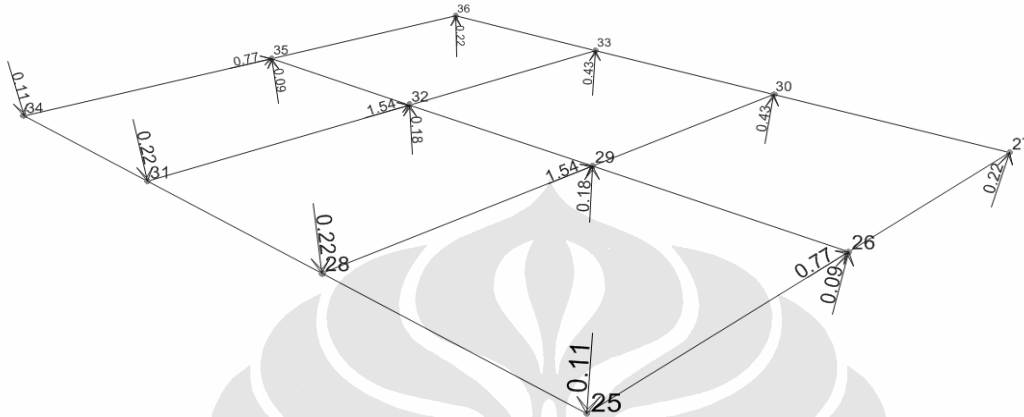
Beban Angin kanan

Arah Z

	1	2	3	4
A	-0.126	-0.251	-0.251	-0.126
B	0.118	0.236	0.236	0.118
C	0.308	0.615	0.615	0.308

Arah X

	1	2	3	4
A	0.000	0.000	0.000	0.000
B	0.304	0.607	0.607	0.304
C	0.000	0.000	0.000	0.000



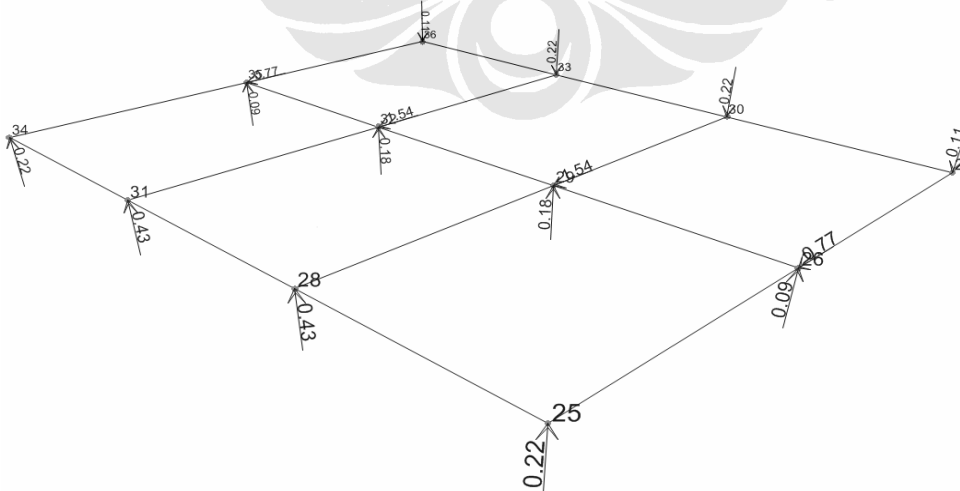
Beban Angin kiri

Arah Z

	1	2	3	4
A	0.308	0.615	0.615	0.308
B	0.118	0.236	0.236	0.118
C	-0.126	-0.251	-0.251	-0.126

Arah -X

	1	2	3	4
A	0.000	0.000	0.000	0.000
B	-0.304	-0.607	-0.607	-0.304
C	0.000	0.000	0.000	0.000



Beban Mati**Gording** 0.05 kN/m²

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.017	0.034	0.034	0.017
Gording 2	0.011	0.021	0.021	0.011
Gording 3	0.011	0.021	0.021	0.011
Gording 4	0.011	0.021	0.021	0.011

Penutup Atap**Genteng tanah liat** 0.25 kN/m²

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.541	1.083	1.083	0.541
Gording 2	0.541	1.083	1.083	0.541
Gording 3	0.496	0.992	0.992	0.496
Gording 4	0.225	0.451	0.451	0.225

Beban Mati Total

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.558	1.117	1.117	0.558
Gording 2	0.552	1.104	1.104	0.552
Gording 3	0.507	1.013	1.013	0.507
Gording 4	0.236	0.472	0.472	0.236

Beban Hidup**Beban Pekerja** 1 kN/m²

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	1	1	1	1
Gording 2	1	1	1	1
Gording 3	1	1	1	1
Gording 4	0.5	0.5	0.5	0.5

Beban Angin kiri**Muka Angin** 0.25 kN/m² Koefisien 0.2

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.054	0.108	0.108	0.054
Gording 2	0.108	0.217	0.217	0.108
Gording 3	0.099	0.198	0.198	0.099
Gording 4	0.045	0.090	0.090	0.045

Angin belakang 0.25 kN/m² Koefisien 0.4

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.108	0.217	0.217	0.108
Gording 2	0.217	0.433	0.433	0.217
Gording 3	0.198	0.397	0.397	0.198
Gording 4	0.090	0.180	0.180	0.090

Beban Angin kanan

Muka Angin **0.25 kN/m²** **Koefisien** **0.2**

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.054	0.108	0.108	0.054
Gording 2	0.108	0.217	0.217	0.108
Gording 3	0.099	0.198	0.198	0.099
Gording 4	0.045	0.090	0.090	0.045

Angin belakang **0.25 kN/m²** **Koefisien** **0.4**

	Rangka Sopi 1	Rangka Sopi 2	Rangka Sopi 3	Rangka Sopi 4
Gording 1	0.108	0.217	0.217	0.108
Gording 2	0.217	0.433	0.433	0.217
Gording 3	0.198	0.397	0.397	0.198
Gording 4	0.090	0.180	0.180	0.090

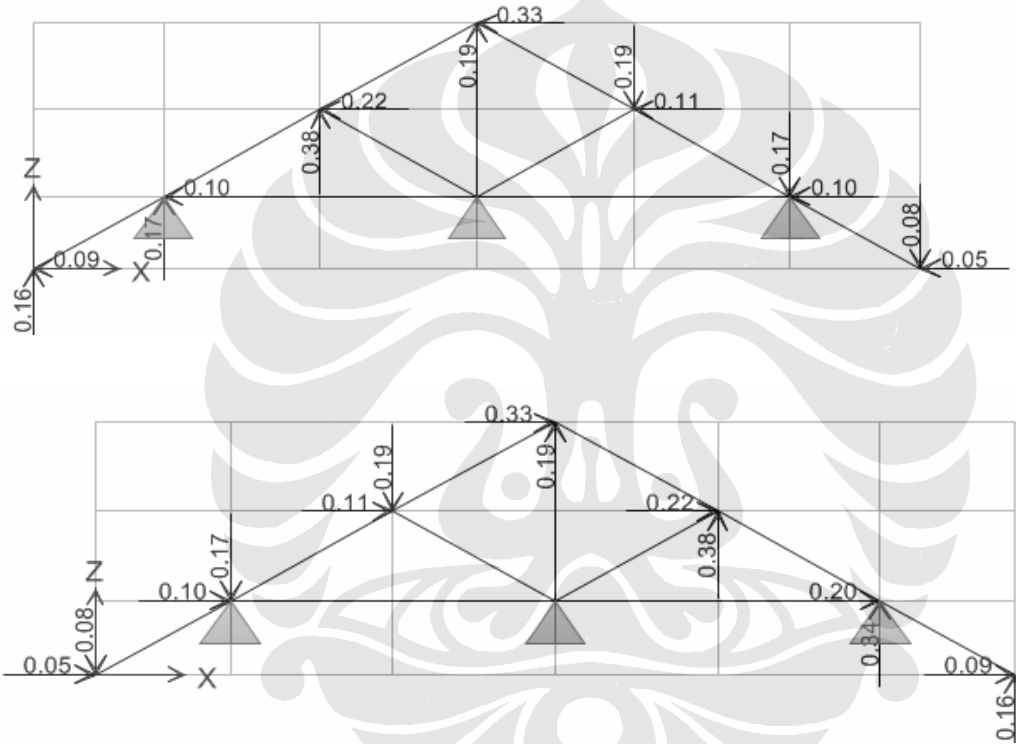


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	1.572
4	0	0	3.033
7	0	0	1.572

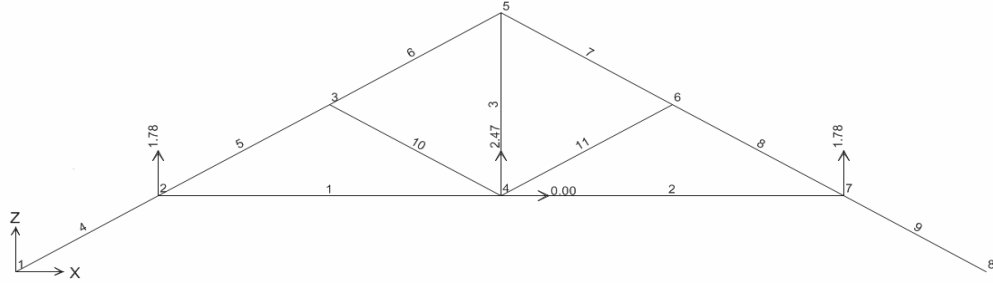


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	1.568
4	0	0	2.671
7	0	0	1.568

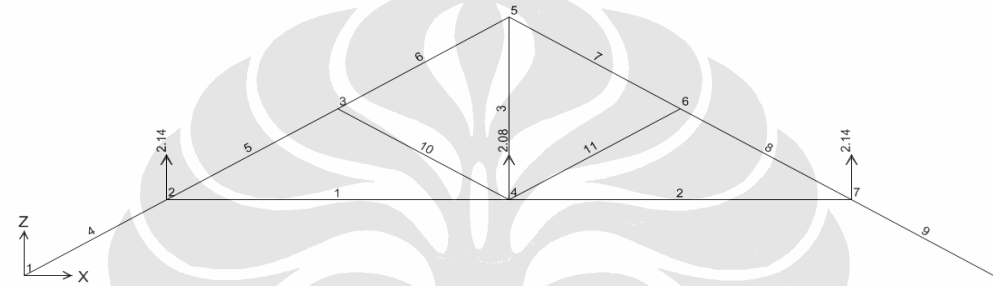


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	0.251
4	-0.607	0	-0.236
7	0	0	-0.615

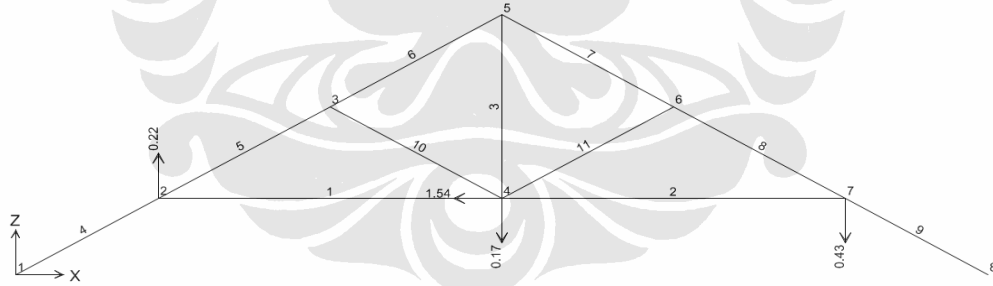
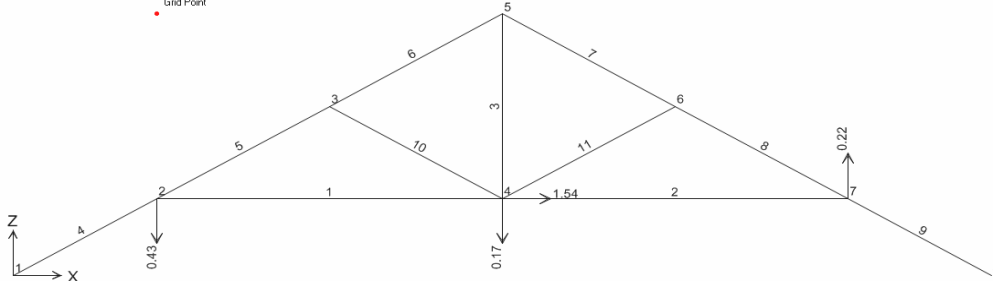


TABLE: Joint Reactions Gording 2

Joint Text	U1 KN	U2 KN	U3 KN
2	0	0	-0.615
4	0.607	0	-0.236
7	0	0	0.251

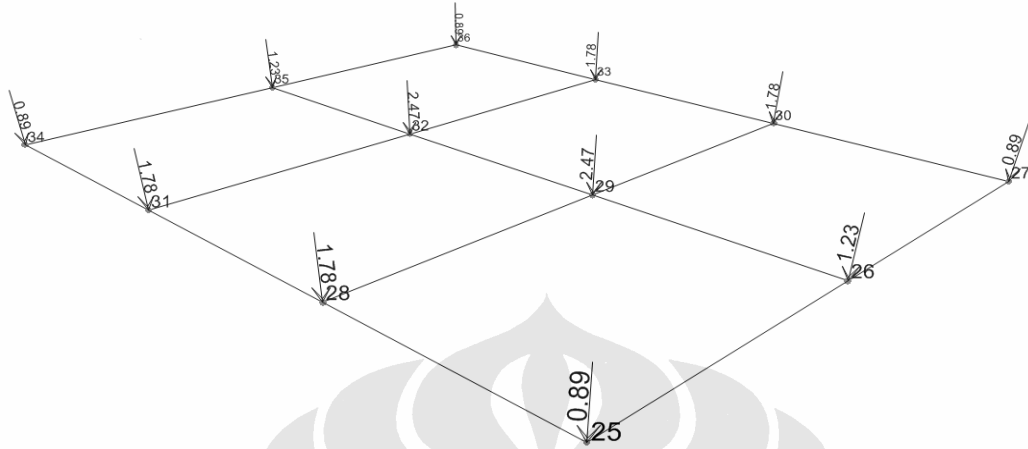


Beban Atap

Reaksi Perletakan Atap

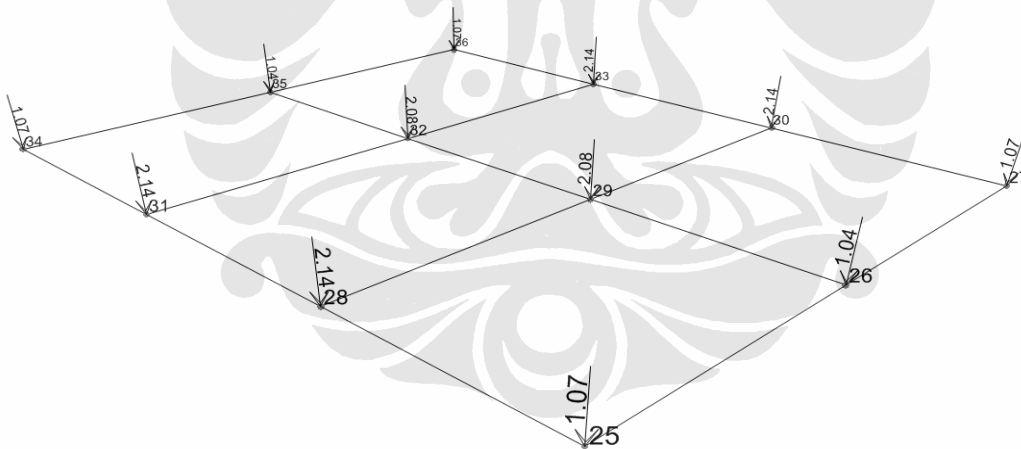
Beban Mati

	1	2	3	4
A	-0.786	-1.572	-1.572	-0.786
B	-1.517	-3.033	-3.033	-1.517
C	-0.786	-1.572	-1.572	-0.786



Beban Hidup

	1	2	3	4
A	-0.784	-1.568	-1.568	-0.784
B	-1.336	-2.671	-2.671	-1.336
C	-0.784	-1.568	-1.568	-0.784



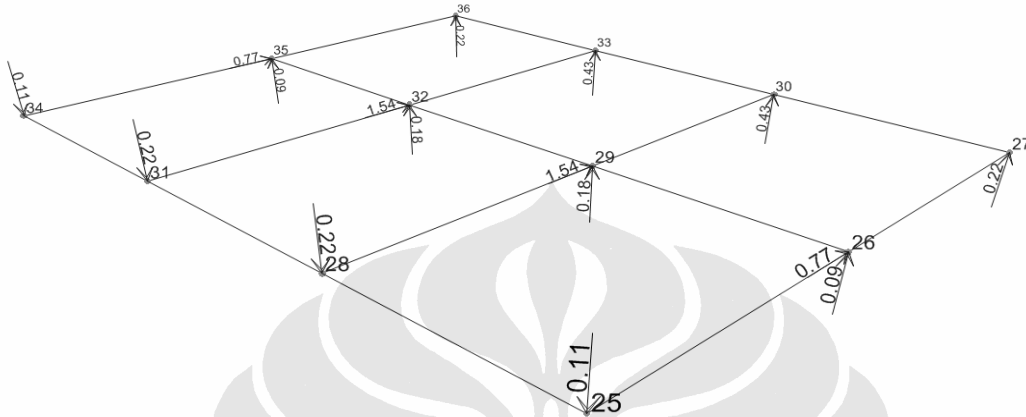
Beban Angin kanan

Arah Z

	1	2	3	4
A	-0.126	-0.251	-0.251	-0.126
B	0.118	0.236	0.236	0.118
C	0.308	0.615	0.615	0.308

Arah X

	1	2	3	4
A	0.000	0.000	0.000	0.000
B	0.304	0.607	0.607	0.304
C	0.000	0.000	0.000	0.000



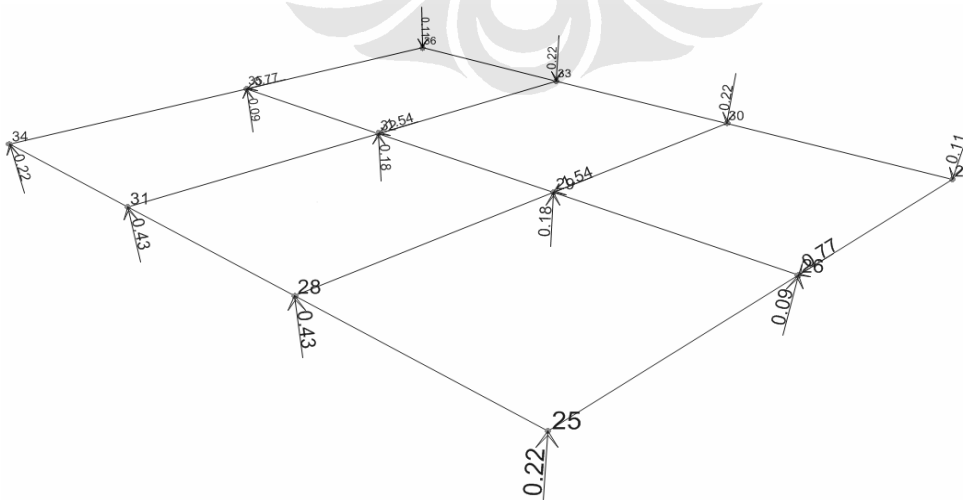
Beban Angin kiri

Arah Z

	1	2	3	4
A	0.308	0.615	0.615	0.308
B	0.118	0.236	0.236	0.118
C	-0.126	-0.251	-0.251	-0.126

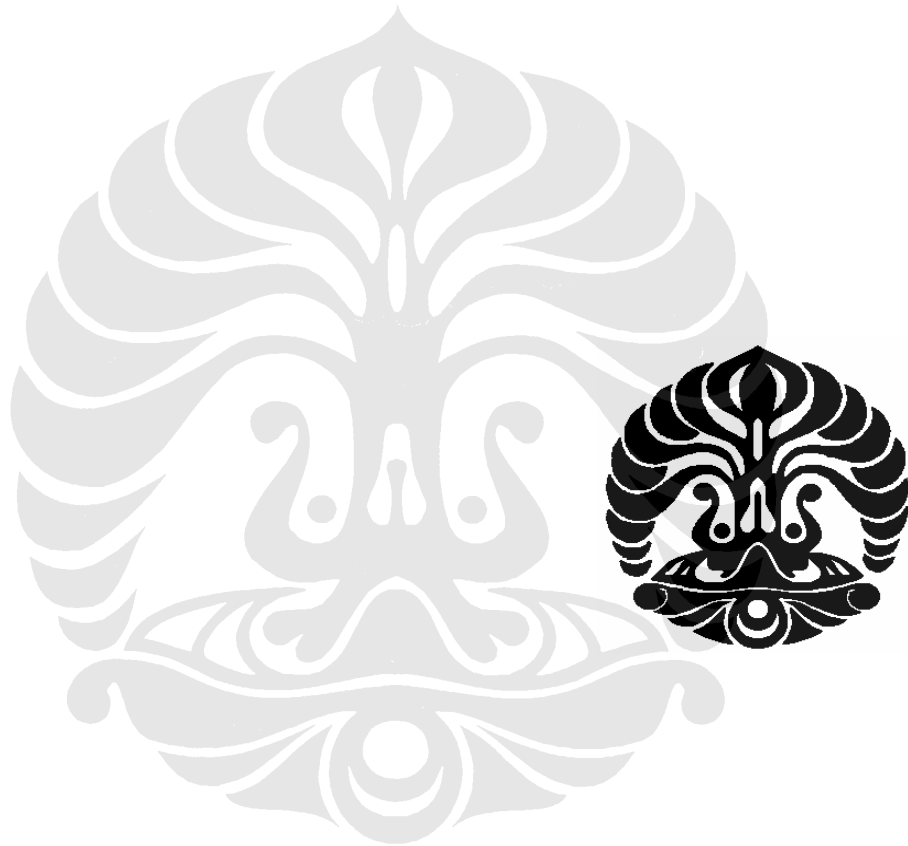
Arah -X

	1	2	3	4
A	0.000	0.000	0.000	0.000
B	-0.304	-0.607	-0.607	-0.304
C	0.000	0.000	0.000	0.000

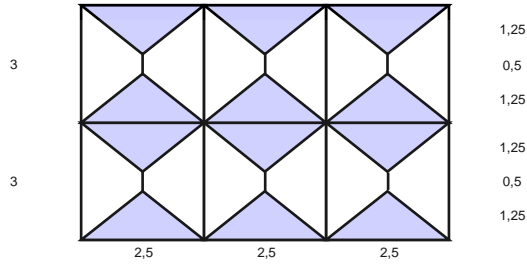


LAMPIRAN A2

Perhitungan Struktur Rumah Tinggal Satu Lantai Dengan Program SAP 2000



Beban Atap / Plafond

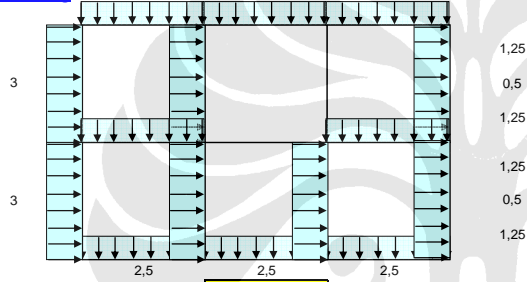


Beban Plafond 0,18 kN/m²

		1	2	3	4	
AB	0	0	0	0	0	0
	0,225	0,225	0,45	0,45	0,225	0,417
	0,225	0,225	0,45	0,45	0,225	0,583
BC	0	0	0	0	0	1
	0,225	0,225	0,45	0,45	0,225	
	0,225	0,225	0,45	0,45	0,225	
	0	0	0	0	0	

		A	B	C
12	0	0	0	0
	0,225	0,225	0,45	0,225
	0	0	0	0
23	0	0	0	0
	0,225	0,225	0,45	0,225
	0	0	0	0
34	0	0	0	0
	0,225	0,225	0,45	0,225
	0	0	0	0

Beban Dinding

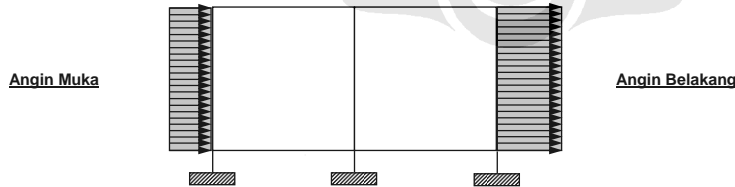


Tinggi Dinding 2,5 kN/m³ 3 m kN/m²

		1	2	3	4
AB	7,5	7,5	7,5	7,5	7,5
	7,5	7,5	7,5	7,5	7,5
BC	7,5	7,5	7,5	0	7,5
	7,5	7,5	7,5	0	7,5

		A	B	C
12	7,5	7,5	7,5	7,5
	7,5	7,5	7,5	7,5
23	7,5	7,5	0	7,5
	7,5	7,5	0	7,5
34	7,5	7,5	7,5	7,5
	7,5	7,5	7,5	7,5

Beban Angin



Angin Muka 0,25 kN/m² koefisien 0,9

		1	2	3	4
Lantai 1	1	1,25	2,5	2,5	1,25
		0,28125	0,5625	0,5625	0,28125

Angin Belakang 0,25 kN/m² koefisien 0,4

		1	2	3	4
Lantai 1	1	1,25	2,5	2,5	1,25
		0,125	0,25	0,25	0,125

Pusat Massa

Kolom Lantai 1

TABLE: Element Forces - Frames						
Frame	Station	P	X	PX	Y	PY
Text	m	KN	KN	KNm	KN	KNm
18	1,5	-7,138	0	0	0	0
19	1,5	-9,445	3	-28,335	0	0
20	1,5	-7,181	6	-43,086	0	0
21	1,5	-9,381	0	0	2,5	-23,4525
22	1,5	-13,088	3	-39,264	2,5	-32,72
23	1,5	-9,474	6	-56,844	2,5	-23,685
24	1,5	-9,456	0	0	5	-47,28
25	1,5	-12,988	3	-38,964	5	-64,94
26	1,5	-9,497	6	-56,982	5	-47,485
27	1,5	-7,149	0	0	7,5	-53,6175
28	1,5	-9,424	3	-28,272	7,5	-70,68
29	1,5	-7,191	6	-43,146	7,5	-53,9325
	TOTAL	-111,412		-334,893		-417,7925
			Xrata2 =	3,006	Yrata2 =	3,750

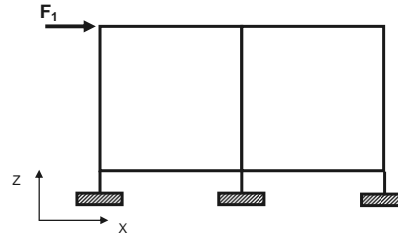
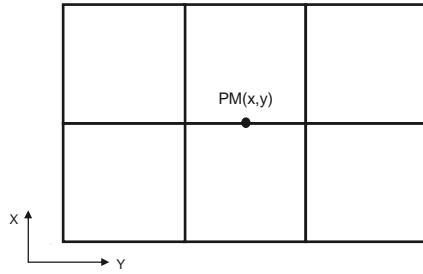
Pusat Rotasi

Frame	Station	Vx	X	Vx.X
Text	m	KN	KN	KN
18	1,5	-7,138	0	0
19	1,5	-9,445	3	-28,335
20	1,5	-7,181	6	-43,086
21	1,5	-9,381	0	0
22	1,5	-13,088	3	-39,264
23	1,5	-9,474	6	-56,844
24	1,5	-9,456	0	0
25	1,5	-12,988	3	-38,964
26	1,5	-9,497	6	-56,982
27	1,5	-7,149	0	0
28	1,5	-9,424	3	-28,272
29	1,5	-7,191	6	-43,146
TOTAL		-111,412		-334,893
			Xrata2 =	3,006

Kolom Lantai 1

Frame	Station	Vy	Y	Vy.Y
Text	m	KN	KN	KN
18	1,5	1,146	0	0
19	1,5	2,085	0	0
20	1,5	1,146	0	0
21	1,5	1,146	2,5	2,865
22	1,5	2,085	2,5	5,2125
23	1,5	1,146	2,5	2,865
24	1,5	1,146	5	5,73
25	1,5	2,085	5	10,425
26	1,5	1,146	5	5,73
27	1,5	1,146	7,5	8,595
28	1,5	2,085	7,5	15,638
29	1,5	1,146	7,5	8,595
TOTAL		17,508		65,655
			Yrata2 =	3,750

1 Gempa Statik Ekuivalen



3

Wilayah Gempa = 3
 h = 3
 T = 0,166631966
 C = 0,5 Didapat Dari Grafik Gbr.2
 I = 1 Keutamaan Bangunan
 R = 3,5 Dari tabel 2
 wt = 111,412
 V = 15,916
 W1 = 111,412
 F1 = 15,916
 (V) = 15,916

Pusat Massa

	x	y
PM 1	3,01	3,75

Pusat Rotasi

	x	y
PR1	3,01	3,75

Eksentrisitas Teoritis

	x	y
ex1	0,000	0,000

Eksentrisitas Desain

Gempa x

B = 7,5
 0.3 B = 2,25 Msk Rumus No.1

edy1	0,375
------	-------

Gempa y

B = 6
 0.3 B = 1,8 Msk Rumus No.1

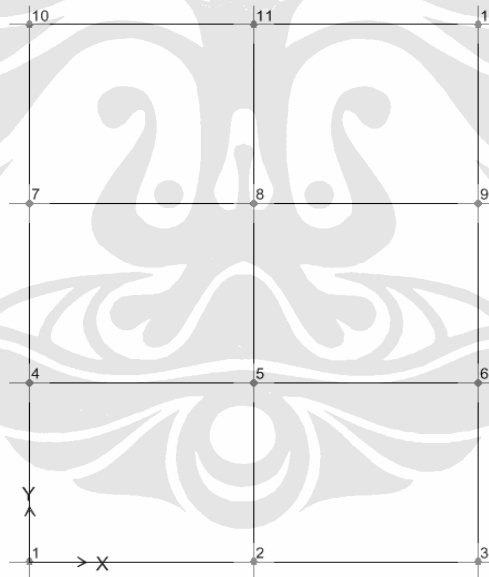
edx1	0,300
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Pusat Massa Desain

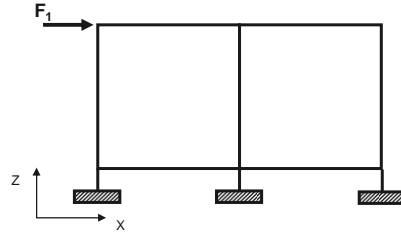
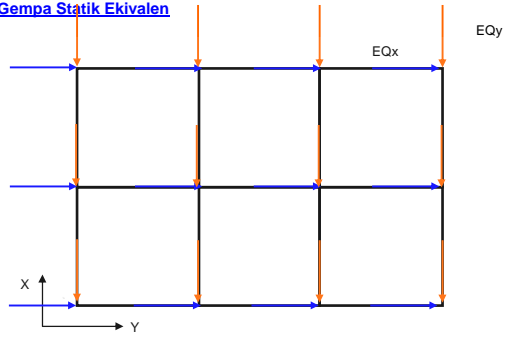
	x	y
Pm'1	3,306	4,125

TABLE: Joint Reactions		X	Y	Z
Joint	OutputCase	U1	U2	U3
Text	Text	KN	KN	KN
1	B.Mati	0,351	0,202	4,187
	LIVE	0,541	-0,0001128	0,363
	WIND.KA	-0,785	0,00004841	-0,562
	WIND.KI	-1,023	-0,108	-2,203
	EQ.x	-0,098	-0,984	-2,439
	EQ.y	1,906	1,317	32,745
2	B.Mati	8,72E-16	0,361	9,001
	LIVE	6,38E-01	-0,00004618	-0,101
	WIND.KA	-0,638	-0,00004618	-0,101
	WIND.KI	-1,906	-3,85E-16	-9,66E-16
	EQ.x	-0,144	-1,07E+00	-2,45E+00
	EQ.y	-0,143	1,405	52,031
3	B.Mati	-0,351	0,202	4,187
	LIVE	0,785	0,00004841	-0,562
	WIND.KA	-0,541	-0,0001128	0,363
	WIND.KI	-1,023	0,108	2,203
	EQ.x	-0,098	-1,156	-2,462
	EQ.y	-1,847	1,301	32,831
4	B.Mati	0,633	-0,025	8,852
	LIVE	0,736	-0,0001076	0,061
	WIND.KA	-1,224	0,00004612	-0,452
	WIND.KI	-1,123	-0,154	-2,112
	EQ.x	-0,019	-1,726	0,286
	EQ.y	2,044	-0,169	48,349
5	B.Mati	-5,99E-16	-0,041	18,63
	LIVE	6,40E-01	-0,00004406	-0,209
	WIND.KA	-0,64	-0,00004406	-0,209
	WIND.KI	-2,035	-6,58E-16	9,71E-17
	EQ.x	-0,04	-1,85E+00	3,47E-01
	EQ.y	-1,153	-0,866	46,178
6	B.Mati	-0,633	-0,025	8,852
	LIVE	1,224	0,00004612	-0,452
	WIND.KA	-0,736	-0,0001076	0,061
	WIND.KI	-1,123	0,154	2,112
	EQ.x	-0,019	-1,972	0,409
	EQ.y	-0,694	-0,192	36,831
7	B.Mati	0,633	0,025	8,852
	LIVE	0,736	0,0001076	0,061
	WIND.KA	-1,224	-0,00004612	-0,452
	WIND.KI	-1,169	-0,154	-2,265
	EQ.x	0,019	-1,726	-0,286
	EQ.y	1,951	0,192	47,889
8	B.Mati	-6,23E-16	0,041	18,63
	LIVE	6,40E-01	0,00004406	-0,209
	WIND.KA	-0,64	0,00004406	-0,209
	WIND.KI	-2,135	-6,54E-16	-3,19E-16
	EQ.x	0,04	-1,85E+00	-3,47E-01
	EQ.y	-0,12	0,866	58,005

9	B.Mati	-0,633	0,025	8,852
	LIVE	1,224	-0,00004612	-0,452
	WIND.KA	-0,736	0,0001076	0,061
	WIND.KI	-1,169	0,154	2,265
	EQ.x	0,019	-1,972	-0,409
	EQ.y	-1,881	0,169	47,965
10	B.Mati	0,351	-0,202	4,187
	LIVE	0,541	0,0001128	0,363
	WIND.KA	-0,785	-0,00004841	-0,562
	WIND.KI	-1,269	-0,108	-2,175
	EQ.x	0,098	-0,984	2,439
	EQ.y	1,907	-1,301	32,704
11	B.Mati	8,37E-16	-0,361	9,001
	LIVE	6,38E-01	0,00004618	-0,101
	WIND.KA	-0,638	0,00004618	-0,101
	WIND.KI	-2,265	-3,68E-16	1,19E-15
	EQ.x	0,144	-1,07E+00	2,45E+00
	EQ.y	-0,042	-1,405	52,093
12	B.Mati	-0,351	-0,202	4,187
	LIVE	0,785	-0,00004841	-0,562
	WIND.KA	-0,541	0,0001128	0,363
	WIND.KI	-1,269	0,108	2,175
	EQ.x	0,098	-1,156	2,462
	EQ.y	-1,929	-1,317	32,81



Beban Gempa Statik Ekuivalen



3

Wilayah Gempa = 3
 h = 3
 T = 0,166631966
 C = 0,5 Didapat Dari Grafik Gbr.2
 I = 1 Keutamaan Bangunan
 R = 3,5 Dari tabel 2
 wt = 111,412
 V = 15,916
 W1 = 111,412
 F1 = 15,916
 (V) = 15,916

Pembagian Beban Gempa Pada Kolom		
Frame	P	F
Text	KN	KN
18	-7,133	1,019
19	-9,446	1,349
20	-7,181	1,026
21	-9,371	1,339
22	-13,09	1,870
23	-9,484	1,355
24	-9,457	1,351
25	-12,991	1,856
26	-9,497	1,357
27	-7,158	1,023
28	-9,425	1,346
29	-7,177	1,025
	-111,41	15,916

Pengecekan Kondisi Diafragma

Akibat Beban Gempa Arah X

Lendutan Ujung kiri = 0,00627

Lendutan Ujung Kanan = 0,00627

Lendutan Rata2 δ_A = 0,00627

Lendutan Tengah δ_M = 0,00702

Kondisi Diafragma $\delta_M \leq 2*\delta_A$ **Rigid/ Kaku**

Akibat Beban Gempa Arah Y

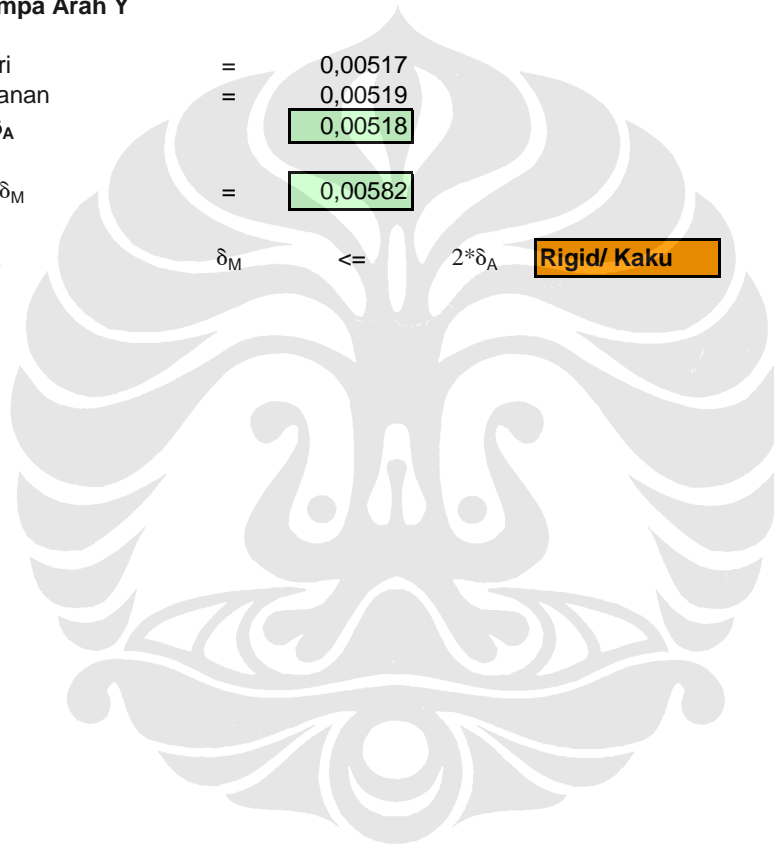
Lendutan Ujung kiri = 0,00517

Lendutan Ujung Kanan = 0,00519

Lendutan Rata2 δ_A = 0,00518

Lendutan Tengah δ_M = 0,00582

Kondisi Diafragma $\delta_M \leq 2*\delta_A$ **Rigid/ Kaku**



Pusat Massa

Kolom Lantai 1

TABLE: Element Forces - Frames						
Frame	Station	P	X	PX	Y	PY
Text	m	KN	KN	KNm	KN	KNm
18	1,5	-3,928	0	0	0	0
19	1,5	-5,576	3	-16,728	0	0
20	1,5	-3,911	6	-23,466	0	0
21	1,5	-5,595	0	0	2,5	-13,9875
22	1,5	-8,515	3	-25,545	2,5	-21,2875
23	1,5	-5,59	6	-33,54	2,5	-13,975
24	1,5	-5,619	0	0	5	-28,095
25	1,5	-8,482	3	-25,446	5	-42,41
26	1,5	-5,6	6	-33,6	5	-28
27	1,5	-3,93	0	0	7,5	-29,475
28	1,5	-5,571	3	-16,713	7,5	-41,7825
29	1,5	-3,914	6	-23,484	7,5	-29,355
	TOTAL	-66,231		-198,522		-248,3675
			Xrata2 =	2,997	Yrata2 =	3,750

Pusat Massa

Kolom Lantai 1				

TABLE: Element Forces - Frames

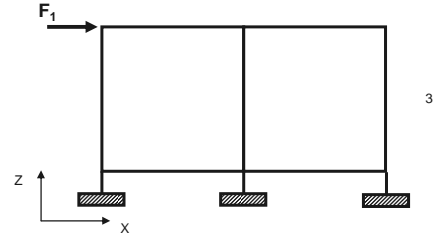
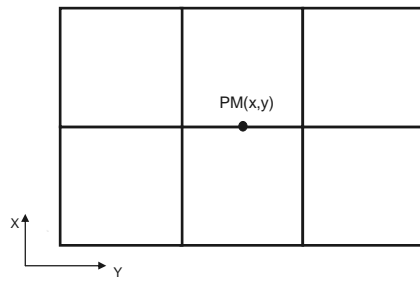
Frame	Station	Vx	X	Vx.X
Text	m	KN	KN	KN
18	1,5	0,553	0	0
19	1,5	0,528	3	1,584
20	1,5	0,553	6	3,318
21	1,5	1,189	0	0
22	1,5	0,718	3	2,154
23	1,5	1,189	6	7,134
24	1,5	1,189	0	0
25	1,5	0,718	3	2,154
26	1,5	1,189	6	7,134
27	1,5	0,553	0	0
28	1,5	0,528	3	1,584
29	1,5	0,553	6	3,318
TOTAL		9,46		28,38
			Xrata2 =	3,000

Kolom Lantai 1

TABLE: Element Forces - Frames

Frame	Station	Vy	Y	Vy.Y
Text	m	KN	KN	KN
18	1,5	0,744	0	0
19	1,5	1,152	0	0
20	1,5	0,744	0	0
21	1,5	0,498	2,5	1,245
22	1,5	1,093	2,5	2,7325
23	1,5	0,498	2,5	1,245
24	1,5	0,498	5	2,49
25	1,5	1,093	5	5,465
26	1,5	0,498	5	2,49
27	1,5	0,744	7,5	5,58
28	1,5	1,152	7,5	8,640
29	1,5	0,744	7,5	5,58
TOTAL		9,458		35,468
			Yrata2 =	3,750

Beban Gempa Statik Ekuivalen



Wilayah Gempa	=	3
h	=	3
T	=	0,166631966
C	=	0,5 Didapat Dari Grafik Gbr.2
I	=	1 Keutamaan Bangunan
R	=	3,5 Dari tabel 2
wt	=	66,231
V	=	9,461571429
W1	=	66,231
F1	=	9,461571429
(V)	=	9,461571429

Pusat Massa

	x	y
PM 1	2,997	3,750

Pusat Rotasi

	x	y
PR1	3,000	3,750

Eksentrisitas Teoritis

ex1	-0,003	0,000
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Eksentrisitas Desain

Gempa x		
B	=	7,5
0.3 B	=	2,25

edy1	0,375
------	-------

Gempa y		
B	=	6
0.3 B	=	1,8

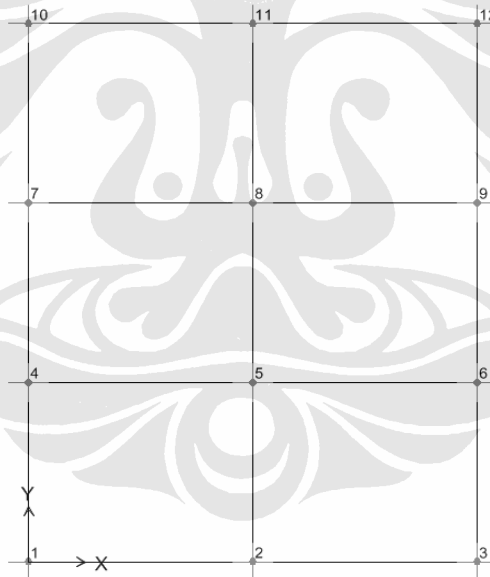
edx1	0,296
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Pusat Massa Desain

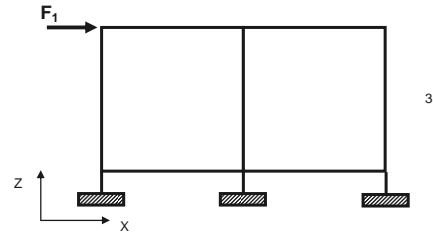
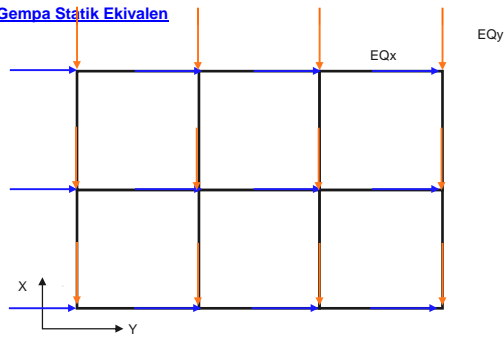
	x	y
Pm'1	2,699	4,125

TABLE: Joint Reactions		X	Y	Z
Joint	OutputCase	U1	U2	U3
Text	Text	KN	KN	KN
1	B.Mati	1,229	0,385	25,544
	LIVE	0,22	0,05	3,728
	WIND.KA	-0,882	0,00002312	-0,638
	WIND.KI	0,615	-0,00005211	0,405
	EQ.x	-0,778	0,000002168	-1,329
	EQ.y	-0,058	-0,421	-1,315
2	B.Mati	-2,90E-02	0,46	46,598
	LIVE	-8,51E-17	0,093	9,076
	WIND.KA	-0,627	-0,0000201	-0,067
	WIND.KI	0,627	-2,01E-05	-6,70E-02
	EQ.x	-1,181	1,18E-19	3,36E-19
	EQ.y	-0,081	-0,412	-0,876
3	B.Mati	-1,089	0,386	25,546
	LIVE	-0,22	0,05	3,728
	WIND.KA	-0,615	-0,00005211	0,405
	WIND.KI	0,882	0,00002312	-0,638
	EQ.x	-0,778	-0,000002168	1,329
	EQ.y	-0,058	-0,477	-1,274
4	B.Mati	0,785	-0,287	42,304
	LIVE	0,196	-0,049	8,461
	WIND.KA	-1,195	0,00002626	-0,43
	WIND.KI	0,66	-0,00005814	-0,034
	EQ.x	-0,448	0,000002432	-1,036
	EQ.y	-0,007334	-1,367	-0,566
5	B.Mati	-7,28E-01	-0,24	41,146
	LIVE	-2,31E-18	-0,023	20,255
	WIND.KA	-0,586	-0,00001668	-0,136
	WIND.KI	0,586	-1,67E-05	-1,36E-01
	EQ.x	-1,098	3,08E-19	1,10E-16
	EQ.y	-0,023	-0,538	0,186
6	B.Mati	-0,238	-0,285	31,017
	LIVE	-0,196	-0,049	8,461
	WIND.KA	-0,66	-0,00005814	-0,034
	WIND.KI	1,195	0,00002626	-0,43
	EQ.x	-0,448	-0,000002432	1,036
	EQ.y	-0,007349	-1,517	-0,579
7	B.Mati	0,717	0,285	41,449
	LIVE	0,196	0,049	8,461
	WIND.KA	-1,195	-0,00002626	-0,43
	WIND.KI	0,66	0,00005814	-0,034
	EQ.x	-0,448	-0,000002432	-1,036
	EQ.y	0,007334	-1,367	0,566
8	B.Mati	-3,50E-02	0,24	54,005
	LIVE	-3,54E-17	0,023	20,255
	WIND.KA	-0,586	0,00001668	-0,136
	WIND.KI	0,586	1,67E-05	-1,36E-01
	EQ.x	-1,098	-6,19E-19	-1,11E-16
	EQ.y	0,023	-0,538	-0,186

9	B.Mati	-0,659	0,287	41,513
	LIVE	-0,196	0,049	8,461
	WIND.KA	-0,66	0,00005814	-0,034
	WIND.KI	1,195	-0,00002626	-0,43
	EQ.x	-0,448	0,000002432	1,036
	EQ.y	0,007349	-1,517	0,579
10	B.Mati	1,203	-0,386	25,495
	LIVE	0,22	-0,05	3,728
	WIND.KA	-0,882	-0,00002312	-0,638
	WIND.KI	0,615	0,00005211	0,405
	EQ.x	-0,778	-0,000002168	-1,329
	EQ.y	0,058	-0,421	1,315
11	B.Mati	1,20E-02	-0,46	46,728
	LIVE	-7,15E-17	-0,093	9,076
	WIND.KA	-0,627	0,0000201	-0,067
	WIND.KI	0,627	2,01E-05	-6,70E-02
	EQ.x	-1,181	9,88E-19	5,17E-19
	EQ.y	0,081	-0,412	0,876
12	B.Mati	-1,169	-0,385	25,466
	LIVE	-0,22	-0,05	3,728
	WIND.KA	-0,615	0,00005211	0,405
	WIND.KI	0,882	-0,00002312	-0,638
	EQ.x	-0,778	0,000002168	1,329
	EQ.y	0,058	-0,477	1,274



Beban Gempa Statik Ekuivalen



Wilayah Gempa	=	3
h	=	3
T	=	0,166631966
C	=	0,5 Didapat Dari Grafik Gbr.2
I	=	1 Keutamaan Bangunan
R	=	3,5 Dari tabel 2
wt	=	66,23
V	=	9,461
W1	=	66,23
F1	=	9,461
(V)	=	9,461

Pembagian Beban Gempa Pada Kolom		
Frame	P	F
Text	KN	KN
18	-3,928	0,561
19	-5,576	0,797
20	-3,911	0,559
21	-5,595	0,799
22	-8,515	1,216
23	-5,59	0,799
24	-5,619	0,803
25	-8,482	1,212
26	-5,6	0,800
27	-3,93	0,561
28	-5,571	0,796
29	-3,914	0,559
	-66,231	9,461

Pengecekan Kondisi Diafragma

Akibat Beban Gempa Arah X

Lendutan Ujung kiri = 0,000615

Lendutan Ujung Kanan = 0,000615

Lendutan Rata2 δ_A = 0,000615

Lendutan Tengah δ_M = 0,000958

Kondisi Diafragma $\delta_M \leq 2 \cdot \delta_A$ **Rigid/ Kaku**

Akibat Beban Gempa Arah Y

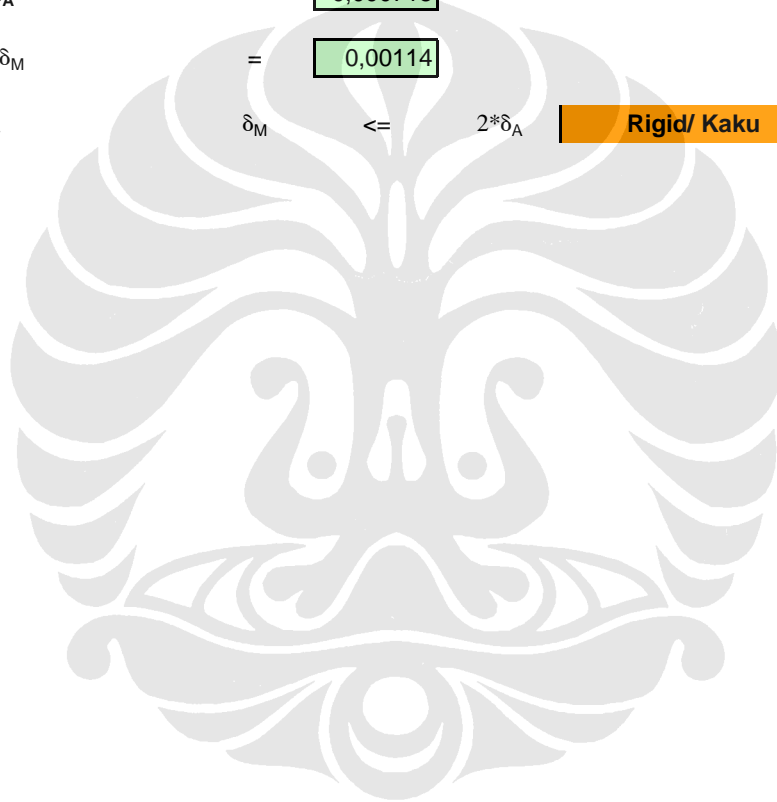
Lendutan Ujung kiri = 0,000719

Lendutan Ujung Kanan = 0,000717

Lendutan Rata2 δ_A = 0,000718

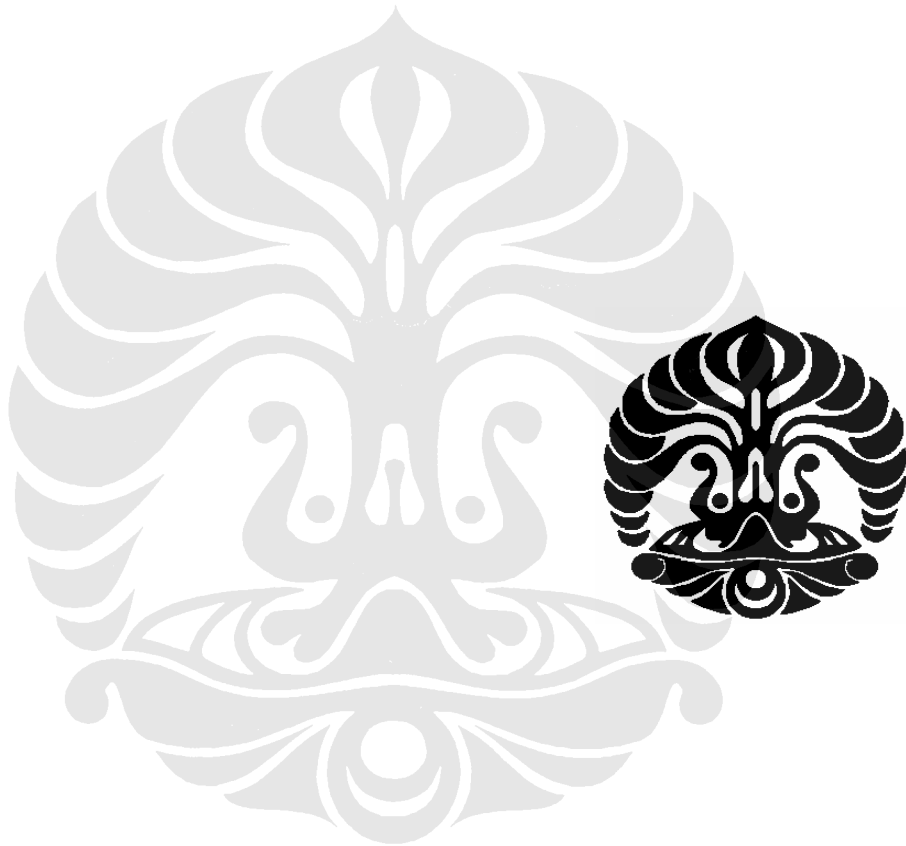
Lendutan Tengah δ_M = 0,00114

Kondisi Diafragma $\delta_M \leq 2 \cdot \delta_A$ **Rigid/ Kaku**

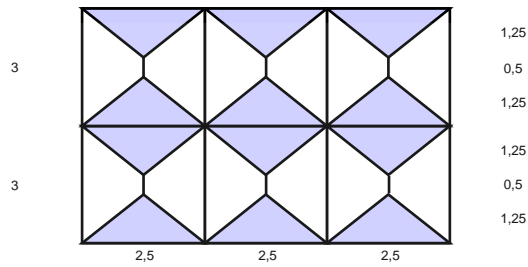


LAMPIRAN A3

Perhitungan Struktur Rumah Tinggal Dua Lantai Dengan Program SAP 2000



Beban Atap / Plafond

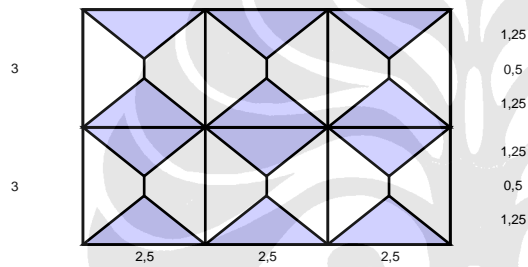


Beban Plafond 0,18 kN/m²

		1	2	3	4
AB	0	0	0	0	0
	0,225	0,225	0,45	0,45	0,225
	0,225	0,225	0,45	0,45	0,225
BC	0	0	0	0	0
	0,225	0,225	0,45	0,45	0,225
	0,225	0,225	0,45	0,45	0,225
	0	0	0	0	0

		A	B	C
12	0	0	0	0
	0,225	0,225	0,45	0,225
	0	0	0	0
23	0	0	0	0
	0,225	0,225	0,45	0,225
	0	0	0	0
34	0	0	0	0
	0,225	0,225	0,45	0,225
	0	0	0	0

Beban Lantai

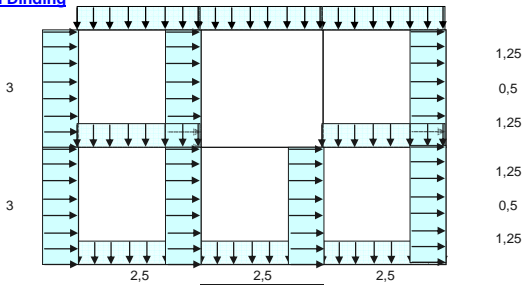


Beban Mati 30,6 kN/m³ 3,06 kN/m²

		1	2	3	4
AB	0	0	0	0	0
	3,825	3,825	7,65	7,65	3,825
	3,825	3,825	7,65	7,65	3,825
BC	0	0	0	0	0
	3,825	3,825	7,65	7,65	3,825
	3,825	3,825	7,65	7,65	3,825
	0	0	0	0	0

		A	B	C
12	0	0	0	0
	3,825	3,825	7,65	3,825
	0	0	0	0
23	0	0	0	0
	3,825	3,825	7,65	3,825
	0	0	0	0
34	0	0	0	0
	3,825	3,825	7,65	3,825
	0	0	0	0

Beban Dinding



Tinggi Dinding 2,5 kN/m³ 3 m kN/m²

Beban Mati	1	2	3	4
AB	7,5	7,5	7,5	7,5
BC	7,5	7,5	0	7,5

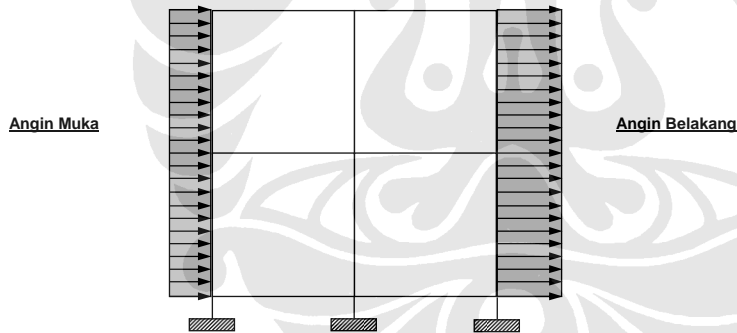
	A	B	C
12	7,5	7,5	7,5
23	7,5	0	7,5
34	7,5	7,5	7,5

Beban Hidup 1,25 kN/m²

	1	2	3	4
AB	0	0	0	0
BC	1,5625	1,5625	3,125	1,5625

	A	B	C
12	0	0	0
23	0	0	0
34	0	0	0

Beban Angin



Angin Muka 0,25 kN/m² koefisien 0,9

	1	2	3	4
Lantai 1	1	0,28125	0,5625	0,28125
Lantai 2	1	0,28125	0,5625	0,28125

Angin Belakang 0,25 kN/m² koefisien 0,4

	1	2	3	4
Lantai 1	1	0,125	0,25	0,125
Lantai 2	1	0,125	0,25	0,125

Pusat Massa

Kolom Lantai 1

TABLE: Element Forces - Frames						
Frame	Station	P	X	PX	Y	PY
Text	m	KN	KN	KNm	KN	KNm
18	1,5	-42,048	0	0	0	0
19	1,5	-65,601	3	-196,803	0	0
20	1,5	-42,077	6	-252,462	0	0
21	1,5	-62,385	0	0	2,5	-155,9625
22	1,5	-71,864	3	-215,592	2,5	-179,66
23	1,5	-51,048	6	-306,288	2,5	-127,62
24	1,5	-62,107	0	0	5	-310,535
25	1,5	-83,585	3	-250,755	5	-417,925
26	1,5	-62,18	6	-373,08	5	-310,9
27	1,5	-42,043	0	0	7,5	-315,3225
28	1,5	-65,633	3	-196,899	7,5	-492,2475
29	1,5	-42,119	6	-252,714	7,5	-315,8925
TOTAL		-692,69		-2044,593		-2626,065
			Xrata2 =	2,952	Yrata2 =	3,791

Kolom Lantai 2

TABLE: Element Forces - Frames						
Frame	Station	P	X	PX	Y	PY
Text	m	KN	KN	KNm	KN	KNm
47	1,5	-7,077	0	0	0	0
48	1,5	-9,556	3	-28,668	0	0
49	1,5	-7,058	6	-42,348	0	0
50	1,5	-9,443	0	0	2,5	-23,6075
51	1,5	-13,127	3	-39,381	2,5	-32,8175
52	1,5	-9,489	6	-56,934	2,5	-23,7225
53	1,5	-9,492	0	0	5	-47,46
54	1,5	-12,982	3	-38,946	5	-64,91
55	1,5	-9,466	6	-56,796	5	-47,33
56	1,5	-7,083	0	0	7,5	-53,1225
57	1,5	-9,565	3	-28,695	7,5	-71,7375
58	1,5	-7,071	6	-42,426	7,5	-53,0325
TOTAL		-111,409		-334,194		-417,74
			Xrata2 =	3,000	Yrata2 =	3,750

Pusat Rotasi

Kolom Lantai 1				

TABLE: Element Forces - Frames

Frame	Station	Vx	X	Vx.X
Text	m	KN	KN	KN
18	1,5	7,726	0	0
19	1,5	7,671	3	23,013
20	1,5	7,615	6	45,69
21	1,5	11,126	0	0
22	1,5	11,05	3	33,15
23	1,5	10,974	6	65,844
24	1,5	11,126	0	0
25	1,5	11,05	3	33,15
26	1,5	10,974	6	65,844
27	1,5	7,726	0	0
28	1,5	7,671	3	23,013
29	1,5	7,615	6	45,69
	TOTAL	112,324		335,394
			Xrata2 =	2,986

Kolom Lantai 2

TABLE: Element Forces - Frames

Frame	Station	Vx	X	Vx.X
Text	m	KN	KN	KN
47	1,5	-2,71	0	0
48	1,5	-2,692	3	-8,076
49	1,5	-2,674	6	-16,044
50	1,5	-2,606	0	0
51	1,5	-2,589	3	-7,767
52	1,5	-2,572	6	-15,432
53	1,5	-2,606	0	0
54	1,5	-2,589	3	-7,767
55	1,5	-2,572	6	-15,432
56	1,5	-2,71	0	0
57	1,5	-2,692	3	-8,076
58	1,5	-2,674	6	-16,044
	TOTAL	-31,686		-94,638
			Xrata2 =	2,987

Kolom Lantai 1

TABLE: Element Forces - Frames

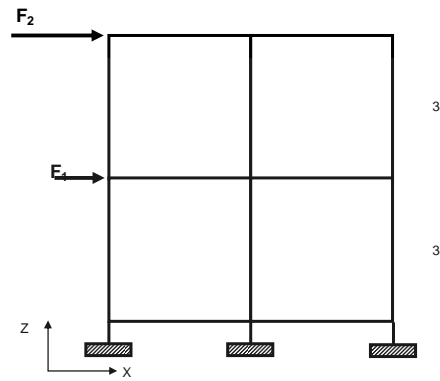
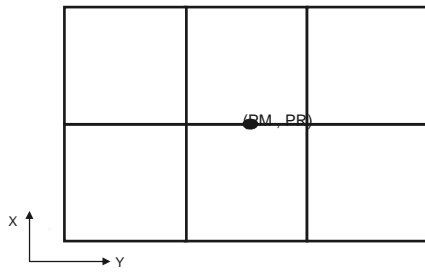
Frame	Station	Vy	Y	Vy.Y
Text	m	KN	KN	KN
18	1,5	7,986	0	0
19	1,5	11,948	0	0
20	1,5	7,986	0	0
21	1,5	8,024	2,5	20,060
22	1,5	12	2,5	30
23	1,5	8,024	2,5	20,060
24	1,5	8,058	5	40,29
25	1,5	12,05	5	60,25
26	1,5	8,058	5	40,29
27	1,5	8,095	7,5	60,7125
28	1,5	12,102	7,5	90,765
29	1,5	8,095	7,5	60,7125
TOTAL		112,426		423,140
			Yrata2 =	3,764

Kolom Lantai 2

TABLE: Element Forces - Frames

Frame	Station	Vy	Y	Vy.Y
Text	m	KN	KN	KN
47	1,5	-3,047	0	0
48	1,5	-3,051	0	0
49	1,5	-3,047	0	0
50	1,5	-3,06	2,5	-7,65
51	1,5	-3,064	2,5	-7,66
52	1,5	-3,06	2,5	-7,65
53	1,5	-3,073	5	-15,365
54	1,5	-3,077	5	-15,385
55	1,5	-3,073	5	-15,365
56	1,5	-3,086	7,5	-23,145
57	1,5	-3,089	7,5	-23,168
58	1,5	-3,086	7,5	-23,145
TOTAL		-36,813		-138,533
			Yrata2 =	3,763

Beban Gempa Statik Ekuivalen



Wilayah Gempa	=	3
h	=	6
T	=	0,280240446
C	=	0,55 Didapat Dari Grafik Gbr.2
I	=	1 Keutamaan Bangunan
R	=	3,5 Dari tabel 2
wt	=	714,791
V	=	112,3243
W1	=	598,152
W2	=	116,639
F1	=	80,80897333
F2	=	31,51532667
(V)	=	112,3243

Pusat Massa

	x	y
PM 2	3,00	3,75
PM 1	2,95	3,79

Pusat Rotasi

	x	y
PR2	2,99	3,76
PR1	2,99	3,76

Eksentrisitas Teoritis

ex2	0,013	-0,014
ex1	-0,034	0,027

Eksentrisitas Desain

Gempa x

B	=	7,5	
0.3 B	=	2,25	Msk Rumus No.1

edy2	0,395
edy1	0,416

Gempa y

B	=	6	
0.3 B	=	1,8	Msk Rumus No.1

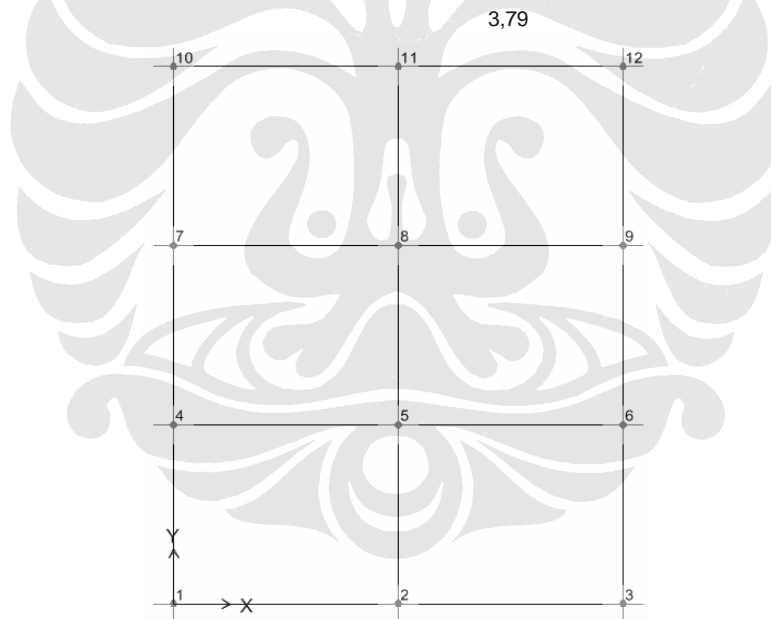
edx2	0,319
edx1	0,249

Pusat Massa Desain

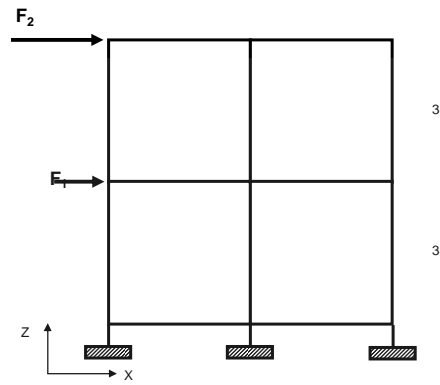
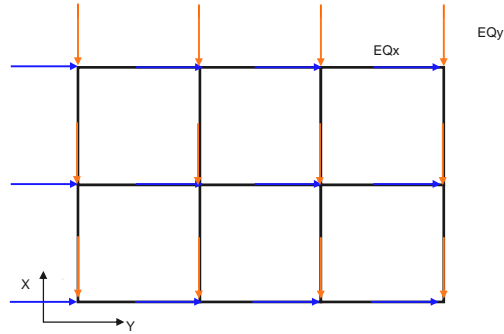
	x	y
Pm'2	3,306	4,158
Pm'1	3,235	4,180

TABLE: Joint Reactions		X	Y	Z
Joint	OutputCase	U1	U2	U3
Text	Text	KN	KN	KN
1	B.Mati	3,79	-0,307	101,454
	LIVE	0,268	-0,003253	6,212
	WIND.KA	-1,651	0,00003709	-0,901
	WIND.KI	1,265	-0,00008655	0,521
	EQ.x	-7,812	-1,001	-9,024
	EQ.y	-0,139	-10,42	1,517
2	B.Mati	-2,359	-1,581	104,813
	LIVE	-4,50E-16	-0,006382	12,229
	WIND.KA	-1,456	-0,00003455	-0,219
	WIND.KI	1,456	-0,00003455	-0,219
	EQ.x	-11,657	6,94E-18	1,93E-18
	EQ.y	-0,225	-11,05	1,781
3	B.Mati	-1,163	-0,313	78,615
	LIVE	-0,268	-0,003253	6,212
	WIND.KA	-1,265	-0,00008655	0,521
	WIND.KI	1,651	0,00003709	-0,901
	EQ.x	-7,812	1,001	9,024
	EQ.y	-0,139	-11,68	2,044
4	B.Mati	3,756	0,196	101,137
	LIVE	0,268	0,003253	6,212
	WIND.KA	-1,651	-0,00003709	-0,901
	WIND.KI	1,265	0,00008655	0,521
	EQ.x	-8,255	-1,001	-9,862
	EQ.y	0,139	-10,42	-1,517
5	B.Mati	-1,585	0,718	105,684
	LIVE	-4,53E-16	0,006382	12,229
	WIND.KA	-1,456	0,00003455	-0,219
	WIND.KI	1,456	0,00003455	-0,219
	EQ.x	-12,372	1,39E-17	9,01E-16
	EQ.y	0,225	-11,05	-1,781
6	B.Mati	-2,004	0,193	89,65
	LIVE	-0,268	0,003253	6,212
	WIND.KA	-1,265	0,00008655	0,521
	WIND.KI	1,651	-0,00003709	-0,901
	EQ.x	-8,255	1,001	9,862
	EQ.y	0,139	-11,68	-2,044
7	B.Mati	3,315	-2,198	68,197
	LIVE	0,141	-0,083	3,069
	WIND.KA	-1,294	-0,00003817	-1,015
	WIND.KI	1,107	0,00008822	0,823
	EQ.x	-8,946	-0,776	-9,373
	EQ.y	0,574	-7,183	11,301
8	B.Mati	-0,251	-1,507	98,536
	LIVE	1,80E-16	-0,157	6,042
	WIND.KA	-1,447	0,00003516	-0,109
	WIND.KI	1,447	0,00003516	-0,109
	EQ.x	-13,22	0,00E+00	-9,01E-16
	EQ.y	0,759	-7,671	11,345

9	B.Mati	-3,274	-2,203	68,385
	LIVE	-0,141	-0,083	3,069
	WIND.KA	-1,107	0,00008822	0,823
	WIND.KI	1,294	-0,00003817	-1,015
	EQ.x	-8,946	0,776	9,373
	EQ.y	0,574	-8,159	11,39
10	B.Mati	3,202	-2,121	68,371
	LIVE	0,121	-0,071	2,966
	WIND.KA	-1,29	-0,00006878	-1,171
	WIND.KI	1,103	0,0001642	0,978
	EQ.x	-9,118	-0,791	-10,925
	EQ.y	0,583	-7,34	13,089
11	B.Mati	-0,26	-1,382	100,702
	LIVE	3,50E-16	-0,132	6,105
	WIND.KA	-1,454	0,00006542	-0,108
	WIND.KI	1,454	0,00006542	-0,108
	EQ.x	-13,604	1,39E-17	8,78E-16
	EQ.y	0,781	-7,837	13,136
12	B.Mati	-3,163	-2,129	68,602
	LIVE	-0,121	-0,071	2,966
	WIND.KA	-1,103	0,0001642	0,978
	WIND.KI	1,29	-0,00006878	-1,171
	EQ.x	-9,118	0,791	10,925
	EQ.y	0,583	-8,334	13,183



Beban Gempa Statik Ekuivalen



Wilayah Gempa = 3
 h = 6
 T = 0,280240446
 C = 0,55 Didapat Dari Grafik Gbr.2
 I = 1 Keutamaan Bangunan
 R = 3,5 Dari tabel 2
 Wt = 714,791
 V = 112,3243

 W1 = 598,152
 W2 = 116,639

 F1 = 80,80897333
 F2 = 31,51532667
 (V) = 112,3243

TABLE: Element Forces - Frames		
Frame	P	F
Text	KN	KN
18	-42,952	4,856
19	-67,424	7,622
20	-42,981	4,859
21	-64,238	7,262
22	-75,577	8,544
23	-52,902	5,981
24	-63,96	7,231
25	-87,297	9,869
26	-64,033	7,239
27	-42,947	4,855
28	-67,457	7,626
29	-43,023	4,864
	-714,791	80,809

TABLE: Element Forces - Frames		
Frame	P	F
Text	KN	KN
47	-7,323	1,979
48	-9,953	2,689
49	-7,303	1,973
50	-9,919	2,680
51	-13,901	3,756
52	-9,965	2,692
53	-9,968	2,693
54	-13,757	3,717
55	-9,942	2,686
56	-7,329	1,980
57	-9,962	2,692
58	-7,317	1,977
	-116,639	31,515

Pengecekan Kondisi Diafragma

Lantai 1

Akibat Beban Gempa Arah X

Lendutan Ujung kiri = 0,02787

Lendutan Ujung Kanan = 0,02667

Lendutan Rata2 δ_A = 0,02727

Lendutan Tengah δ_M = 0,02727

Kondisi Diafragma $\delta_M \leq 2*\delta_A$ **Rigid/ Kaku**

Akibat Beban Gempa Arah Y

Lendutan Ujung kiri = 0,02193

Lendutan Ujung Kanan = 0,02083

Lendutan Rata2 δ_A = 0,02138

Lendutan Tengah δ_M = 0,02138

Kondisi Diafragma $\delta_M \leq 2*\delta_A$ **Rigid/ Kaku**

Lantai 2

Akibat Beban Gempa Arah X

Lendutan Ujung kiri = 0,04686

Lendutan Ujung Kanan = 0,04526

Lendutan Rata2 δ_A = 0,04606

Lendutan Tengah δ_M = 0,04706

Kondisi Diafragma $\delta_M \leq 2*\delta_A$ **Rigid/ Kaku**

Akibat Beban Gempa Arah Y

Lendutan Ujung kiri = 0,03608

Lendutan Ujung Kanan = 0,02307

Lendutan Rata2 δ_A = 0,029575

Lendutan Tengah δ_M = 0,03566

Kondisi Diafragma $\delta_M \leq 2*\delta_A$ **Rigid/ Kaku**

Pusat Massa

Kolom Lantai 1

TABLE: Element Forces - Frames						
Frame	Station	P	X	PX	Y	PY
Text	m	KN	KN	KNm	KN	KNm
18	1,5	-36,258	0	0	0	0
19	1,5	-60,793	3	-182,379	0	0
20	1,5	-35,658	6	-213,948	0	0
21	1,5	-58,009	0	0	2,5	-145,0225
22	1,5	-74,581	3	-223,743	2,5	-186,4525
23	1,5	-47,372	6	-284,232	2,5	-118,43
24	1,5	-57,613	0	0	5	-288,065
25	1,5	-87,625	3	-262,875	5	-438,125
26	1,5	-57,458	6	-344,748	5	-287,29
27	1,5	-36,223	0	0	7,5	-271,6725
28	1,5	-60,748	3	-182,244	7,5	-455,61
29	1,5	-35,672	6	-214,032	7,5	-267,54
TOTAL		-648,01		-1908,201		-2458,2075
			Xrata2 =	2,945	Yrata2 =	3,793

Kolom Lantai 2

TABLE: Element Forces - Frames						
Frame	Station	P	X	PX	Y	PY
Text	m	KN	KN	KNm	KN	KNm
47	1,5	-4,119	0	0	0	0
48	1,5	-6,044	3	-18,132	0	0
49	1,5	-4,106	6	-24,636	0	0
50	1,5	-6,086	0	0	2,5	-15,215
51	1,5	-9,297	3	-27,891	2,5	-23,2425
52	1,5	-6,084	6	-36,504	2,5	-15,21
53	1,5	-6,096	0	0	5	-30,48
54	1,5	-9,261	3	-27,783	5	-46,305
55	1,5	-6,088	6	-36,528	5	-30,44
56	1,5	-4,121	0	0	7,5	-30,9075
57	1,5	-6,047	3	-18,141	7,5	-45,3525
58	1,5	-4,11	6	-24,66	7,5	-30,825
TOTAL		-71,459		-214,275		-267,9775
			Xrata2 =	2,999	Yrata2 =	3,750

Pusat Rotasi

Kolom Lantai 1				

TABLE: Element Forces - Frames

Frame	Station	Vx	X	Vx.X
Text	m	KN	KN	KN
18	1,5	3,831	0	0
19	1,5	3,223	3	9,669
20	1,5	3,781	6	22,686
21	1,5	18,369	0	0
22	1,5	3,579	3	10,737
23	1,5	18,132	6	108,792
24	1,5	18,369	0	0
25	1,5	3,579	3	10,737
26	1,5	18,132	6	108,792
27	1,5	3,831	0	0
28	1,5	3,223	3	9,669
29	1,5	3,781	6	22,686
TOTAL		101,83		303,768
			Xrata2 =	2,983

Kolom Lantai 2

TABLE: Element Forces - Frames

Frame	Station	Vx	X	Vx.X
Text	m	KN	KN	KN
47	1,5	-0,059	0	0
48	1,5	-0,138	3	-0,414
49	1,5	-0,058	6	-0,348
50	1,5	-1,791	0	0
51	1,5	-0,063	3	-0,189
52	1,5	-1,768	6	-10,608
53	1,5	-1,791	0	0
54	1,5	-0,063	3	-0,189
55	1,5	-1,768	6	-10,608
56	1,5	-0,059	0	0
57	1,5	-0,138	3	-0,414
58	1,5	-0,058	6	-0,348
TOTAL		-7,754		-23,118
			Xrata2 =	2,981

Kolom Lantai 1

TABLE: Element Forces - Frames

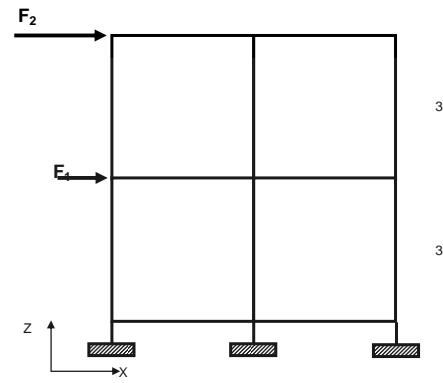
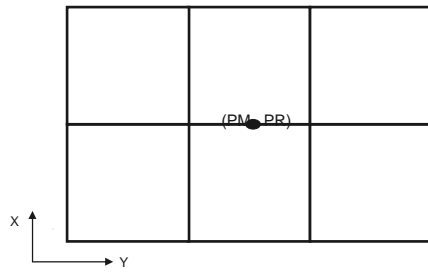
Frame	Station	Vy	Y	Vy.Y
Text	m	KN	KN	KN
18	1,5	9,188	0	0
19	1,5	14,689	0	0
20	1,5	9,188	0	0
21	1,5	2,856	2,5	7,140
22	1,5	11,832	2,5	29,58
23	1,5	2,856	2,5	7,140
24	1,5	2,869	5	14,345
25	1,5	11,896	5	59,48
26	1,5	2,869	5	14,345
27	1,5	9,332	7,5	69,99
28	1,5	14,924	7,5	111,930
29	1,5	9,332	7,5	69,99
TOTAL		101,831		383,940
			Yrata2 =	3,770

Kolom Lantai 2

TABLE: Element Forces - Frames

Frame	Station	Vy	Y	Vy.Y
Text	m	KN	KN	KN
47	1,5	-1,340	0	0
48	1,5	-1,110	0	0
49	1,5	-1,340	0	0
50	1,5	-0,063	2,5	-0,1575
51	1,5	-1,244	2,5	-3,11
52	1,5	-0,063	2,5	-0,1575
53	1,5	-0,063	5	-0,315
54	1,5	-1,250	5	-6,25
55	1,5	-0,063	5	-0,315
56	1,5	-1,361	7,5	-10,2075
57	1,5	-1,127	7,5	-8,453
58	1,5	-1,361	7,5	-10,2075
TOTAL		-10,385		-39,173
			Yrata2 =	3,772

Beban Gempa Statik Ekuivalen



Wilayah Gempa	=	3
h	=	6
T	=	0,280240446
C	=	0,55 Didapat Dari Grafik Gbr.2
I	=	1 Keutamaan Bangunan
R	=	3,5 Dari tabel 2
wt	=	648,01
V	=	101,8301429
W1	=	576,551
W2	=	71,459
F1	=	81,60222427
F2	=	20,22791859
(V)	=	101,8301429

Pusat Massa

	x	y
PM 2	3,00	3,75
PM 1	2,94	3,79

Pusat Rotasi

	x	y
PR2	2,98	3,77
PR1	2,98	3,77

Eksentrisitas Teoritis

ex2	0,017	0,022
ex1	0,038	0,023

Eksentrisitas Desain

Gempa x

B	=	7,5	
0.3 B	=	2,25	Msk Rumus No.1

edy2	0,408
edy1	0,410

Gempa y

B	=	6	
0.3 B	=	1,8	Msk Rumus No.1

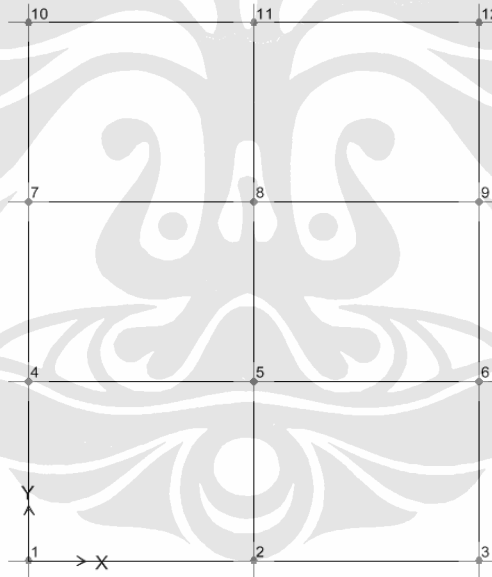
edx2	0,326
edx1	0,358

Pusat Massa Desain

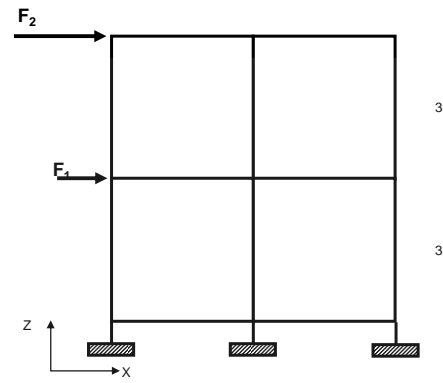
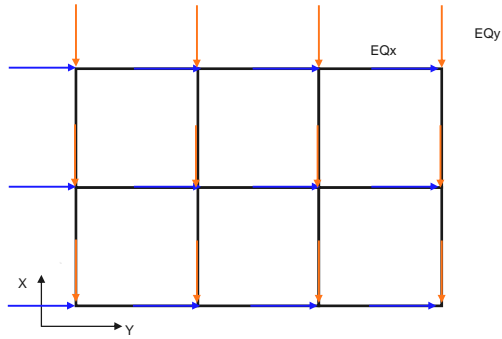
	x	y
Pm'2	3,307	3,364
Pm'1	2,626	4,180

TABLE: Joint Reactions		X	Y	Z
Joint	OutputCase	U1	U2	U3
Text	Text	KN	KN	KN
1	B.Mati	4,987	1,076	61,081
	LIVE	0,244	0,043	2,865
	WIND.KA	-1,493	0,0002375	-1,717
	WIND.KI	1,321	-0,0003177	1,53
	EQ.x	-6,605	-0,215	-10,936
	EQ.y	-1,339	-3,201	-12,785
2	B.Mati	0,498	1,36	98,584
	LIVE	2,64E-16	0,083	5,835
	WIND.KA	-1,945	-0,000046	-0,114
	WIND.KI	1,945	-0,000046	-0,114
	EQ.x	-10,814	-1,74E-17	-9,03E-16
	EQ.y	-2,2	-2,539	-4,988
3	B.Mati	-4,034	1,085	60,065
	LIVE	-0,244	0,043	2,865
	WIND.KA	-1,321	-0,0003177	1,53
	WIND.KI	1,493	0,0002375	-1,717
	EQ.x	-6,605	0,215	10,936
	EQ.y	-1,346	-2,922	-7,726
4	B.Mati	1,937	-1,07	94,496
	LIVE	0,14	-0,041	5,95
	WIND.KA	-1,142	0,0005361	-0,972
	WIND.KI	0,713	-0,000711	0,544
	EQ.x	-2,237	-0,94	-7,18
	EQ.y	-0,529	-15,256	-10,046
5	B.Mati	-3,409	-0,796	104,642
	LIVE	-2,87E-16	-0,016	13,371
	WIND.KA	-1,604	-0,00002939	-0,171
	WIND.KI	1,604	-0,00002939	-0,171
	EQ.x	-9,188	-2,08E-17	-1,34E-15
	EQ.y	-2,151	-2,847	1,118
6	B.Mati	-0,41	-1,006	73,632
	LIVE	-0,14	-0,041	5,95
	WIND.KA	-0,713	-0,000711	0,544
	WIND.KI	1,142	0,0005361	-0,972
	EQ.x	-2,237	0,94	7,18
	EQ.y	-0,532	-14,036	-6,258
7	B.Mati	1,91	0,879	94,146
	LIVE	0,14	0,041	5,95
	WIND.KA	-1,142	-0,0005361	-0,972
	WIND.KI	0,713	0,000711	0,544
	EQ.x	-2,357	-0,946	-6,608
	EQ.y	-0,61	-15,257	6,628
8	B.Mati	-1,846	0,46	105,383
	LIVE	-2,71E-16	0,016	13,371
	WIND.KA	-1,604	0,00002939	-0,171
	WIND.KI	1,604	0,00002939	-0,171
	EQ.x	-9,821	-2,08E-17	-1,33E-15
	EQ.y	-2,561	-2,847	-1,118

9	B.Mati	-0,843	0,952	83,501
	LIVE	-0,14	0,041	5,95
	WIND.KA	-0,713	0,000711	0,544
	WIND.KI	1,142	-0,0005361	-0,972
	EQ.x	-2,357	0,946	6,608
	EQ.y	-0,606	-14,035	9,676
10	B.Mati	4,934	-1,064	61,172
	LIVE	0,244	-0,043	2,865
	WIND.KA	-1,493	-0,0002375	-1,717
	WIND.KI	1,321	0,0003177	1,53
	EQ.x	-8,081	-0,217	-11,845
	EQ.y	-2,301	-3,202	7,138
11	B.Mati	0,446	-0,825	89,904
	LIVE	2,55E-16	-0,083	5,835
	WIND.KA	-1,945	0,000046	-0,114
	WIND.KI	1,945	0,000046	-0,114
	EQ.x	-13,219	-1,04E-17	-3,53E-15
	EQ.y	-3,757	-2,539	4,988
12	B.Mati	-4,169	-1,05	60,234
	LIVE	-0,244	-0,043	2,865
	WIND.KA	-1,321	0,0003177	1,53
	WIND.KI	1,493	-0,0002375	-1,717
	EQ.x	-8,081	0,217	11,845
	EQ.y	-2,295	-2,922	13,373



1 Gempa Statik Ekuivalen

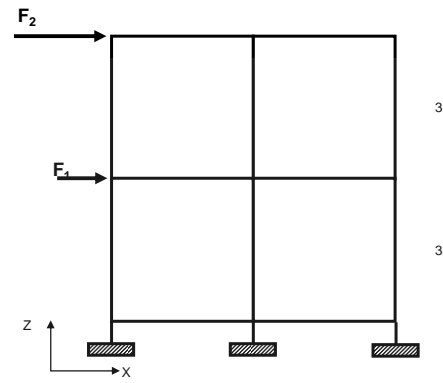
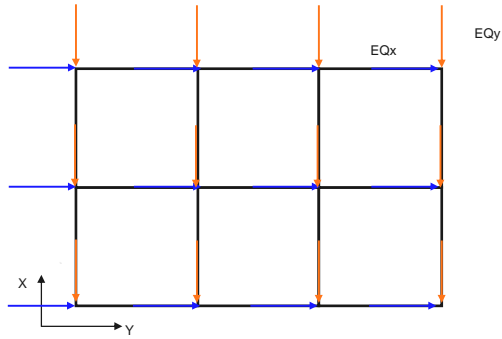


Wilayah Gempa	=	3
h	=	6
T	=	0,280240446
C	=	0,55 Didapat Dari Grafik Gbr.2
I	=	1 Keutamaan Bangunan
R	=	3,5 Dari tabel 2
Wt	=	648,01
V	=	101,8301429
W1	=	576,551
W2	=	71,459
F1	=	81,60222427
F2	=	20,22791859
(V)	=	101,8301429

Pembagian Beban Gempa Pada Kolom		
Frame	P	F1
Text	KN	KN
18	-36,258	4,566
19	-60,793	7,656
20	-35,658	4,490
21	+58,009	7,305
22	-74,581	9,392
23	-47,372	5,965
24	-57,613	7,255
25	-87,625	11,034
26	-57,458	7,236
27	-36,223	4,561
28	-60,748	7,650
29	-35,672	4,492
	-648,01	81,602

Pembagian Beban Gempa Pada Kolom		
Frame	P	F2
Text	KN	KN
47	-4,119	1,166
48	-6,044	1,711
49	-4,106	1,162
50	-6,086	1,723
51	-9,297	2,632
52	-6,084	1,722
53	-6,096	1,726
54	-9,261	2,622
55	-6,088	1,723
56	-4,121	1,167
57	-6,047	1,712
58	-4,11	1,163
	-71,459	20,228

1 Gempa Statik Ekuivalen



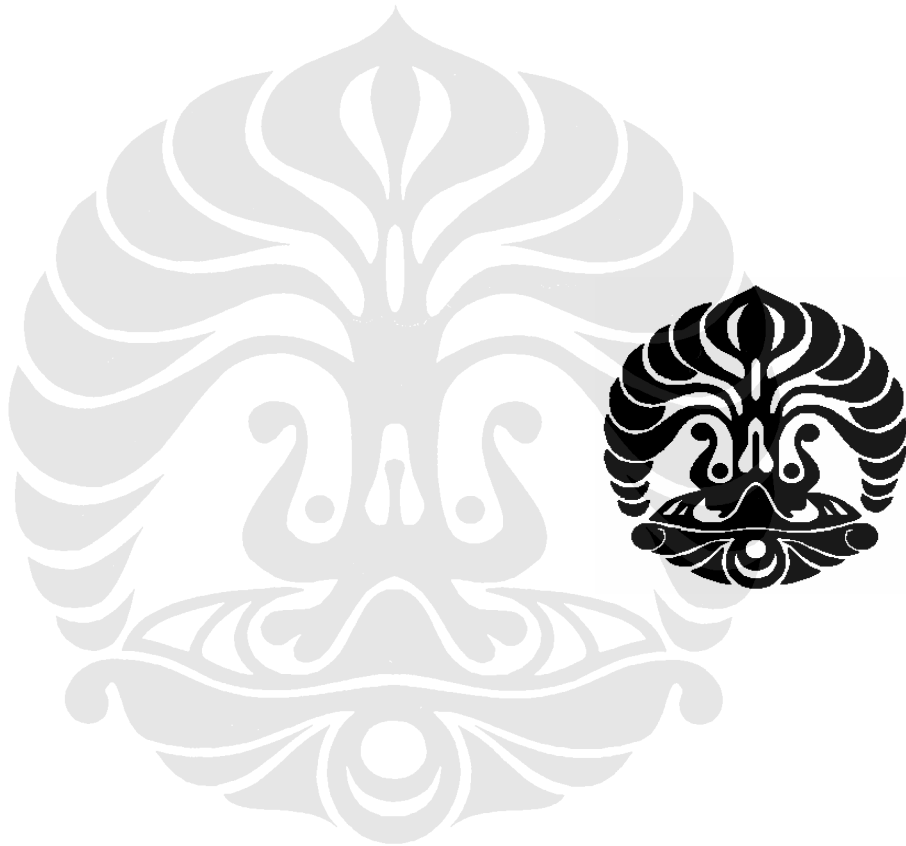
Wilayah Gempa	=	3
h	=	6
T	=	0,280240446
C	=	0,55 Didapat Dari Grafik Gbr.2
I	=	1 Keutamaan Bangunan
R	=	3,5 Dari tabel 2
Wt	=	648,01
V	=	101,8301429
W1	=	576,551
W2	=	71,459
F1	=	81,60222427
F2	=	20,22791859
(V)	=	101,8301429

Pembagian Beban Gempa Pada Kolom		
Frame	P	F1
Text	KN	KN
18	-36,258	4,566
19	-60,793	7,656
20	-35,658	4,490
21	-58,009	7,305
22	-74,581	9,392
23	-47,372	5,965
24	-57,613	7,255
25	-87,625	11,034
26	-57,458	7,236
27	-36,223	4,561
28	-60,748	7,650
29	-35,672	4,492
	-648,01	81,602

Pembagian Beban Gempa Pada Kolom		
Frame	P	F2
Text	KN	KN
47	-4,119	1,166
48	-6,044	1,711
49	-4,106	1,162
50	-6,086	1,723
51	-9,297	2,632
52	-6,084	1,722
53	-6,096	1,726
54	-9,261	2,622
55	-6,088	1,723
56	-4,121	1,167
57	-6,047	1,712
58	-4,11	1,163
	-71,459	20,228

LAMPIRAN B1

Analisa Kekuatan Struktur dan Daya Layan Pada Elemen Bangunan Rumah Tinggal (Sloof, Kolom, Balok dan Ring Balok)



Penulangan Rumah Tinggal 1 Lantai dengan menggunakan bekisting Baja

		Sloof		Ring Balok		Kolom	
		15x20		15x15		20x20	
Tulangan Lentur	Tulangan Atas						
	Diameter Tulangan	D 12	mm	D 10	mm	D 12	mm
	Luas Tulangan Max	455	mm ²	127	mm ²	574	mm ²
	Jumlah Tulangan	5	bh	2	bh	6	bh
	Tulangan Bawah						
	Diameter Tulangan	D 12	mm	D 10	mm		
Tulangan Geser	Diameter Tulangan	D 8	mm	D 6	mm	D 6	mm
	Luas Tulangan Max	199	mm ² /m	0	mm ² /m	0	mm ² /m
	Jarak Tulangan	200	mm	200	bh	200	bh

Penulangan Rumah Tinggal 2 Lantai dengan menggunakan bekisting Baja

		Sloof		Balok		Ring Balok		Kolom Lt.1		Kolom Lt.2	
		15x20		15x20		15x15		20x20		20x20	
Tulangan Lentur	Tulangan Atas										
	Diameter Tulangan	D 12	mm	D 16	mm	D 10	mm	D 16	mm	D 12	mm
	Luas Tulangan Max	546	mm ²	617	mm ²	61	mm ²	1654	mm ²	350	mm ²
	Jumlah Tulangan	5	bh	4	bh	1	bh	9	bh	4	bh
	Tulangan Bawah										
	Diameter Tulangan	D 12	mm	D 16	mm	D 10	mm				
Tulangan Geser	Diameter Tulangan	D 8	mm	D 8	mm	D 8	mm	D 8	mm	D 6	mm
	Luas Tulangan Max /m	203	mm ²	227	mm ²	0	mm ²	125	mm ²	0	mm ²
	Jarak Tulangan	200	mm	200	mm	200	mm	150	mm	200	mm

Penulangan Rumah Tinggal 1 Lantai dengan menggunakan bekisting Cara Tradisional

		Sloof		Ring Balok		Kolom	
		10x25		10x10		10x20	
Tulangan Lentur	Tulangan Tarik						
	Diameter Tulangan	D 12	mm	D 10	mm	D 12	mm
	Luas Tulangan Max	420	mm ²	112	mm ²	618	mm ²
	Jumlah Tulangan	4	bh	2	bh	6	bh
	Tulangan tekan						
	Diameter Tulangan	D 12	mm	D 10	mm	-	-
Tulangan Geser	Diameter Tulangan	D 8	mm	D 6	mm	D 6	mm
	Luas Tulangan Max /m	125	mm ²	0	mm ²	0	mm ²
	Jarak Tulangan	200	mm	200	bh	200	bh

Penulangan Rumah Tinggal 2 Lantai dengan menggunakan bekisting Cara Tradisional

		Sloof		Balok		Ring Balok		Kolom Lt.1		Kolom Lt.2	
		10x25		10x30		10x10		10x40		10x20	
Tulangan Lentur	Tulangan tarik										
	Diameter Tulangan	D 12	mm	D 12	mm	D 10	mm	D 16	mm	D 12	mm
	Luas Tulangan Max	639	mm ²	626	mm ²	109	mm ²	2155	mm ²	392	mm ²
	Jumlah Tulangan	6	bh	6	bh	2	bh	11	bh	4	bh
	Tulangan tekan										
	Diameter Tulangan	D 12	mm	D 12	mm	D 10	mm				
Tulangan Geser	Diameter Tulangan	D 8	mm	D 6	mm	D 6	mm	D 8	mm	D 6	mm
	Luas Tulangan Max /m	188	mm ²	235	mm ²	0	mm ²	125	mm ²	0	mm ²
	Jarak Tulangan	200	mm	200	mm	200	mm	200	mm	200	mm

Hasil Perhitungan Struktur (Gaya dalam dan lendutan maksimum)

Rumah Tinggal Dengan Bekisting Baja 1 lantai

	Pu	Vu-x	Vu-y	Mu-x	Mu-y	δu-x	δu-y
	KN	KN	KN	KN-m	KN-m	cm	cm
Sloof	0	25,022	0,032	0,0428	14,3512	0,109134	0,000015
Ring Balok	1,421E-14	2,995	2,262E-16	5,718E-16	2,5305	0,012667	0
Kolom	23,116	3,531	2,628	5,5942	8,6458	0,062445	0,010024

Rumah Tinggal Dengan Bekisting Baja 2 lantai

	Pu	Vu-x	Vu-y	Mu-x	Mu-y	δu-x	δu-y
	KN	KN	KN	KN-m	KN-m	cm	cm
Kolom It.1	151,705	14,547	12,95	20,003	22,1749	0,009837	0,001369
Kolom It.2	28,341	5,49	4,791	11,9728	13,8497	0,051381	0,00275
Ring Balok	0	3,701	8,882E-16	2,254E-15	2,4755	0,018274	0
Balok	0	37,618	1,81E-15	2,731E-15	21,8402	0,161286	0
Sloof	0	27,265	0,138	0,1859	18,3707	0,096814	0

Rumah Tinggal Dengan Bekisting Cara Tradisional 1 lantai

	Pu	Vu-x	Vu-y	Mu-x	Mu-y	δu-x	δu-y
	KN	KN	KN	KN-m	KN-m	cm	cm
Sloof	0	27,13	6,794E-05	9,288E-05	16,7073	0,124479	0
Ring Balok	0	1,587	1,214E-18	3,036E-18	1,0335	0,057481	0
Kolom	16,086	2,385	0,7	1,5565	5,4123	0,14733	0,027877

Rumah Tinggal Dengan Bekisting Cara Tradisional 2 lantai

	Pu	Vu-x	Vu-y	Mu-x	Mu-y	δu-x	δu-y
	KN	KN	KN	KN-m	KN-m	cm	cm
Kolom It.1	125,774	14,859	16,829	28,8802	26,0565	0,018647	0,001288
Kolom It.2	16,202	1,879	1,308	3,5401	4,7865	0,072924	0,003994
Ring Balok	0	1,589	1,11E-16	2,776E-16	0,883	0,075247	0
Balok	0	33,982	7,216E-17	4,774E-16	25,8932	0,104299	0
Sloof	0	22,26	0,034	0,0451	17,4504	0,087714	0

RT Baja 2 Lantai

Kolom lt.1

Arah - X

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D D 16} = 1005,30965 \text{ nr}$$

$$A_s' = 4 \text{ D D 16} = 804,247719 \text{ nr}$$

$$A_{st} = 1809,557368 \text{ nr}$$

$$A_g = 40000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 200 \text{ mm}$$

$$h = 200 \text{ mm}$$

$$d' = 36 \text{ mm}$$

$$d = 164 \text{ mm}$$

D 8 - 150

$$A_v = 50,265$$

$$V_c = 36,4335 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 27,325 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$14,547 \leq 20,493845 \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,009837 \leq 2,5714286 \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 98,4$$

$$\epsilon_b = 0,0031$$

$$\epsilon_s' = 0,0019$$

$$a = 83,64$$

$$C_c = 391,017$$

$$C_s' = 302,900$$

$$T_s = 402,124$$

$$P_n = 291,793$$

$$X_{Cc} = 122,18$$

$$X_{Cs'} = 128$$

$$X_{Pn} = 64$$

$$M_n = 67,871$$

$$P_u \leq \phi P_n$$

$$151,705 \leq 233,43435 \text{ok!}$$

$$M_u \leq \phi M_n$$

$$22,1749 \leq 54,2967065 \text{ok!}$$

Arah - Y

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D D 16} = 1005,30965 \text{ nr}$$

$$A_s' = 4 \text{ D D 16} = 804,247719 \text{ nr}$$

$$A_{st} = 1809,557368 \text{ nr}$$

$$A_g = 40000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 200 \text{ mm}$$

$$h = 200 \text{ mm}$$

$$d' = 36 \text{ mm}$$

$$d = 164 \text{ mm}$$

D 8 - 150

$$A_v = 50,265$$

$$V_c = 36,4335 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 27,325 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$12,95 \leq 20,493845 \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,001369 \leq 2,5714286 \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 98,4$$

$$\epsilon_b = 0,0031$$

$$\epsilon_s' = 0,0019$$

$$a = 83,64$$

$$C_c = 391,017$$

$$C_s' = 302,900$$

$$T_s = 402,124$$

$$P_n = 291,793$$

$$X_{Cc} = 122,18$$

$$X_{Cs'} = 128$$

$$X_{Pn} = 64$$

$$M_n = 67,871$$

$$P_u \leq \phi P_n$$

$$151,705 \leq 233,43435 \text{ok!}$$

$$M_u \leq \phi M_n$$

$$20,003 \leq 54,2967065 \text{ok!}$$

Kolom It.2

Arah - X

$f_c' = 27,5$ MPa
 $f_y = 400$ MPa
 $E_s = 200000$ MPa

$A_s = 2 \text{ D D } 12 = 226,194671$ m²
 $A_s' = 2 \text{ D D } 12 = 226,194671$ m²
 $A_{st} = 452,3893421$ m²
 $A_g = 40000$ m²

$L = 3000$ mm
 $b = 200$ mm
 $h = 200$ mm
 $d' = 32$ mm
 $d = 168$ mm

D 6 - 200

$A_v = 28,274$
 $V_c = 30,21629$ kN
 $V_s = 0,000$ kN
 $V_n = 22,662$ kN
 $V_u \leq \phi V_n$

$\epsilon_{Cu} = 0,003$
 $\epsilon_s = 0,002$
 $C = 100,8$
 $\epsilon_b = 0,0030$
 $\epsilon_s' = 0,0020$

$a = 85,68$ $X_{Cc} = 125,16$
 $C_c = 400,554$ $X_{Cs}' = 136$
 $C_s' = 85,191$ $X_{Pn} = 68$
 $T_s = 90,478$
 $P_n = 395,267$ $M_n = 34,841$

$1,879 \leq 16,996662 \dots \dots \dots \text{ok!}$

$P_u \leq \phi P_n$
 $16,202 \leq 316,21336 \dots \dots \dots \text{ok!}$

$\delta_u \leq \delta_n$
 $0,072924 \leq 2,5714286 \dots \dots \dots \text{ok!}$

$M_u \leq \phi M_n$
 $3,5401 \leq 27,8728963 \dots \dots \dots \text{ok!}$

Arah - Y

$f_c' = 27,5$ MPa
 $f_y = 400$ MPa
 $E_s = 200000$ MPa

$A_s = 2 \text{ D D } 12 = 226,194671$ m²
 $A_s' = 2 \text{ D D } 12 = 226,194671$ m²
 $A_{st} = 452,3893421$ m²
 $A_g = 40000$ m²

$L = 3000$ mm
 $b = 200$ mm
 $h = 200$ mm
 $d' = 32$ mm
 $d = 168$ mm

D 6 - 200

$A_v = 28,274$
 $V_c = 30,21629$ kN
 $V_s = 0,000$ kN
 $V_n = 22,662$ kN
 $V_u \leq \phi V_n$

$\epsilon_{Cu} = 0,003$
 $\epsilon_s = 0,002$
 $C = 100,8$
 $\epsilon_b = 0,0030$
 $\epsilon_s' = 0,0020$

$a = 85,68$ $X_{Cc} = 125,16$
 $C_c = 400,554$ $X_{Cs}' = 136$
 $C_s' = 85,191$ $X_{Pn} = 68$
 $T_s = 90,478$
 $P_n = 395,267$ $M_n = 34,841$

$1,308 \leq 16,996662 \dots \dots \dots \text{ok!}$

$P_u \leq \phi P_n$
 $16,202 \leq 316,21336 \dots \dots \dots \text{ok!}$

$\delta_u \leq \delta_n$
 $0,003994 \leq 2,5714286 \dots \dots \dots \text{ok!}$

$M_u \leq \phi M_n$
 $4,7865 \leq 27,8728963 \dots \dots \dots \text{ok!}$

Ring balok J61

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 1 \text{ D D } 10 = 78,5398163 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 150 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D D } 8 & d' &= 33 \text{ mm} \\
 & & & & d &= 117 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 D \ 8 & - 200 \\
 A_v &= 50,265 & a &= 8,95997905 \\
 V_c &= 15,339 \text{ kN} & M_n &= 3,53492038 \text{ kNm} \\
 V_s &= 0,000 \text{ kN} \\
 V_n &= 11,504 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 1,589 &\leq 8,6280915 \dots\dots\dots\text{ok!} & 0,883 &\leq 2,82793631 \dots\dots\dots\text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,075247 &\leq 1,4583333 \dots\dots\dots\text{ok!}
 \end{aligned}$$

Balok RT Baja 1 Lantai

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 4 \text{ D D } 16 = 804,247719 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 200 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D D } 8 & d' &= 36 \text{ mm} \\
 & & & & d &= 164 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 D \ 8 & - 200 \\
 A_v &= 50,265 & a &= 91,7501854 \\
 V_c &= 21,501 \text{ kN} & M_n &= 38,0006749 \text{ kNm} \\
 V_s &= 32,974 \text{ kN} \\
 V_n &= 40,856 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 33,982 &\leq 30,64204 \dots\dots\dots\text{red} & 25,8932 &\leq 30,4005399 \dots\dots\dots\text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,104299 &\leq 1,4583333 \dots\dots\dots\text{ok!}
 \end{aligned}$$

Sloof J93

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 5 \text{ D D } 12 = 565,486678 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 200 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D D } 8 & d' &= 34 \text{ mm} \\
 & & & & d &= 166 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 D \ 8 & - 200 \\
 A_v &= 50,265 & a &= 64,5118491 \\
 V_c &= 21,763 \text{ kN} & M_n &= 30,2521971 \text{ kNm} \\
 V_s &= 33,376 \text{ kN} \\
 V_n &= 41,354 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 22,26 &\leq 31,015723 \dots\dots\dots\text{ok!} & 17,4504 &\leq 24,2017577 \dots\dots\dots\text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,087714 &\leq 1,4583333 \dots\dots\dots\text{ok!}
 \end{aligned}$$

RT Cara Tradisional 2 Lantai

Kolom lt.1

Arah - X

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D D } 16 = 1005,30965 \text{ nr}$$

$$A_s' = 4 \text{ D D } 16 = 804,247719 \text{ nr}$$

$$A_{st} = 1809,557368 \text{ nr}$$

$$A_g = 40000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 100 \text{ mm}$$

$$h = 400 \text{ mm}$$

$$d' = 36 \text{ mm}$$

$$d = 364 \text{ mm}$$

D 8 - 200

$$A_v = 50,265$$

$$V_c = 38,95915 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 29,219 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$14,859 \leq 21,914522 \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,018647 \leq 2,5714286 \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 218,4$$

$$\epsilon_b = 0,0025$$

$$\epsilon_s' = 0,0025$$

$$a = 185,64$$

$$C_c = 433,9335$$

$$C_s' = 302,900$$

$$T_s = 402,124$$

$$P_n = 334,709$$

$$P_u \leq \phi P_n$$

$$125,774 \leq 267,76755 \text{ok!}$$

$$M_u \leq \phi M_n$$

$$26,0565 \leq 129,706298 \text{ok!}$$

$$X_{Cc} = 271,18$$

$$X_{Cs'} = 328$$

$$X_{Pn} = 164$$

$$M_n = 162,133$$

Arah - Y

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D D } 16 = 1005,30965 \text{ nr}$$

$$A_s' = 4 \text{ D D } 16 = 804,247719 \text{ nr}$$

$$A_{st} = 1809,557368 \text{ nr}$$

$$A_g = 40000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 400 \text{ mm}$$

$$h = 100 \text{ mm}$$

$$d' = 36 \text{ mm}$$

$$d = 64 \text{ mm}$$

D 8 - 200

$$A_v = 50,265$$

$$V_c = 27,39984 \text{ kN}$$

$$V_s = 12,868 \text{ kN}$$

$$V_n = 30,201 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$16,829 \leq 22,65064 \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,001288 \leq 2,5714286 \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 38,4$$

$$\epsilon_b = 0,0048$$

$$\epsilon_s' = 0,0002$$

$$a = 32,64$$

$$C_c = 305,184$$

$$C_s' = 302,900$$

$$T_s = 402,124$$

$$P_n = 205,960$$

$$P_u \leq \phi P_n$$

$$125,774 \leq 164,76795 \text{ok!}$$

$$M_u \leq \phi M_n$$

$$28,8802 \leq 16,1191427 \text{red}$$

$$X_{Cc} = 47,68$$

$$X_{Cs'} = 28$$

$$X_{Pn} = 14$$

$$M_n = 20,149$$

Kolom It.2

Arah - X

$f_c' = 27,5$ MPa
 $f_y = 400$ MPa
 $E_s = 200000$ MPa

$A_s = 2 \text{ D } 12 = 226,194671$ m²
 $A_s' = 2 \text{ D } 12 = 226,194671$ m²
 $A_{st} = 452,3893421$ m²
 $A_g = 20000$ m²

$L = 3000$ mm
 $b = 100$ mm
 $h = 200$ mm
 $d' = 32$ mm
 $d = 168$ mm

D 6 - 200

$A_v = 28,274$
 $V_c = 15,53296$ kN
 $V_s = 0,000$ kN
 $V_n = 11,650$ kN
 $V_u \leq \phi V_n$

$\epsilon_{Cu} = 0,003$
 $\epsilon_s = 0,002$
 $C = 100,8$
 $\epsilon_b = 0,0030$
 $\epsilon_s' = 0,0020$

$a = 85,68$
 $C_c = 200,277$
 $C_s' = 85,191$
 $T_s = 90,478$
 $P_n = 194,990$
 $X_{Cc} = 125,16$
 $X_{Cs}' = 136$
 $X_{Pn} = 68$
 $M_n = 23,393$

$1,879 \leq 8,7372922 \dots\dots\dots\text{ok!}$

$P_u \leq \phi P_n$
 $16,202 \leq 155,99176 \dots\dots\dots\text{ok!}$

$\delta_u \leq \delta_n$
 $0,072924 \leq 2,5714286 \dots\dots\dots\text{ok!}$

$M_u \leq \phi M_n$
 $3,5401 \leq 18,7146296 \dots\dots\dots\text{ok!}$

Arah - Y

$f_c' = 27,5$ MPa
 $f_y = 400$ MPa
 $E_s = 200000$ MPa

$A_s = 2 \text{ D } 12 = 226,194671$ m²
 $A_s' = 2 \text{ D } 12 = 226,194671$ m²
 $A_{st} = 452,3893421$ m²
 $A_g = 20000$ m²

$L = 3000$ mm
 $b = 200$ mm
 $h = 100$ mm
 $d' = 32$ mm
 $d = 68$ mm

D 6 - 200

$A_v = 28,274$
 $V_c = 12,5743$ kN
 $V_s = 0,000$ kN
 $V_n = 9,431$ kN
 $V_u \leq \phi V_n$

$\epsilon_{Cu} = 0,003$
 $\epsilon_s = 0,002$
 $C = 40,8$
 $\epsilon_b = 0,0044$
 $\epsilon_s' = 0,0006$

$a = 34,68$
 $C_c = 162,129$
 $C_s' = 85,191$
 $T_s = 90,478$
 $P_n = 156,842$
 $X_{Cc} = 50,66$
 $X_{Cs}' = 36$
 $X_{Pn} = 18$
 $M_n = 8,457$

$1,308 \leq 7,0730461 \dots\dots\dots\text{ok!}$

$P_u \leq \phi P_n$
 $16,202 \leq 125,47336 \dots\dots\dots\text{ok!}$

$\delta_u \leq \delta_n$
 $0,003994 \leq 2,5714286 \dots\dots\dots\text{ok!}$

$M_u \leq \phi M_n$
 $4,7865 \leq 6,765732 \dots\dots\dots\text{ok!}$

Ring balok

$$\begin{array}{lcl}
 f'c & = & \boxed{27,5} \text{ MPa} \\
 f_y & = & \boxed{400} \text{ MPa} \\
 E_s & = & \boxed{200000} \text{ MPa} \\
 A_s & = & \boxed{2 \text{ D } \text{ D } 10} = \boxed{157,079633} \pi \\
 A_v & = & \boxed{\text{D } \text{ D } 10} \\
 b & = & \boxed{100} \text{ mm} \\
 h & = & \boxed{100} \text{ mm} \\
 d' & = & \boxed{35} \text{ mm} \\
 d & = & \boxed{65} \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 10 & - & 200 \\
 A_v & = & 78,540 \qquad a = 26,8799371 \\
 V_c & = & 5,681 \text{ kN} \qquad M_n = 3,23961232 \text{ kNm} \\
 V_s & = & 0,000 \text{ kN} \\
 V_n & = & 4,261 \text{ kN}
 \end{array}$$

$$\begin{array}{lcl}
 V_u \leq \phi V_n & & M_u \leq \phi M_n \\
 \boxed{1,589} \leq 3,1955895 \dots\dots\dots\text{ok!} & & \boxed{0,883} \leq 2,59168986 \dots\dots\dots\text{ok!} \\
 \delta_u \leq \delta_n & & \\
 \boxed{0,075247} \leq 1,4583333 \dots\dots\dots\text{ok!} & &
 \end{array}$$

Balok

$$\begin{array}{lcl}
 f'c & = & \boxed{27,5} \text{ MPa} \\
 f_y & = & \boxed{400} \text{ MPa} \\
 E_s & = & \boxed{200000} \text{ MPa} \\
 A_s & = & \boxed{6 \text{ D } \text{ D } 12} = \boxed{678,584013} \pi \\
 A_v & = & \boxed{\text{D } \text{ D } 10} \\
 b & = & \boxed{100} \text{ mm} \\
 h & = & \boxed{300} \text{ mm} \\
 d' & = & \boxed{36} \text{ mm} \\
 d & = & \boxed{264} \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 10 & - & 200 \\
 A_v & = & 78,540 \qquad a = 116,121328 \\
 V_c & = & 23,074 \text{ kN} \qquad M_n = 55,8988564 \text{ kNm} \\
 V_s & = & 82,938 \text{ kN} \\
 V_n & = & 79,509 \text{ kN}
 \end{array}$$

$$\begin{array}{lcl}
 V_u \leq \phi V_n & & M_u \leq \phi M_n \\
 \boxed{33,982} \leq 59,63166 \dots\dots\dots\text{ok!} & & \boxed{25,8932} \leq 44,7190851 \dots\dots\dots\text{ok!} \\
 \delta_u \leq \delta_n & & \\
 \boxed{0,104299} \leq 1,4583333 \dots\dots\dots\text{ok!} & &
 \end{array}$$

Sloof

$$\begin{array}{lcl}
 f'c & = & \boxed{27,5} \text{ MPa} \\
 f_y & = & \boxed{400} \text{ MPa} \\
 E_s & = & \boxed{200000} \text{ MPa} \\
 A_s & = & \boxed{6 \text{ D } \text{ D } 12} = \boxed{678,584013} \pi \\
 A_v & = & \boxed{\text{D } \text{ D } 10} \\
 b & = & \boxed{100} \text{ mm} \\
 h & = & \boxed{250} \text{ mm} \\
 d' & = & \boxed{36} \text{ mm} \\
 d & = & \boxed{214} \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 10 & - & 200 \\
 A_v & = & 78,540 \qquad a = 116,121328 \\
 V_c & = & 18,704 \text{ kN} \qquad M_n = 42,3271761 \text{ kNm} \\
 V_s & = & 67,230 \text{ kN} \\
 V_n & = & 64,450 \text{ kN}
 \end{array}$$

$$\begin{array}{lcl}
 V_u \leq \phi V_n & & M_u \leq \phi M_n \\
 \boxed{22,26} \leq 48,337785 \dots\dots\dots\text{ok!} & & \boxed{17,4504} \leq 33,8617409 \dots\dots\dots\text{ok!} \\
 \delta_u \leq \delta_n & & \\
 \boxed{0,087714} \leq 1,4583333 \dots\dots\dots\text{ok!} & &
 \end{array}$$

RT Baja 1 Lantai

Kolom lt.1

Arah - X

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D } 12 = 565,486678 \text{ nr}$$

$$A_s' = 4 \text{ D } 12 = 452,389342 \text{ nr}$$

$$A_{st} = 1017,87602 \text{ nr}$$

$$A_g = 40000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 200 \text{ mm}$$

$$h = 200 \text{ mm}$$

$$d' = 32 \text{ mm}$$

$$d = 168 \text{ mm}$$

$$D_6 - 200$$

$$A_v = 28,274$$

$$V_c = 30,57886 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 22,934 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$3,531 \leq 17,200609 \dots \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,062445 \leq 2,5714286 \dots \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 100,8$$

$$\epsilon_b = 0,0030$$

$$\epsilon_s' = 0,0020$$

$$a = 85,68$$

$$C_c = 400,554$$

$$C_s' = 170,381$$

$$T_s = 226,195$$

$$P_n = 344,740$$

$$P_u \leq \phi P_n$$

$$23,116 \leq 275,792372$$

$$X_{Cc} = 125,16$$

$$X_{Cs'} = 136$$

$$X_{Pn} = 68$$

$$M_n = 49,863$$

$$M_u \leq \phi M_n$$

$$8,6458 \leq 39,8902572$$

Arah - Y

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D } 12 = 565,486678 \text{ nr}$$

$$A_s' = 4 \text{ D } 12 = 452,389342 \text{ nr}$$

$$A_{st} = 1017,87602 \text{ nr}$$

$$A_g = 40000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 200 \text{ mm}$$

$$h = 200 \text{ mm}$$

$$d' = 32 \text{ mm}$$

$$d = 168 \text{ mm}$$

$$D_6 - 200$$

$$A_v = 28,274$$

$$V_c = 30,57886 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 22,934 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$2,628 \leq 17,200609 \dots \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,010024 \leq 2,5714286 \dots \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 100,8$$

$$\epsilon_b = 0,0030$$

$$\epsilon_s' = 0,0020$$

$$a = 85,68$$

$$C_c = 400,554$$

$$C_s' = 170,381$$

$$T_s = 226,195$$

$$P_n = 344,740$$

$$P_u \leq \phi P_n$$

$$23,116 \leq 275,792372 \dots \text{ok!}$$

$$M_u \leq \phi M_n$$

$$5,5942 \leq 39,8902572 \dots \text{ok!}$$

$$X_{Cc} = 125,16$$

$$X_{Cs'} = 136$$

$$X_{Pn} = 68$$

$$M_n = 49,863$$

Ring balok

f_c'	=	<input type="text" value="27,5"/> MPa	A_s	=	<input type="text" value="2"/> D <input type="text" value="D 10"/>	=	<input type="text" value="157,079633"/> π	b	=	<input type="text" value="150"/> mm
f_y	=	<input type="text" value="400"/> MPa						h	=	<input type="text" value="150"/> mm
E_s	=	<input type="text" value="200000"/> MPa	A_v	=	<input type="text" value="D"/> D <input type="text" value="D 6"/>			d'	=	<input type="text" value="31"/> mm
								d	=	<input type="text" value="119"/> mm

D 6	-	200								
A_v	=	<input type="text" value="28,274"/>	a	=	<input type="text" value="17,9199581"/>					
V_c	=	<input type="text" value="15,601"/> kN	M_n	=	<input type="text" value="6,91401843"/> kNm					
V_s	=	<input type="text" value="0,000"/> kN								
V_n	=	<input type="text" value="11,701"/> kN								
V_u	\leq	ϕV_n	M_u	\leq	ϕM_n					

<input type="text" value="2,995"/>	\leq	<input type="text" value="8,7755803"/>ok!	<input type="text" value="2,5305"/>	\leq	<input type="text" value="5,53121474"/>ok!
δ_u	\leq	δ_n					
<input type="text" value="0,012667"/>	\leq	<input type="text" value="1,4583333"/>ok!				

Sloof

f_c'	=	<input type="text" value="27,5"/> MPa	A_s	=	<input type="text" value="5"/> D <input type="text" value="D 12"/>	=	<input type="text" value="565,486678"/> π	b	=	<input type="text" value="150"/> mm
f_y	=	<input type="text" value="400"/> MPa						h	=	<input type="text" value="200"/> mm
E_s	=	<input type="text" value="200000"/> MPa	A_v	=	<input type="text" value="D"/> D <input type="text" value="D 8"/>			d'	=	<input type="text" value="34"/> mm
								d	=	<input type="text" value="166"/> mm

D 8	-	200								
A_v	=	<input type="text" value="50,265"/>	a	=	<input type="text" value="64,5118491"/>					
V_c	=	<input type="text" value="21,763"/> kN	M_n	=	<input type="text" value="30,2521971"/> kNm					
V_s	=	<input type="text" value="33,376"/> kN								
V_n	=	<input type="text" value="41,354"/> kN								
V_u	\leq	ϕV_n	M_u	\leq	ϕM_n					

<input type="text" value="25,022"/>	\leq	<input type="text" value="31,015723"/>ok!	<input type="text" value="14,3512"/>	\leq	<input type="text" value="24,2017577"/>ok!
δ_u	\leq	δ_n					
<input type="text" value="0,109134"/>	\leq	<input type="text" value="1,4583333"/>ok!				

RT Cara Tradisional 1 Lantai

Kolom lt.1

Arah - X

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D D } 12 = 565,486678 \text{ nr}$$

$$A_s' = 4 \text{ D D } 12 = 452,389342 \text{ nr}$$

$$A_{st} = 1017,87602 \text{ nr}$$

$$A_g = 20000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 100 \text{ mm}$$

$$h = 200 \text{ mm}$$

$$d' = 32 \text{ mm}$$

$$d = 168 \text{ mm}$$

$$D \ 6 \ - \ 200$$

$$A_v = 28,274$$

$$V_c = 15,52688 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 11,645 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$2,385 \leq 8,7338705 \dots \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,14733 \leq 2,5714286 \dots \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 100,8$$

$$\epsilon_b = 0,0030$$

$$\epsilon_s' = 0,0020$$

$$a = 85,68$$

$$C_c = 200,277$$

$$C_s' = 170,381$$

$$T_s = 226,195$$

$$P_n = 144,463$$

$$P_u \leq \phi P_n$$

$$16,086 \leq 115,570772 \dots \text{ok!}$$

$$M_u \leq \phi M_n$$

$$5,4123 \leq 30,7319906 \dots \text{ok!}$$

$$X_{Cc} = 125,16$$

$$X_{Cs'} = 136$$

$$X_{Pn} = 68$$

$$M_n = 38,415$$

Arah - Y

$$f_c' = 27,5 \text{ MPa}$$

$$f_y = 400 \text{ MPa}$$

$$E_s = 200000 \text{ MPa}$$

$$A_s = 5 \text{ D D } 12 = 565,486678 \text{ nr}$$

$$A_s' = 4 \text{ D D } 12 = 452,389342 \text{ nr}$$

$$A_{st} = 1017,87602 \text{ nr}$$

$$A_g = 20000 \text{ nr}$$

$$L = 3000 \text{ mm}$$

$$b = 200 \text{ mm}$$

$$h = 100 \text{ mm}$$

$$d' = 32 \text{ mm}$$

$$d = 68 \text{ mm}$$

$$D \ 6 \ - \ 200$$

$$A_v = 28,274$$

$$V_c = 12,56938 \text{ kN}$$

$$V_s = 0,000 \text{ kN}$$

$$V_n = 9,427 \text{ kN}$$

$$V_u \leq \phi V_n$$

$$0,7 \leq 7,0702761 \dots \text{ok!}$$

$$\delta_u \leq \delta_n$$

$$0,027877 \leq 2,5714286 \dots \text{ok!}$$

$$\epsilon_{Cu} = 0,003$$

$$\epsilon_s = 0,002$$

$$C = 40,8$$

$$\epsilon_b = 0,0044$$

$$\epsilon_s' = 0,0006$$

$$a = 34,68$$

$$C_c = 162,129$$

$$C_s' = 170,381$$

$$T_s = 226,195$$

$$P_n = 106,315$$

$$P_u \leq \phi P_n$$

$$16,086 \leq 85,0523719 \dots \text{ok!}$$

$$M_u \leq \phi M_n$$

$$1,5565 \leq 9,94679813 \dots \text{ok!}$$

$$X_{Cc} = 50,66$$

$$X_{Cs'} = 36$$

$$X_{Pn} = 18$$

$$M_n = 12,433$$

Ring balok

f_c'	=	<input type="text" value="27,5"/>	MPa	A_s	=	<input type="text" value="2"/>	D	<input type="text" value="10"/>	=	<input type="text" value="157,079633"/>	π	b	=	<input type="text" value="100"/>	mm
f_y	=	<input type="text" value="400"/>	MPa									h	=	<input type="text" value="100"/>	mm
E_s	=	<input type="text" value="200000"/>	MPa	A_v	=	<input type="text" value="D"/>	D	<input type="text" value="6"/>				d'	=	<input type="text" value="31"/>	mm
												d	=	<input type="text" value="69"/>	mm

D 6 - 200

A_v	=	<input type="text" value="28,274"/>		a	=	<input type="text" value="26,8799371"/>	
V_c	=	<input type="text" value="6,031"/>	kN	M_n	=	<input type="text" value="3,49093973"/>	kNm

V_s = kN

V_n = kN

$V_u \leq \phi V_n$

$M_u \leq \phi M_n$

\leq ok!

\leq ok!

$\delta_u \leq \delta_n$

\leq ok!

Sloof

f_c'	=	<input type="text" value="27,5"/>	MPa	A_s	=	<input type="text" value="4"/>	D	<input type="text" value="12"/>	=	<input type="text" value="452,389342"/>	π	b	=	<input type="text" value="100"/>	mm
f_y	=	<input type="text" value="400"/>	MPa									h	=	<input type="text" value="250"/>	mm
E_s	=	<input type="text" value="200000"/>	MPa	A_v	=	<input type="text" value="D"/>	D	<input type="text" value="8"/>				d'	=	<input type="text" value="34"/>	mm
												d	=	<input type="text" value="216"/>	mm

D 8 - 200

A_v	=	<input type="text" value="50,265"/>		a	=	<input type="text" value="77,414219"/>	
V_c	=	<input type="text" value="18,879"/>	kN	M_n	=	<input type="text" value="32,0821656"/>	kNm

V_s = kN

V_n = kN

$V_u \leq \phi V_n$

$M_u \leq \phi M_n$

\leq ok!

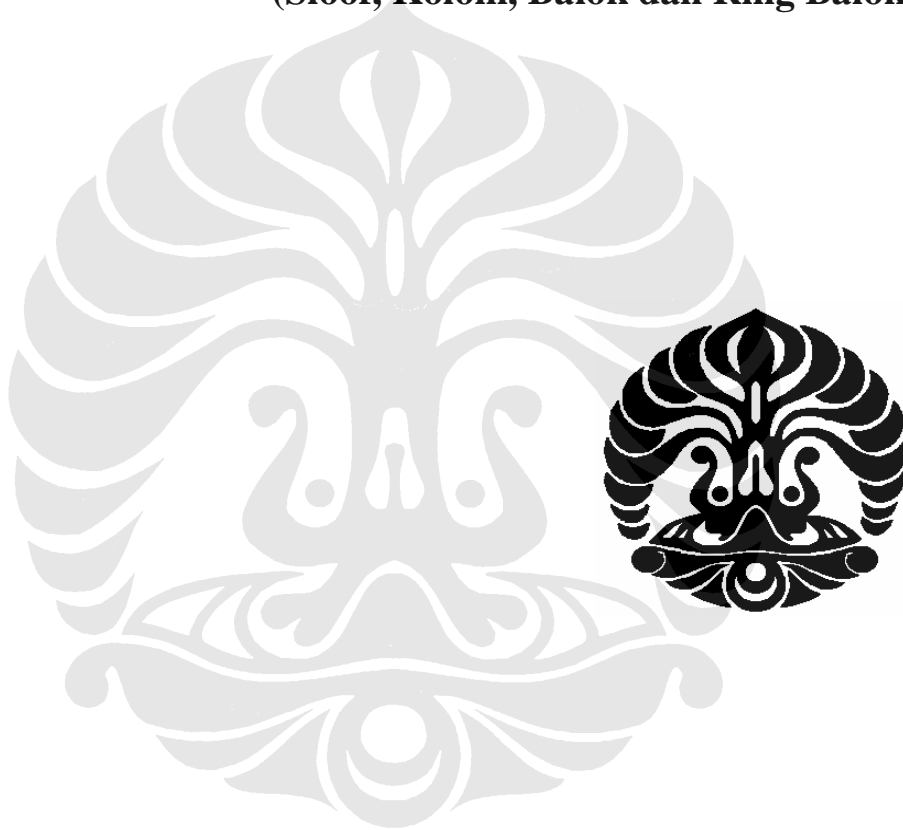
\leq ok!

$\delta_u \leq \delta_n$

\leq ok!

LAMPIRAN B2

**Perbandingan Analisa Kekuatan Struktur
dan Daya Layan Bangunan Rumah Tinggal
Pada Elemen dan Kombinasi yang sama
(Sloof, Kolom, Balok dan Ring Balok)**



Penulangan Rumah Tinggal 1 Lantai dengan menggunakan bekisting Baja

		Sloof	Ring Balok	Kolom
		15x20	15x15	20x20
Tulangan Lentur	Tulangan Atas			
	Diameter Tulangan	D 12 mm	D 10 mm	D 12 mm
	Luas Tulangan Max	455 mm ²	127 mm ²	574 mm ²
	Jumlah Tulangan	5 bh	2 bh	6 bh
	Tulangan Bawah			
	Diameter Tulangan	D 12 mm	D 10 mm	
	Luas Tulangan Max	245 mm ²	83 mm ²	
Jumlah Tulangan	3 bh	2 bh		
Tulangan Geser	Tulangan Atas			
	Diameter Tulangan	D 8 mm	D 6 mm	D 6 mm
	Luas Tulangan Max	199 mm ² /m	0 mm ² /m	0 mm ² /m
	Jarak Tulangan	200 mm	200 bh	200 bh

Penulangan Rumah Tinggal 2 Lantai dengan menggunakan bekisting Baja

		Sloof	Balok	Ring Balok	Kolom It.1	Kolom It.2
		15x20	15x20	15x15	20x20	20x20
Tulangan Lentur	Tulangan Atas					
	Diameter Tulangan	D 12 mm	D 16 mm	D 10 mm	D 16 mm	D 12 mm
	Luas Tulangan Max	546 mm ²	617 mm ²	61 mm ²	1654 mm ²	350 mm ²
	Jumlah Tulangan	5 bh	4 bh	1 bh	9 bh	4 bh
	Tulangan Bawah					
	Diameter Tulangan	D 12 mm	D 16 mm	D 10 mm		
	Luas Tulangan Max	254 mm ²	289 mm ²	40 mm ²		
Jumlah Tulangan	3 bh	2 bh	1 bh			
Tulangan Geser	Tulangan Atas					
	Diameter Tulangan	D 8 mm	D 8 mm	D 8 mm	D 8 mm	D 6 mm
	Luas Tulangan Max /m	203 mm ²	227 mm ²	0 mm ²	125 mm ²	0 mm ²
	Jarak Tulangan	200 mm	200 mm	200 mm	150 mm	200 mm

Penulangan Rumah Tinggal 1 Lantai dengan menggunakan bekisting Cara Tradisional

		Sloof		Ring Balok		Kolom	
		10x25		10x10		10x20	
Tulangan Lentur	Tulangan Tarik						
	Diameter Tulangan	D 12 mm		D 10 mm		D 12 mm	
	Luas Tulangan Max	420 mm ²		112 mm ²		618 mm ²	
	Jumlah Tulangan	4 bh		2 bh		6 bh	
	Tulangan tekan						
	Diameter Tulangan	D 12 mm		D 10 mm		-	-
	Luas Tulangan Max	236 mm ²		54 mm ²		-	-
Jumlah Tulangan	3 bh		1 bh		-	-	
Tulangan Geser	Tulangan Geser						
	Diameter Tulangan	D 8 mm		D 6 mm		D 6 mm	
	Luas Tulangan Max	125 mm ² /m		0 mm ² /m		0 mm ² /m	
	Jarak Tulangan	200 mm		200 bh		200 bh	

Penulangan Rumah Tinggal 2 Lantai dengan menggunakan bekisting Cara Tradisional

		Sloof	Balok	Ring Balok	Kolom It.1	Kolom It.2
		10x25	10x30	10x10	10x40	10x20
Tulangan Lentur	Tulangan tarik					
	Diameter Tulangan	D 12 mm	D 12 mm	D 10 mm	D 16 mm	D 12 mm
	Luas Tulangan Max	639 mm ²	626 mm ²	109 mm ²	2155 mm ²	392 mm ²
	Jumlah Tulangan	6 bh	6 bh	2 bh	11 bh	4 bh
	Tulangan tekan					
	Diameter Tulangan	D 12 mm	D 12 mm	D 10 mm		
	Luas Tulangan Max	297 mm ²	293 mm ²	54 mm ²		
Jumlah Tulangan	3 bh	3 bh	1 bh			
Tulangan Geser	Tulangan Geser					
	Diameter Tulangan	D 10 mm	D 10 mm	D 10 mm	D 8 mm	D 6 mm
	Luas Tulangan Max	188 mm ² /m	235 mm ² /m	0 mm ² /m	125 mm ² /m	0 mm ² /m
	Jarak Tulangan	200 mm	200 mm	200 mm	200 mm	200 mm

Gaya Dalam Struktur

Rumah Tinggal Dengan Bekisting Baja 1 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Sloof	0	11,312	0,001044	0,0015	8,1873	0,010565	0
Ring Balok	0	2,659	1,561E-18	2,602E-18	1,6068	0,033106	0
Kolom	17,407	1,845	0,27	0,8473	4,1863	0,005339	0,01017

Rumah Tinggal Dengan Bekisting Baja 2 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Kolom lt.1	74,599	1,825	0,381	0,6142	1,5098	0,031425	0,001361
Kolom lt.2	17,38	1,669	0,014	0,1233	3,6621	0,029334	0,002708
Ring Balok	0	2,542	0	0	1,0797	0,026026	0
Balok	0	16,088	0	0	7,1447	0,08389	0
Sloof	0	3,093	0,0002007	0,0003124	0,978	0,009426	0

Rumah Tinggal Dengan Bekisting Cara Tradisional 1 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Sloof	0	12,62	2,614E-05	3,773E-05	10,5535	0,021613	0
Ring Balok	0	1,373	0	0	0,7548	0,097297	0
Kolom	10,986	0,598	0,421	1,2506	1,1665	0,021535	0,027817

Rumah Tinggal Dengan Bekisting Cara Tradisional 2 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Kolom lt.1	68,087	0,715	1,274	1,7235	0,6392	0,04445	0,001137
Kolom lt.2	10,964	0,533	0,051	0,1567	0,9651	0,032114	0,004333
Ring Balok	0	1,348	0	6,505E-20	0,7243	0,085181	0
Balok	0	11,446	0	0	2,4234	0,0529	0
Sloof	0	1,661	0,0005046	0,0007848	0,5864	0,004771	0

RT Baja 2 Lantai

Kolom lt.1

Arah - X

f_c' =	27,5	MPa	A_s =	5 D D 16	=	1005,30965	m ²	L =	3000	mm	
f_y =	400	MPa	A_s' =	4 D D 16	=	804,247719	m ²	b =	200	mm	
E_s =	200000	MPa	A_{st} =			1809,557368	m ²	h =	200	mm	
			A_g =			40000	m ²	d' =	36	mm	
								d =	164	mm	
D 8 - 150											
A_v =	50,265		ϵ_{Cu} =	0,003		a =	83,64	X_{Cc} =	122,18		
V_c =	32,4863	kN	ϵ_s =	0,002		C_c =	391,017	$X_{Cs'}$ =	128		
V_s =	0,000	kN	C =	98,4		C_s' =	302,900	X_{Pn} =	64		
V_n =	24,365	kN	ϵ_b =	0,0031		T_s =	402,124				
$V_u \leq \phi V_n$			ϵ_s' =	0,0019		P_n =	291,793	M_n =	67,871		
1,825	\leq	18,273546ok!								
						74,599	\leq	233,43435ok!		
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$					
0,031425	\leq	2,5714286ok!								
						0,6142	\leq	54,2967065ok!		

Arah - Y

f_c' =	27,5	MPa	A_s =	4 D D 16	=	804,247719	m ²	L =	3000	mm	
f_y =	400	MPa	A_s' =	5 D D 16	=	1005,30965	m ²	b =	200	mm	
E_s =	200000	MPa	A_{st} =			1809,557368	m ²	h =	200	mm	
			A_g =			40000	m ²	d' =	36	mm	
								d =	164	mm	
D 8 - 150											
A_v =	50,265		ϵ_{Cu} =	0,003		a =	83,64	X_{Cc} =	122,18		
V_c =	32,4863	kN	ϵ_s =	0,002		C_c =	391,017	$X_{Cs'}$ =	128		
V_s =	0,000	kN	C =	98,4		C_s' =	378,625	X_{Pn} =	64		
V_n =	24,365	kN	ϵ_b =	0,0031		T_s =	321,699				
$V_u \leq \phi V_n$			ϵ_s' =	0,0019		P_n =	447,943	M_n =	67,570		
0,381	\leq	18,273546ok!								
						74,599	\leq	358,354127ok!		
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$					
0,001361	\leq	2,5714286ok!								
						1,5098	\leq	54,0560756ok!		

Kolom lt.2

Arah - X

f_c'	=	27,5 MPa	A_s	=	2 D D 12 = 226,194671	mm	L	=	3000	mm
f_y	=	400 MPa	A_s'	=	2 D D 12 = 226,194671	mm	b	=	200	mm
E_s	=	200000 MPa	A_{st}	=	452,3893421	mm	h	=	200	mm
			A_g	=	40000	mm	d'	=	32	mm
						d	=	168	mm	

D 6	-	200	ϵ_{Cu}	=	0,003	a	=	85,68	X_{Cc}	=	125,16
A_v	=	28,274	ϵ_s	=	0,002	C_c	=	400,554	X_{Cs}'	=	136
V_c	=	30,27806 kN	C	=	100,8	C_s'	=	85,191	X_{Pn}	=	68
V_s	=	0,000 kN	ϵ_b	=	0,0030	T_s	=	90,478			
V_n	=	22,709 kN	ϵ_s'	=	0,0020	P_n	=	395,267	M_n	=	34,841
V_u	\leq	ϕV_n				P_u	\leq	ϕP_n			
		1,669 \leq 17,03141ok!						17,38 \leq 316,21336ok!			
δ_u	\leq	δ_n				M_u	\leq	ϕM_n			
		0,029334 \leq 2,5714286ok!						0,1233 \leq 27,8728963ok!			

Arah - Y

f_c'	=	27,5 MPa	A_s	=	2 D D 12 = 226,194671	mm	L	=	3000	mm
f_y	=	400 MPa	A_s'	=	2 D D 12 = 226,194671	mm	b	=	200	mm
E_s	=	200000 MPa	A_{st}	=	452,3893421	mm	h	=	200	mm
			A_g	=	40000	mm	d'	=	32	mm
						d	=	168	mm	

D 6	-	200	ϵ_{Cu}	=	0,003	a	=	85,68	X_{Cc}	=	125,16
A_v	=	28,274	ϵ_s	=	0,002	C_c	=	400,554	X_{Cs}'	=	136
V_c	=	30,27806 kN	C	=	100,8	C_s'	=	85,191	X_{Pn}	=	68
V_s	=	0,000 kN	ϵ_b	=	0,0030	T_s	=	90,478			
V_n	=	22,709 kN	ϵ_s'	=	0,0020	P_n	=	395,267	M_n	=	34,841
V_u	\leq	ϕV_n				P_u	\leq	ϕP_n			
		0,014 \leq 17,03141ok!						17,38 \leq 316,21336ok!			
δ_u	\leq	δ_n				M_u	\leq	ϕM_n			
		0,002708 \leq 2,5714286ok!						3,6621 \leq 27,8728963ok!			

Ring balok

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 1 \text{ D } 10 = 78,5398163 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 150 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 8 & d' &= 33 \text{ mm} \\
 & & & & d &= 117 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{D } 8 & - 200 \\
 A_v &= 50,265 & a &= 8,95997905 \\
 V_c &= 15,339 \text{ kN} & M_n &= 3,53492038 \text{ kNm} \\
 V_s &= 0,000 \text{ kN} \\
 V_n &= 11,504 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 2,542 &\leq 8,6280915 \dots\dots\dots\text{ok!} & 1,0797 &\leq 2,82793631 \dots\dots\dots\text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,026026 &\leq 1,4583333 \dots\dots\dots\text{ok!}
 \end{aligned}$$

Balok

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 4 \text{ D } 16 = 804,247719 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 200 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 8 & d' &= 36 \text{ mm} \\
 & & & & d &= 164 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{D } 8 & - 200 \\
 A_v &= 50,265 & a &= 91,7501854 \\
 V_c &= 21,501 \text{ kN} & M_n &= 38,0006749 \text{ kNm} \\
 V_s &= 32,974 \text{ kN} \\
 V_n &= 40,856 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 16,088 &\leq 30,64204 \dots\dots\dots\text{ok!} & 7,1447 &\leq 30,4005399 \dots\dots\dots\text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,08389 &\leq 1,4583333 \dots\dots\dots\text{ok!}
 \end{aligned}$$

Sloof

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 5 \text{ D } 12 = 565,486678 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 200 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 8 & d' &= 34 \text{ mm} \\
 & & & & d &= 166 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{D } 8 & - 200 \\
 A_v &= 50,265 & a &= 64,5118491 \\
 V_c &= 21,763 \text{ kN} & M_n &= 30,2521971 \text{ kNm} \\
 V_s &= 33,376 \text{ kN} \\
 V_n &= 41,354 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 3,093 &\leq 31,015723 \dots\dots\dots\text{ok!} & 0,978 &\leq 24,2017577 \dots\dots\dots\text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,009426 &\leq 1,4583333 \dots\dots\dots\text{ok!}
 \end{aligned}$$

RT Baja 2 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt.1			
Rasio Aksial			
Pu	=	74,599	
ϕP_n	=	233,4343501	
R	=	0,319571648	
Rasio Lentur			
Arah X		Arah Y	
Mu	=	0,6142	Mu = 1,5098
ϕM_n	=	54,29670648	$\phi M_n = 54,05607557$
R	=	0,01131192	R = 0,027930255
Rasio Geser			
Arah X		Arah Y	
Vu	=	1,825	Vu = 0,381
ϕV_n	=	18,27354569	$\phi V_n = 18,27354569$
R	=	0,099871149	R = 0,020849812
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,031425	$\delta u = 0,001361$
δn	=	2,571428571	$\delta n = 2,571428571$
R	=	0,012220833	R = 0,000529278

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Kolom lt.2

Rasio Aksial

$$P_u = 17,38$$

$$\phi P_n = 316,2133597$$

$$R = 0,05496289$$

Rasio Lentur

Arah X

$$M_u = 0,1233$$

$$\phi M_n = 27,87289625$$

$$R = 0,004423652$$

Arah Y

$$M_u = 3,6621$$

$$\phi M_n = 27,87289625$$

$$R = 0,131385701$$

Rasio Geser

Arah X

$$V_u = 1,669$$

$$\phi V_n = 17,03141023$$

$$R = 0,097995408$$

Arah Y

$$V_u = 0,014$$

$$\phi V_n = 17,03141023$$

$$R = 0,000822011$$

Rasio Lendutan

Arah X

$$\delta u = 0,029334$$

$$\delta n = 2,571428571$$

$$R = 0,011407667$$

Arah Y

$$\delta u = 0,002708$$

$$\delta n = 2,571428571$$

$$R = 0,001053111$$

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\mu = 1,0797$$

$$\phi M_n = 2,827936306$$

$$R = 0,381797849$$

Rasio Lendutan

$$\delta_u = 0,026026$$

$$\delta_n = 1,458333333$$

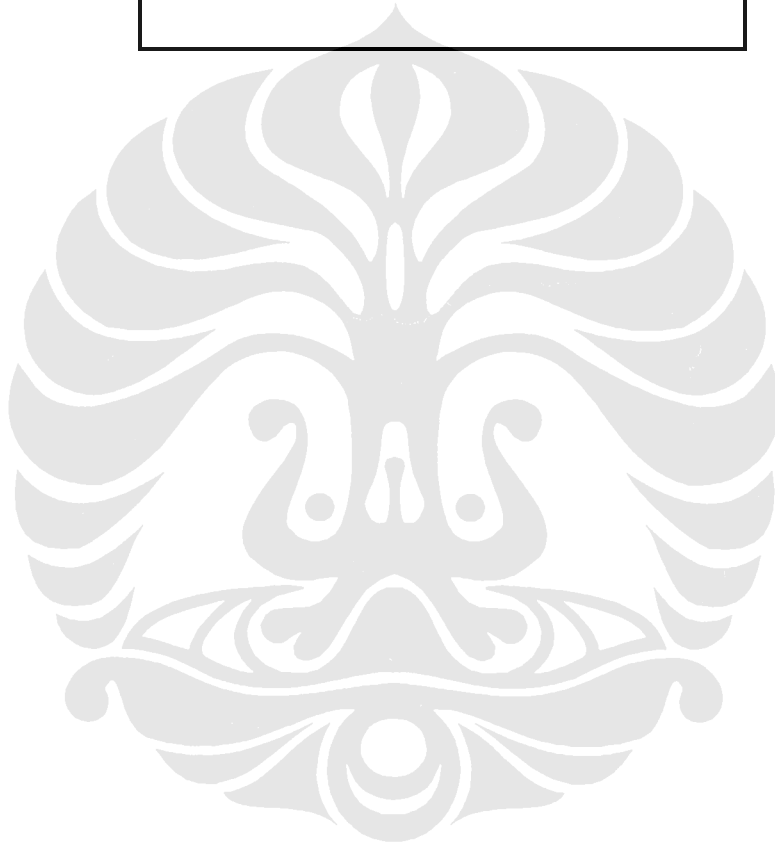
$$R = 0,0178464$$

Rasio Geser

$$V_u = 2,542$$

$$\phi V_n = 8,62809154$$

$$R = 0,294619035$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Balok

Rasio Lentur

Rasio Lendutan

$$M_u = 7,1447$$

$$\delta_u = 0,08389$$

$$\phi M_n = 30,40053993$$

$$\delta_n = 1,458333333$$

$$R = 0,235018852$$

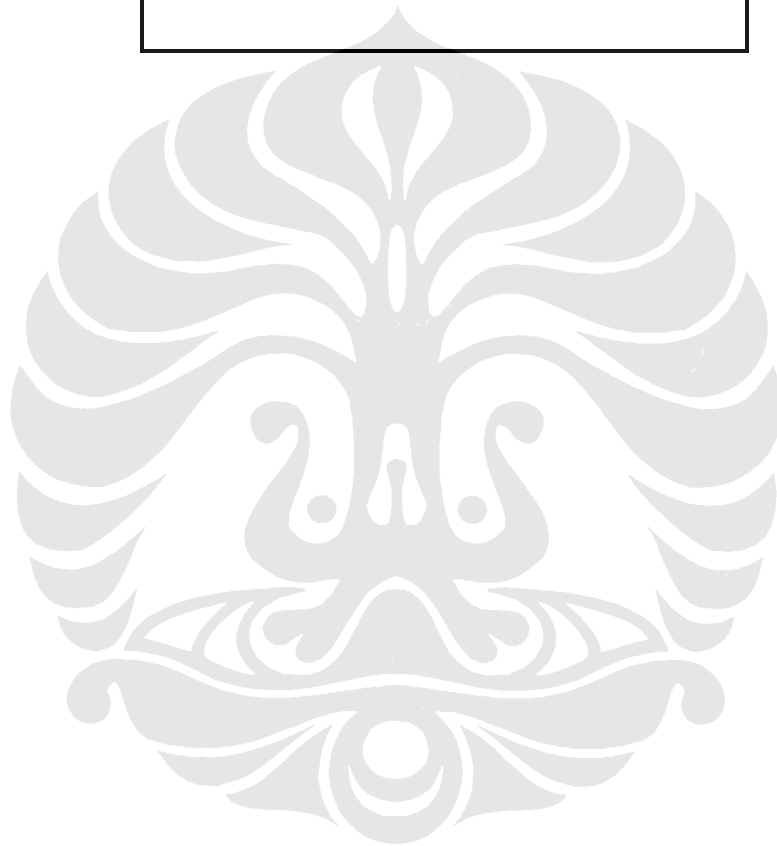
$$R = 0,057524571$$

Rasio Geser

$$V_u = 16,088$$

$$\phi V_n = 30,64204006$$

$$R = 0,525030317$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

Rasio Lendutan

$$\mu_u = 0,978$$

$$\delta_u = 0,009426$$

$$\phi M_n = 24,20175772$$

$$\delta_n = 1,458333333$$

$$R = 0,040410288$$

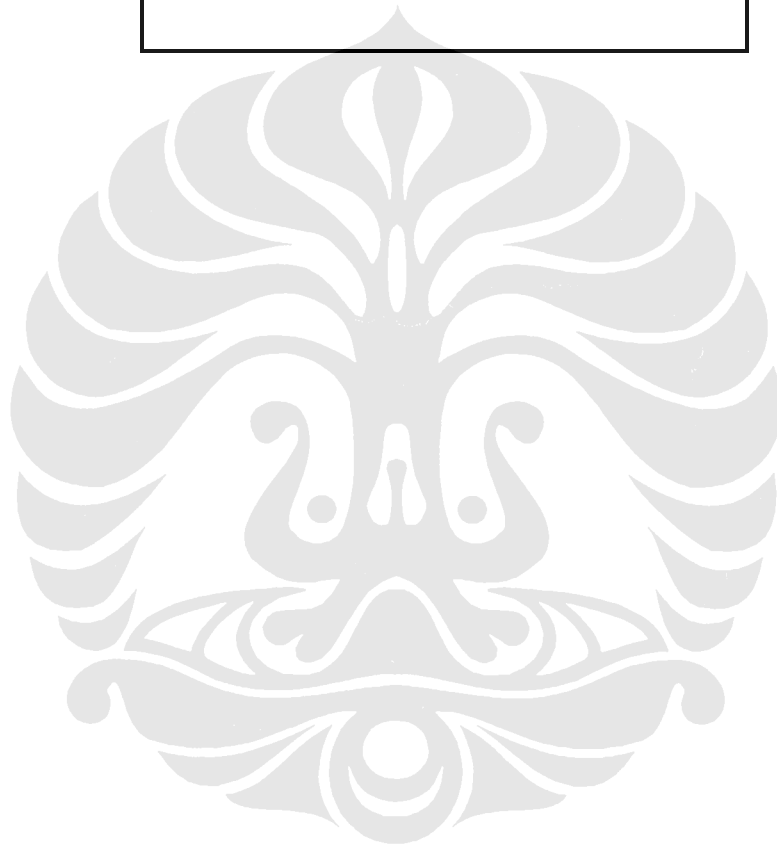
$$R = 0,006463543$$

Rasio Geser

$$V_u = 3,093$$

$$\phi V_n = 31,01572347$$

$$R = 0,099723613$$



RT Cara Tradisional 2 Lantai

Kolom lt.1

Arah - X

f_c' = 27,5 MPa	A_s = 6 D D 16 = 1206,37158 π	L = 3000 mm	
f_y = 400 MPa	A_s' = 5 D D 16 = 1005,30965 π	b = 100 mm	
E_s = 200000 MPa	A_{st} = 2211,681228 π	h = 400 mm	
	A_g = 40000 π	d' = 36 mm	
		d = 364 mm	
D 8 - 200			
A_v = 50,265	ϵ_{Cu} = 0,003	a = 185,64	X_{Cc} = 271,18
V_c = 35,68192 kN	ϵ_s = 0,002	C_c = 433,9335	$X_{Cs'}$ = 328
V_s = 0,000 kN	C = 218,4	C_s' = 378,625	X_{Pn} = 164
V_n = 26,761 kN	ϵ_b = 0,0025	T_s = 482,549	
$V_u \leq \phi V_n$	ϵ_s' = 0,0025	P_n = 330,010	M_n = 187,741
0,715 \leq 20,071082ok!		$P_u \leq \phi P_n$	
		68,087 \leq 264,007692ok!	
$\delta_u \leq \delta_n$		$M_u \leq \phi M_n$	
0,04445 \leq 2,5714286ok!		1,7235 \leq 150,193141ok!	

Arah - Y

f_c' = 27,5 MPa	A_s = 5 D D 16 = 1005,30965 π	L = 3000 mm	
f_y = 400 MPa	A_s' = 6 D D 16 = 1206,37158 π	b = 400 mm	
E_s = 200000 MPa	A_{st} = 2211,681228 π	h = 100 mm	
	A_g = 40000 π	d' = 36 mm	
		d = 64 mm	
D 8 - 200			
A_v = 50,265	ϵ_{Cu} = 0,003	a = 32,64	X_{Cc} = 47,68
V_c = 25,09498 kN	ϵ_s = 0,002	C_c = 305,184	$X_{Cs'}$ = 28
V_s = 0,000 kN	C = 38,4	C_s' = 454,350	X_{Pn} = 14
V_n = 18,821 kN	ϵ_b = 0,0048	T_s = 402,124	
$V_u \leq \phi V_n$	ϵ_s' = 0,0002	P_n = 357,410	M_n = 22,269
1,274 \leq 14,115926ok!		$P_u \leq \phi P_n$	
		68,087 \leq 285,927869ok!	
$\delta_u \leq \delta_n$		$M_u \leq \phi M_n$	
0,001137 \leq 2,5714286ok!		0,6392 \leq 17,8153815ok!	

Kolom lt.2

Arah - X

f_c'	=	27,5 MPa	A_s	=	2 D D 12 = 226,194671 ir	L	=	3000 mm	b	=	100 mm
f_y	=	400 MPa	A_s'	=	2 D D 12 = 226,194671 ir	h	=	200 mm	d'	=	32 mm
E_s	=	200000 MPa	A_{st}	=	452,3893421 ir	d	=	168 mm			
			A_g	=	20000 ir						
D 6	-	200									
A_v	=	28,274	ϵ_{Cu}	=	0,003	a	=	85,68	X_{Cc}	=	125,16
V_c	=	15,25828 kN	ϵ_s	=	0,002	C_c	=	200,277	X_{Cs}'	=	136
V_s	=	0,000 kN	C	=	100,8	C_s'	=	85,191	X_{Pn}	=	68
V_n	=	11,444 kN	ϵ_b	=	0,0030	T_s	=	90,478			
$V_u \leq \phi V_n$			ϵ_s'	=	0,0020	P_n	=	194,990	M_n	=	23,393
0,533	\leq	8,582783ok!				$P_u \leq \phi P_n$					
						10,964	\leq	155,99176ok!			
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$					
0,032114	\leq	2,5714286ok!				0,1567	\leq	18,7146296ok!			

Arah - Y

f_c'	=	27,5 MPa	A_s	=	2 D D 12 = 226,194671 ir	L	=	3000 mm	b	=	200 mm
f_y	=	400 MPa	A_s'	=	2 D D 12 = 226,194671 ir	h	=	100 mm	d'	=	32 mm
E_s	=	200000 MPa	A_{st}	=	452,3893421 ir	d	=	68 mm			
			A_g	=	20000 ir						
D 6	-	200									
A_v	=	28,274	ϵ_{Cu}	=	0,003	a	=	34,68	X_{Cc}	=	50,66
V_c	=	12,35194 kN	ϵ_s	=	0,002	C_c	=	162,129	X_{Cs}'	=	36
V_s	=	0,000 kN	C	=	40,8	C_s'	=	85,191	X_{Pn}	=	18
V_n	=	9,264 kN	ϵ_b	=	0,0044	T_s	=	90,478			
$V_u \leq \phi V_n$			ϵ_s'	=	0,0006	P_n	=	156,842	M_n	=	8,457
0,051	\leq	6,9479672ok!				$P_u \leq \phi P_n$					
						10,964	\leq	125,47336ok!			
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$					
0,004333	\leq	2,5714286ok!				0,9651	\leq	6,765732ok!			

Ring balok

$$\begin{array}{l}
 f'c = 27,5 \text{ MPa} \\
 f_y = 400 \text{ MPa} \\
 E_s = 200000 \text{ MPa}
 \end{array}
 \quad
 \begin{array}{l}
 A_s = 2 \text{ D } 10 = 157,079633 \text{ nr} \\
 A_v = \text{D } 10
 \end{array}
 \quad
 \begin{array}{l}
 b = 100 \text{ mm} \\
 h = 100 \text{ mm} \\
 d' = 35 \text{ mm} \\
 d = 65 \text{ mm}
 \end{array}$$

$$\begin{array}{l}
 \text{D } 10 - 200 \\
 A_v = 78,540 \quad a = 26,8799371 \\
 V_c = 5,681 \text{ kN} \quad M_n = 3,23961232 \text{ kNm} \\
 V_s = 0,000 \text{ kN} \\
 V_n = 4,261 \text{ kN}
 \end{array}$$

$$\begin{array}{l}
 V_u \leq \phi V_n \\
 1,348 \leq 3,1955895 \dots \text{ok!} \\
 \delta_u \leq \delta_n \\
 0,085181 \leq 1,4583333 \dots \text{ok!}
 \end{array}
 \quad
 \begin{array}{l}
 M_u \leq \phi M_n \\
 0,7243 \leq 2,59168986 \dots \text{ok!}
 \end{array}$$

Balok

$$\begin{array}{l}
 f'c = 27,5 \text{ MPa} \\
 f_y = 400 \text{ MPa} \\
 E_s = 200000 \text{ MPa}
 \end{array}
 \quad
 \begin{array}{l}
 A_s = 6 \text{ D } 12 = 678,584013 \text{ nr} \\
 A_v = \text{D } 10
 \end{array}
 \quad
 \begin{array}{l}
 b = 100 \text{ mm} \\
 h = 300 \text{ mm} \\
 d' = 36 \text{ mm} \\
 d = 264 \text{ mm}
 \end{array}$$

$$\begin{array}{l}
 \text{D } 10 - 200 \\
 A_v = 78,540 \quad a = 116,121328 \\
 V_c = 23,074 \text{ kN} \quad M_n = 55,8988564 \text{ kNm} \\
 V_s = 82,938 \text{ kN} \\
 V_n = 79,509 \text{ kN}
 \end{array}$$

$$\begin{array}{l}
 V_u \leq \phi V_n \\
 11,446 \leq 59,63166 \dots \text{ok!} \\
 \delta_u \leq \delta_n \\
 0,0529 \leq 1,4583333 \dots \text{ok!}
 \end{array}
 \quad
 \begin{array}{l}
 M_u \leq \phi M_n \\
 2,4234 \leq 44,7190851 \dots \text{ok!}
 \end{array}$$

Sloof

$$\begin{array}{l}
 f'c = 27,5 \text{ MPa} \\
 f_y = 400 \text{ MPa} \\
 E_s = 200000 \text{ MPa}
 \end{array}
 \quad
 \begin{array}{l}
 A_s = 6 \text{ D } 12 = 678,584013 \text{ nr} \\
 A_v = \text{D } 10
 \end{array}
 \quad
 \begin{array}{l}
 b = 100 \text{ mm} \\
 h = 250 \text{ mm} \\
 d' = 36 \text{ mm} \\
 d = 214 \text{ mm}
 \end{array}$$

$$\begin{array}{l}
 \text{D } 10 - 200 \\
 A_v = 78,540 \quad a = 116,121328 \\
 V_c = 18,704 \text{ kN} \quad M_n = 42,3271761 \text{ kNm} \\
 V_s = 67,230 \text{ kN} \\
 V_n = 64,450 \text{ kN}
 \end{array}$$

$$\begin{array}{l}
 V_u \leq \phi V_n \\
 1,661 \leq 48,337785 \dots \text{ok!} \\
 \delta_u \leq \delta_n \\
 0,004771 \leq 1,4583333 \dots \text{ok!}
 \end{array}
 \quad
 \begin{array}{l}
 M_u \leq \phi M_n \\
 0,5864 \leq 33,8617409 \dots \text{ok!}
 \end{array}$$

RT Cara Tradisional 2 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt.1			
Rasio Aksial			
P_u	=	68,087	
ϕP_n	=	264,007692	
R	=	0,257897789	
Rasio Lentur			
Arah X		Arah Y	
M_u	=	1,7235	M_u = 0,6392
ϕM_n	=	150,1931412	ϕM_n = 17,81538152
R	=	0,011475224	R = 0,035879108
Rasio Geser			
Arah X		Arah Y	
V_u	=	0,715	V_u = 1,274
ϕV_n	=	20,07108197	ϕV_n = 14,11592578
R	=	0,035623391	R = 0,090252671
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,04445	δu = 0,001137
δn	=	2,571428571	δn = 2,571428571
R	=	0,017286111	R = 0,000442167

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Kolom lt.2

Rasio Aksial

$$P_u = 10,964$$

$$\phi P_n = 125,4733597$$

$$R = 0,087381099$$

Rasio Lentur

Arah X

$$M_u = 0,1567$$

$$\phi M_n = 18,7146296$$

$$R = 0,008373129$$

Arah Y

$$M_u = 0,9651$$

$$\phi M_n = 6,765731996$$

$$R = 0,142645319$$

Rasio Geser

Arah X

$$V_u = 0,533$$

$$\phi V_n = 8,582782998$$

$$R = 0,062101069$$

Arah Y

$$V_u = 0,051$$

$$\phi V_n = 6,947967189$$

$$R = 0,007340276$$

Rasio Lendutan

Arah X

$$\delta u = 0,032114$$

$$\delta n = 2,571428571$$

$$R = 0,012488778$$

Arah Y

$$\delta u = 0,004333$$

$$\delta n = 2,571428571$$

$$R = 0,001685056$$

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\mu = 0,7243$$

$$\phi M_n = 2,591689855$$

$$R = 0,279470168$$

Rasio Lendutan

$$\delta_u = 0,085181$$

$$\delta_n = 1,458333333$$

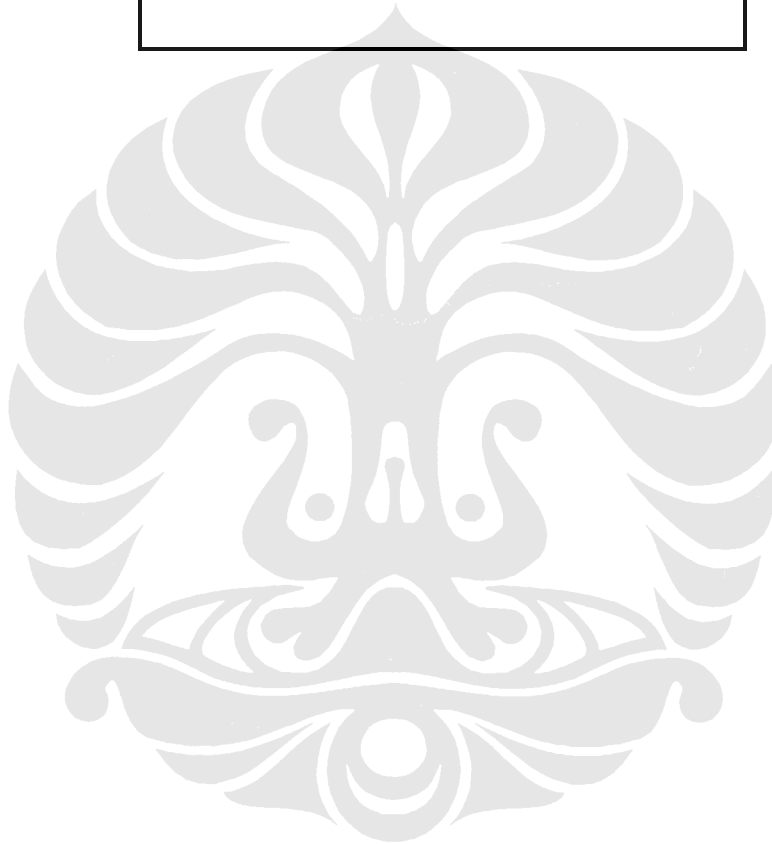
$$R = 0,058409829$$

Rasio Geser

$$V_u = 1,348$$

$$\phi V_n = 3,195589459$$

$$R = 0,421831408$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Balok

Rasio Lentur

Rasio Lendutan

$$\mu_u = 2,4234$$

$$\delta_u = 0,0529$$

$$\phi M_n = 44,7190851$$

$$\delta_n = 1,458333333$$

$$R = 0,054191627$$

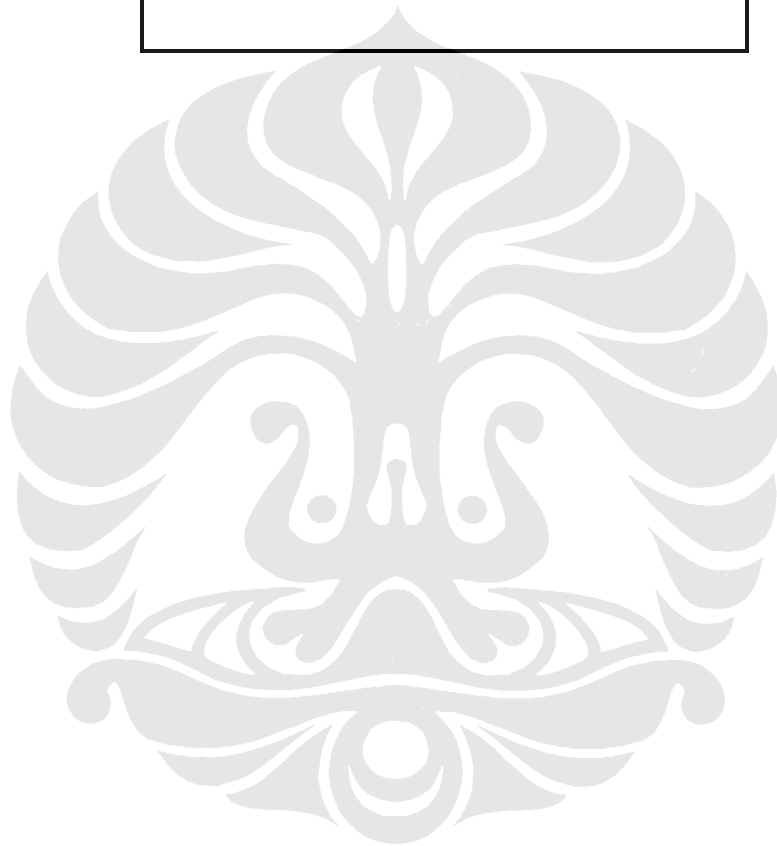
$$R = 0,036274286$$

Rasio Geser

$$V_u = 11,446$$

$$\phi V_n = 59,6316604$$

$$R = 0,191945016$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

Rasio Lendutan

$$\mu_u = 0,5864$$

$$\delta_u = 0,004771$$

$$\phi M_n = 33,86174089$$

$$\delta_n = 1,458333333$$

$$R = 0,017317479$$

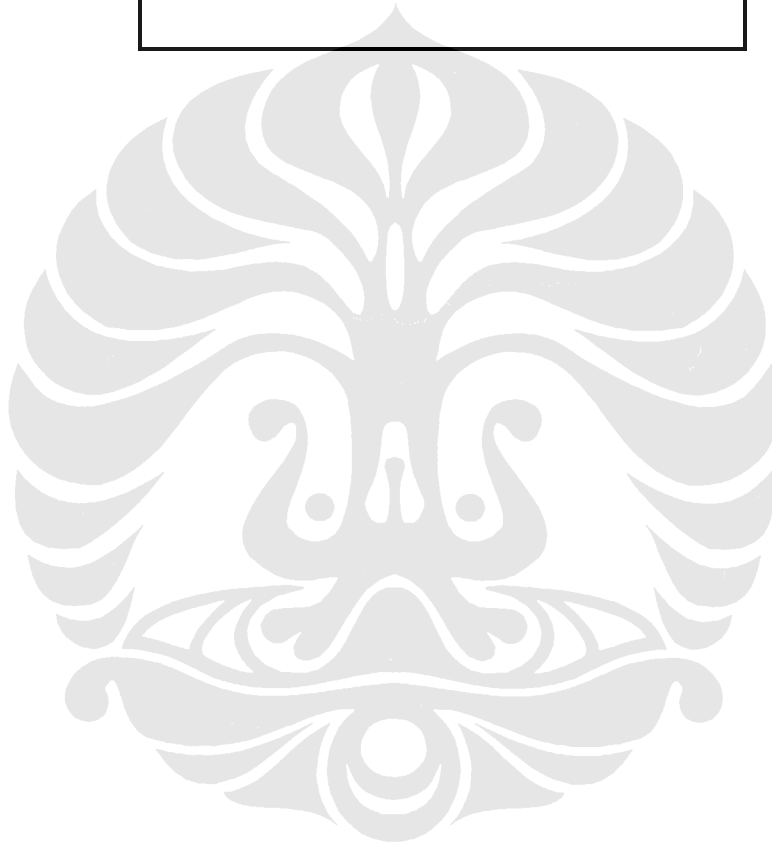
$$R = 0,003271543$$

Rasio Geser

$$V_u = 1,661$$

$$\phi V_n = 48,33778533$$

$$R = 0,034362352$$



RT Baja 1 Lantai

Kolom lt.1

Arah - X

f_c' = 27,5 MPa	A_s = 3 D D 12 = 339,292007 π	L = 3000 mm	b = 200 mm
f_y = 400 MPa	A_s' = 3 D D 12 = 339,292007 π	h = 200 mm	d' = 32 mm
E_s = 200000 MPa	A_{st} = 678,5840132 π	d = 168 mm	
	A_g = 40000 π		
D 6 - 200			
A_v = 28,274	ϵ_{Cu} = 0,003	a = 85,68	XC_c = 125,16
V_c = 30,27948 kN	ϵ_s = 0,002	C_c = 400,554	XC_s' = 136
V_s = 0,000 kN	C = 100,8	C_s' = 127,786	XP_n = 68
V_n = 22,710 kN	ϵ_b = 0,0030	T_s = 135,717	
$V_u \leq \phi V_n$	ϵ_s' = 0,0020	P_n = 392,623	M_n = 40,814
1,845 \leq 17,032207ok!		$P_u \leq \phi P_n$	$M_u \leq \phi M_n$
		17,407 \leq 314,098439	4,1863 \leq 32,6510777
$\delta_u \leq \delta_n$	ok!ok!
0,005339 \leq 2,5714286ok!			

Arah - Y

f_c' = 27,5 MPa	A_s = 3 D D 12 = 339,292007 π	L = 3000 mm	b = 200 mm
f_y = 400 MPa	A_s' = 3 D D 12 = 339,292007 π	h = 200 mm	d' = 32 mm
E_s = 200000 MPa	A_{st} = 678,5840132 π	d = 168 mm	
	A_g = 40000 π		
D 6 - 200			
A_v = 28,274	ϵ_{Cu} = 0,003	a = 85,68	XC_c = 125,16
V_c = 30,27948 kN	ϵ_s = 0,002	C_c = 400,554	XC_s' = 136
V_s = 0,000 kN	C = 100,8	C_s' = 127,786	XP_n = 68
V_n = 22,710 kN	ϵ_b = 0,0030	T_s = 135,717	
$V_u \leq \phi V_n$	ϵ_s' = 0,0020	P_n = 392,623	M_n = 40,814
0,27 \leq 17,032207ok!		$P_u \leq \phi P_n$	
		17,407 \leq 314,098439ok!
$\delta_u \leq \delta_n$		$M_u \leq \phi M_n$	
0,01017 \leq 2,5714286ok!		0,8473 \leq 32,6510777ok!

Ring balok

$$\begin{array}{lcl}
 f_c' & = & 27,5 \text{ MPa} \\
 f_y & = & 400 \text{ MPa} \\
 E_s & = & 200000 \text{ MPa} \\
 A_s & = & 2 \text{ D } 10 = 157,079633 \text{ m}^2 \\
 A_v & = & \text{D } 6 \\
 b & = & 150 \text{ mm} \\
 h & = & 150 \text{ mm} \\
 d' & = & 31 \text{ mm} \\
 d & = & 119 \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 6 & - & 200 \\
 A_v & = & 28,274 \\
 V_c & = & 15,601 \text{ kN} \\
 V_s & = & 0,000 \text{ kN} \\
 V_n & = & 11,701 \text{ kN} \\
 V_u & \leq & \phi V_n
 \end{array}
 \qquad
 \begin{array}{lcl}
 a & = & 17,9199581 \\
 M_n & = & 6,91401843 \text{ kNm} \\
 M_u & \leq & \phi M_n
 \end{array}$$

$$\begin{array}{lcl}
 2,659 & \leq & 8,7755803 \dots\dots\dots\text{ok!} \\
 \delta_u & \leq & \delta_n \\
 0,033106 & \leq & 1,4583333 \dots\dots\dots\text{ok!} \\
 1,6068 & \leq & 5,53121474 \dots\dots\dots\text{ok!}
 \end{array}$$

Sloof

$$\begin{array}{lcl}
 f_c' & = & 27,5 \text{ MPa} \\
 f_y & = & 400 \text{ MPa} \\
 E_s & = & 200000 \text{ MPa} \\
 A_s & = & 5 \text{ D } 12 = 565,486678 \text{ m}^2 \\
 A_v & = & \text{D } 8 \\
 b & = & 150 \text{ mm} \\
 h & = & 200 \text{ mm} \\
 d' & = & 34 \text{ mm} \\
 d & = & 166 \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 8 & - & 200 \\
 A_v & = & 50,265 \\
 V_c & = & 21,763 \text{ kN} \\
 V_s & = & 33,376 \text{ kN} \\
 V_n & = & 41,354 \text{ kN} \\
 V_u & \leq & \phi V_n
 \end{array}
 \qquad
 \begin{array}{lcl}
 a & = & 64,5118491 \\
 M_n & = & 30,2521971 \text{ kNm} \\
 M_u & \leq & \phi M_n
 \end{array}$$

$$\begin{array}{lcl}
 11,312 & \leq & 31,015723 \dots\dots\dots\text{ok!} \\
 \delta_u & \leq & \delta_n \\
 0,010565 & \leq & 1,4583333 \dots\dots\dots\text{ok!} \\
 8,1873 & \leq & 24,2017577 \dots\dots\dots\text{ok!}
 \end{array}$$

RT Baja 1 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt.1			
Rasio Aksial			
P_u	=	17,407	
ϕP_n	=	314,0984395	
R	=	0,055418932	
Rasio Lentur			
Arah X		Arah Y	
M_u	=	4,1863	M_u = 0,8473
ϕM_n	=	32,65107772	ϕM_n = 32,65107772
R	=	0,128213226	R = 0,025950139
Rasio Geser			
Arah X		Arah Y	
V_u	=	1,845	V_u = 0,27
ϕV_n	=	17,03220667	ϕV_n = 17,03220667
R	=	0,10832419	R = 0,015852321
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,005339	δu = 0,01017
δn	=	2,571428571	δn = 2,571428571
R	=	0,002076278	R = 0,003955

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$M_u = 1,6068$$

$$\phi M_n = 5,531214743$$

$$R = 0,290496767$$

Rasio Lendutan

$$\delta_u = 0,033106$$

$$\delta_n = 1,458333333$$

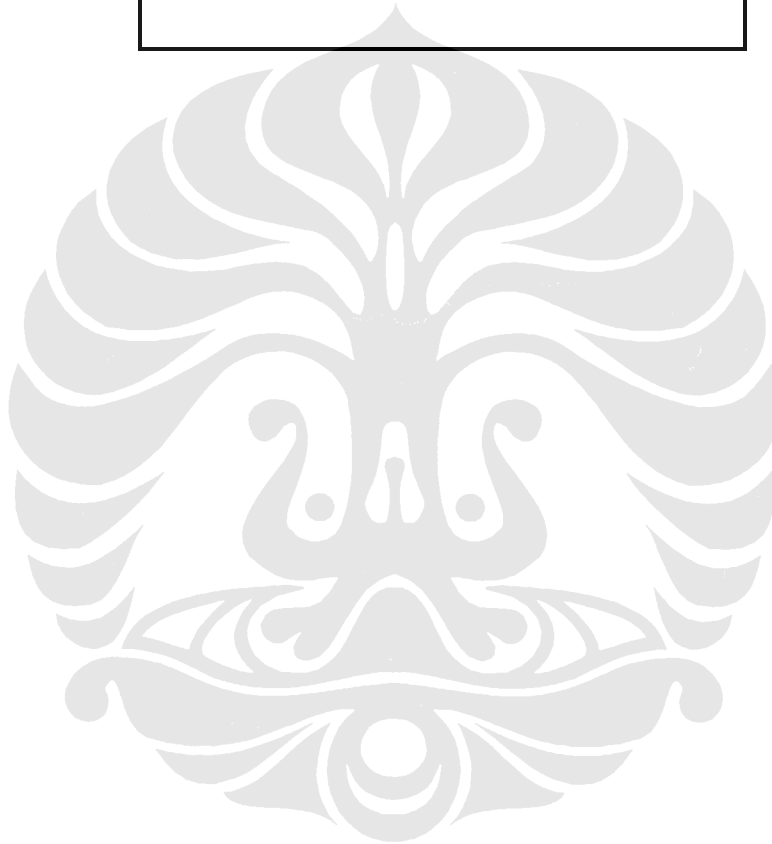
$$R = 0,022701257$$

Rasio Geser

$$V_u = 2,659$$

$$\phi V_n = 8,775580284$$

$$R = 0,302999906$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

$$M_u = 8,1873$$

$$\phi M_n = 24,20175772$$

$$R = 0,338293611$$

Rasio Lendutan

$$\delta u = 0,010565$$

$$\delta n = 1,458333333$$

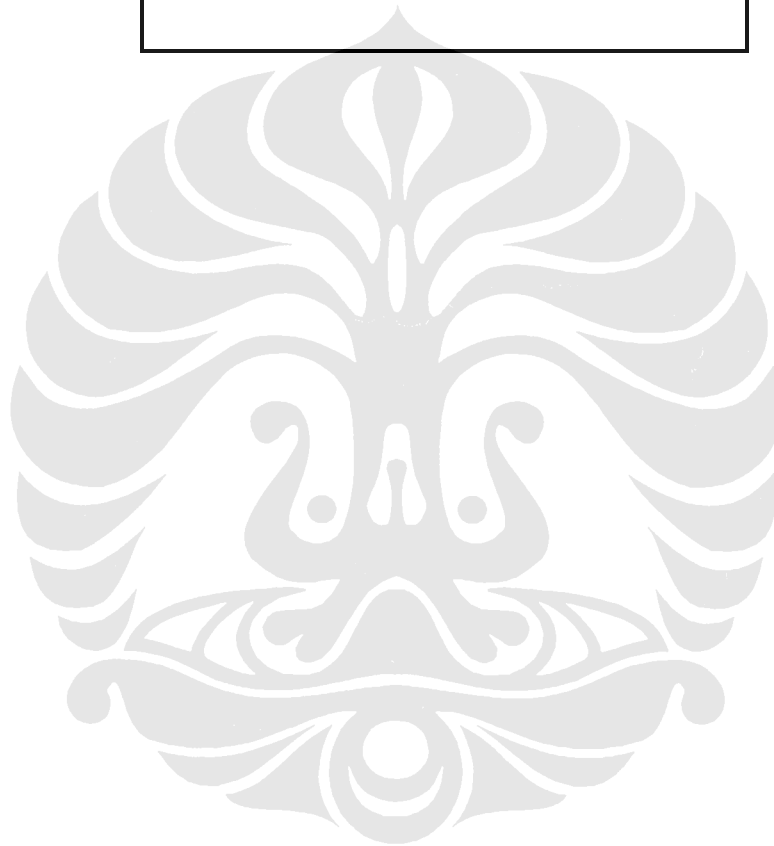
$$R = 0,007244571$$

Rasio Geser

$$V_u = 11,312$$

$$\phi V_n = 31,01572347$$

$$R = 0,364718238$$



RT Cara Tradisional 1 Lantai

Kolom lt.1

Arah - X

f_c'	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>27,5</td></tr></table> MPa	27,5	A_s	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>3</td><td>D</td><td>D</td><td>12</td></tr></table> $=$ <table border="1" style="display: inline-table; text-align: center;"><tr><td>339,292007</td></tr></table> ir	3	D	D	12	339,292007	L	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>3000</td></tr></table> mm	3000
27,5															
3	D	D	12												
339,292007															
3000															
f_y	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>400</td></tr></table> MPa	400	A_s'	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>3</td><td>D</td><td>D</td><td>12</td></tr></table> $=$ <table border="1" style="display: inline-table; text-align: center;"><tr><td>339,292007</td></tr></table> ir	3	D	D	12	339,292007	b	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>100</td></tr></table> mm	100
400															
3	D	D	12												
339,292007															
100															
E_s	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>200000</td></tr></table> MPa	200000	A_{st}	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>678,5840132</td></tr></table> ir	678,5840132	h	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>200</td></tr></table> mm	200				
200000															
678,5840132															
200															
			A_g	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>20000</td></tr></table> ir	20000	d'	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>32</td></tr></table> mm	32					
20000															
32															
						d	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>168</td></tr></table> mm	168						
168															

D 6	-	200		ϵ_{Cu}	$=$	0,003	a	$=$	85,68	X_{Cc}	$=$	125,16		
A_v	$=$	28,274		ϵ_s	$=$	0,002	C_c	$=$	200,277	X_{Cs}'	$=$	136		
V_c	$=$	15,25943 kN		C	$=$	100,8	C_s'	$=$	127,786	X_{Pn}	$=$	68		
V_s	$=$	0,000 kN		ϵ_b	$=$	0,0030	T_s	$=$	135,717					
V_n	$=$	11,445 kN		ϵ_s'	$=$	0,0020	P_n	$=$	192,346	M_n	$=$	29,366		
V_u	\leq	ϕV_n					P_u	\leq	ϕP_n					
<table border="1" style="display: inline-table; text-align: center;"><tr><td>0,598</td></tr></table>	0,598	\leq	8,5834319ok!				<table border="1" style="display: inline-table; text-align: center;"><tr><td>10,986</td></tr></table>	10,986	\leq	153,876839ok!		
0,598														
10,986														
δ_u	\leq	δ_n					M_u	\leq	ϕM_n					
<table border="1" style="display: inline-table; text-align: center;"><tr><td>0,021535</td></tr></table>	0,021535	\leq	2,5714286ok!				<table border="1" style="display: inline-table; text-align: center;"><tr><td>1,1665</td></tr></table>	1,1665	\leq	23,4928111ok!		
0,021535														
1,1665														

Arah - Y

f_c'	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>27,5</td></tr></table> MPa	27,5	A_s	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>3</td><td>D</td><td>D</td><td>12</td></tr></table> $=$ <table border="1" style="display: inline-table; text-align: center;"><tr><td>339,292007</td></tr></table> ir	3	D	D	12	339,292007	L	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>3000</td></tr></table> mm	3000
27,5															
3	D	D	12												
339,292007															
3000															
f_y	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>400</td></tr></table> MPa	400	A_s'	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>3</td><td>D</td><td>D</td><td>12</td></tr></table> $=$ <table border="1" style="display: inline-table; text-align: center;"><tr><td>339,292007</td></tr></table> ir	3	D	D	12	339,292007	b	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>200</td></tr></table> mm	200
400															
3	D	D	12												
339,292007															
200															
E_s	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>200000</td></tr></table> MPa	200000	A_{st}	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>678,5840132</td></tr></table> ir	678,5840132	h	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>100</td></tr></table> mm	100				
200000															
678,5840132															
100															
			A_g	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>20000</td></tr></table> ir	20000	d'	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>32</td></tr></table> mm	32					
20000															
32															
						d	$=$	<table border="1" style="display: inline-table; text-align: center;"><tr><td>68</td></tr></table> mm	68						
68															

D 6	-	200		ϵ_{Cu}	$=$	0,003	a	$=$	34,68	X_{Cc}	$=$	50,66		
A_v	$=$	28,274		ϵ_s	$=$	0,002	C_c	$=$	162,129	X_{Cs}'	$=$	36		
V_c	$=$	12,35288 kN		C	$=$	40,8	C_s'	$=$	127,786	X_{Pn}	$=$	18		
V_s	$=$	0,000 kN		ϵ_b	$=$	0,0044	T_s	$=$	135,717					
V_n	$=$	9,265 kN		ϵ_s'	$=$	0,0006	P_n	$=$	154,198	M_n	$=$	10,038		
V_u	\leq	ϕV_n					P_u	\leq	ϕP_n					
<table border="1" style="display: inline-table; text-align: center;"><tr><td>0,421</td></tr></table>	0,421	\leq	6,9484925ok!				<table border="1" style="display: inline-table; text-align: center;"><tr><td>10,986</td></tr></table>	10,986	\leq	123,358439ok!		
0,421														
10,986														
δ_u	\leq	δ_n					M_u	\leq	ϕM_n					
<table border="1" style="display: inline-table; text-align: center;"><tr><td>0,027817</td></tr></table>	0,027817	\leq	2,5714286ok!				<table border="1" style="display: inline-table; text-align: center;"><tr><td>1,2506</td></tr></table>	1,2506	\leq	8,03054474ok!		
0,027817														
1,2506														

Ring balok

f_c'	=	27,5 MPa	A_s	=	2 D D 10	=	157,079633	tr	b	=	100 mm
f_y	=	400 MPa	A_v	=	D D 6				h	=	100 mm
E_s	=	200000 MPa							d'	=	31 mm
									d	=	69 mm

D 6	-	200									
A_v	=	28,274				a	=	26,8799371			
V_c	=	6,031 kN				M_n	=	3,49093973 kNm			
V_s	=	0,000 kN									
V_n	=	4,523 kN									
V_u	\leq	ϕV_n				M_u	\leq	ϕM_n			

1,373	\leq	3,3922411ok!	0,7548	\leq	2,79275179ok!
δ_u	\leq	δ_n					
0,097297	\leq	1,4583333ok!				

Sloof

f_c'	=	27,5 MPa	A_s	=	4 D D 12	=	452,389342	tr	b	=	100 mm
f_y	=	400 MPa	A_v	=	D D 8				h	=	250 mm
E_s	=	200000 MPa							d'	=	34 mm
									d	=	216 mm

D 8	-	200									
A_v	=	50,265				a	=	77,414219			
V_c	=	18,879 kN				M_n	=	32,0821656 kNm			
V_s	=	43,429 kN									
V_n	=	46,731 kN									
V_u	\leq	ϕV_n				M_u	\leq	ϕM_n			

12,62	\leq	35,048214ok!	10,5535	\leq	25,6657325ok!
δ_u	\leq	δ_n					
0,021613	\leq	1,4583333ok!				

RT Cara Tradisional 1 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt.1			
Rasio Aksial			
P_u	=		10,986
ϕP_n	=	123,3584395	
R	=	0,089057547	
Rasio Lentur			
Arah X		Arah Y	
M_u	=	1,1665	M_u = 1,2506
ϕM_n	=	23,49281107	ϕM_n = 8,030544738
R	=	0,049653487	R = 0,155730407
Rasio Geser			
Arah X		Arah Y	
V_u	=	0,598	V_u = 0,421
ϕV_n	=	8,583431948	ϕV_n = 6,94849253
R	=	0,069669102	R = 0,060588681
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,021535	δu = 0,027817
δn	=	2,571428571	δn = 2,571428571
R	=	0,008374722	R = 0,010817722

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\mu_u = 0,7548$$

$$\phi M_n = 2,792751785$$

$$R = 0,270271065$$

Rasio Lendutan

$$\delta_u = 0,097297$$

$$\delta_n = 1,458333333$$

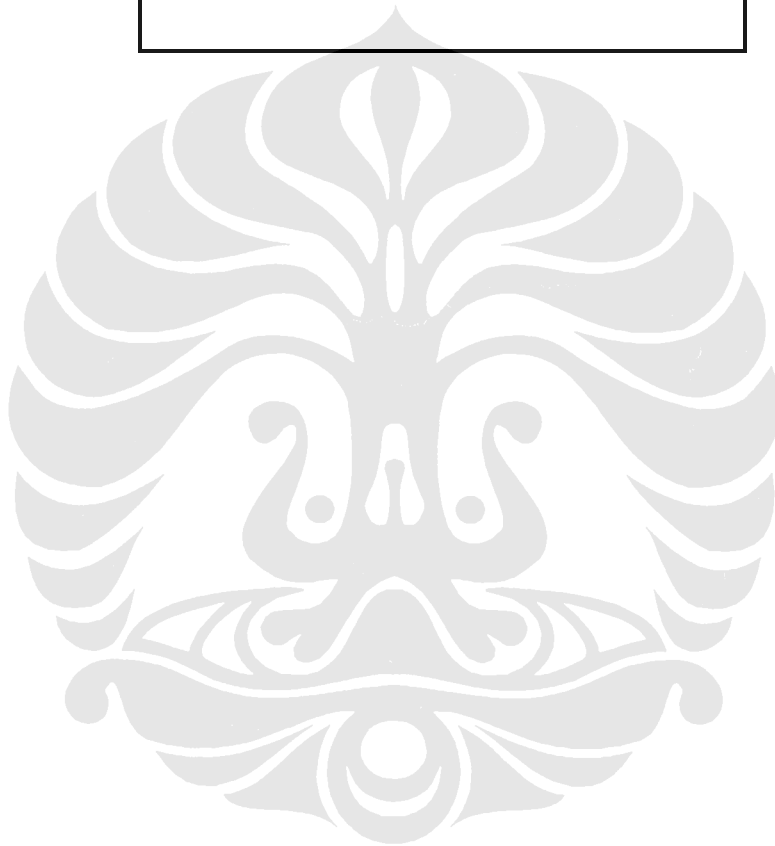
$$R = 0,066717943$$

Rasio Geser

$$V_u = 1,373$$

$$\phi V_n = 3,392241118$$

$$R = 0,404747172$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

$$M_u = 10,5535$$

$$\phi M_n = 25,66573251$$

$$R = 0,41119029$$

Rasio Lendutan

$$\delta u = 0,021613$$

$$\delta n = 1,458333333$$

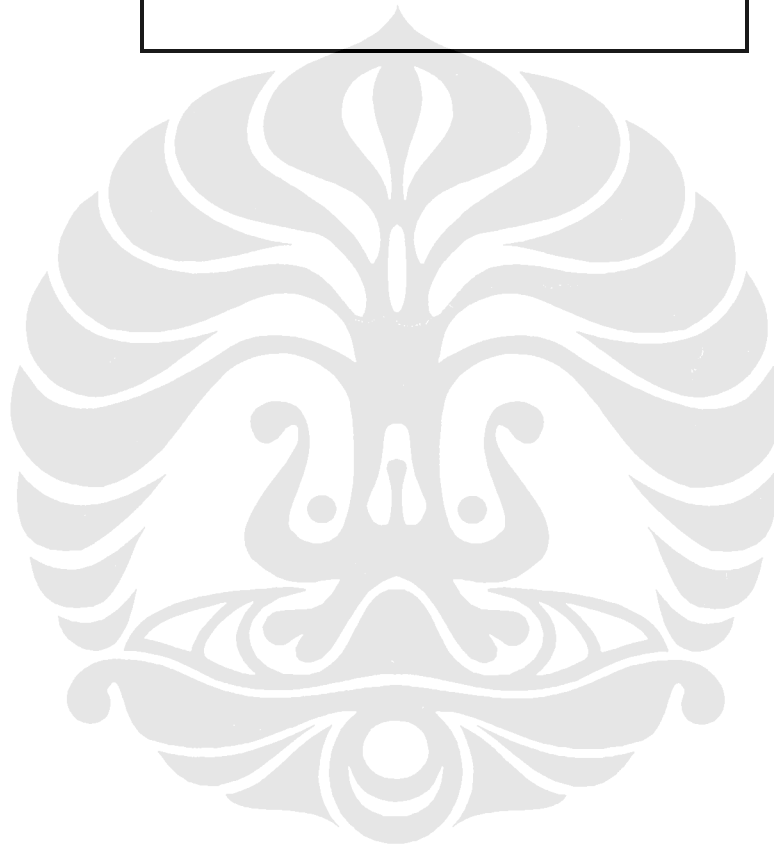
$$R = 0,014820343$$

Rasio Geser

$$V_u = 12,62$$

$$\phi V_n = 35,04821406$$

$$R = 0,360075409$$



Rumah tinggal 2 Lantai

Dengan Bekisting Baja

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	74,599	233,43435	0,3195716	0,6142	54,296706	0,0113119
Kolom lt.2	17,38	316,21336	0,0549629	0,1233	27,872896	0,0044237

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δ u	δ n	R	δ u	δ n	R
Kolom lt.1	1,825	18,273546	0,0998711	0,381	18,273546	0,0208498	0,031425	2,5714286	0,0122208	0,001361	2,5714286	0,0005293
Kolom lt.2	1,669	17,03141	0,0979954	0,014	17,03141	0,000822	0,029334	2,5714286	0,0114077	0,002708	2,5714286	0,0010531

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δ u	δ n	R
Ring Balok	1,0797	2,8279363	0,3817978	2,542	8,6280915	0,294619	0,026026	1,4583333	0,0178464
Balok	7,1447	30,40054	0,2350189	16,088	30,64204	0,5250303	0,08389	1,4583333	0,0575246
Sloof	0,978	24,201758	0,0404103	3,093	31,015723	0,0997236	0,009426	1,4583333	0,0064635

Dengan Bekisting Cara Tradisional

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	68,087	264,00769	0,2578978	1,7235	150,19314	0,0114752
Kolom lt.2	10,964	125,47336	0,0873811	0,1567	18,71463	0,0083731

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δ u	δ n	R	δ u	δ n	R
Kolom lt.1	0,715	20,071082	0,0356234	1,274	14,115926	0,0902527	0,04445	2,5714286	0,0172861	0,001137	2,5714286	0,0004422
Kolom lt.2	0,533	8,582783	0,0621011	0,051	6,9479672	0,0073403	0,032114	2,5714286	0,0124888	0,004333	2,5714286	0,0016851

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δ u	δ n	R
Ring Balok	0,7243	2,5916899	0,2794702	1,348	3,1955895	0,4218314	0,085181	1,4583333	0,0584098
Balok	2,4234	44,719085	0,0541916	11,446	59,63166	0,191945	0,0529	1,4583333	0,0362743
Sloof	0,5864	33,861741	0,0173175	1,661	48,337785	0,0343624	0,004771	1,4583333	0,0032715

Rumah tinggal 1 Lantai

Dengan Bekisting Baja

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	17,407	314,09844	0,0554189	4,1863	32,651078	0,1282132

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δu	δn	R	δu	δn	R
Kolom lt.1	1,845	17,032207	0,1083242	0,27	17,032207	0,0158523	0,005339	2,5714286	0,0020763	0,01017	2,5714286	0,003955

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δu	δn	R
Ring Balok	1,6068	5,5312147	0,2904968	2,659	8,7755803	0,3029999	0,033106	1,4583333	0,0227013
Sloof	8,1873	24,201758	0,3382936	11,312	31,015723	0,3647182	0,010565	1,4583333	0,0072446

Dengan Bekisting Cara Tradisional

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	10,986	123,35844	0,0890575	1,1665	23,492811	0,0496535

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δu	δn	R	δu	δn	R
Kolom lt.1	0,598	8,5834319	0,0696691	0,421	6,9484925	0,0605887	0,021535	2,5714286	0,0083747	0,027817	2,5714286	0,0108177

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δu	δn	R
Ring Balok	0,7548	2,7927518	0,2702711	1,373	3,3922411	0,4047472	0,097297	1,4583333	0,0667179
Sloof	10,5535	25,665733	0,4111903	12,62	35,048214	0,3600754	0,021613	1,4583333	0,0148203

Rumah tinggal 2 Lantai

Dengan Bekisting Baja

	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,359	0,100	0,021	0,012	0,001	-
Kolom lt.2	-	0,191	0,098	0,001	0,011	0,001	-
Ring Balok	0,382	-	0,295	-	-	-	0,018
Balok	0,235	-	0,525	-	-	-	0,058
Sloof	0,040	-	0,100	-	-	-	0,006

Dengan Bekisting Cara Tradisional

	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,305	0,036	0,090	0,017	0,000	-
Kolom lt.2	-	0,238	0,062	0,007	0,012	0,002	-
Ring Balok	0,279	-	0,422	-	-	-	0,058
Balok	0,054	-	0,192	-	-	-	0,036
Sloof	0,017	-	0,034	-	-	-	0,003

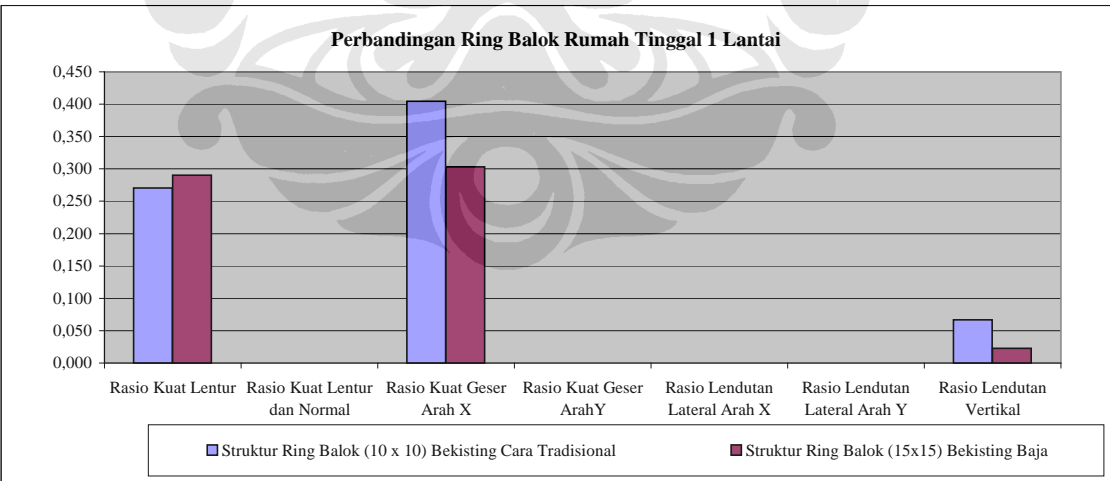
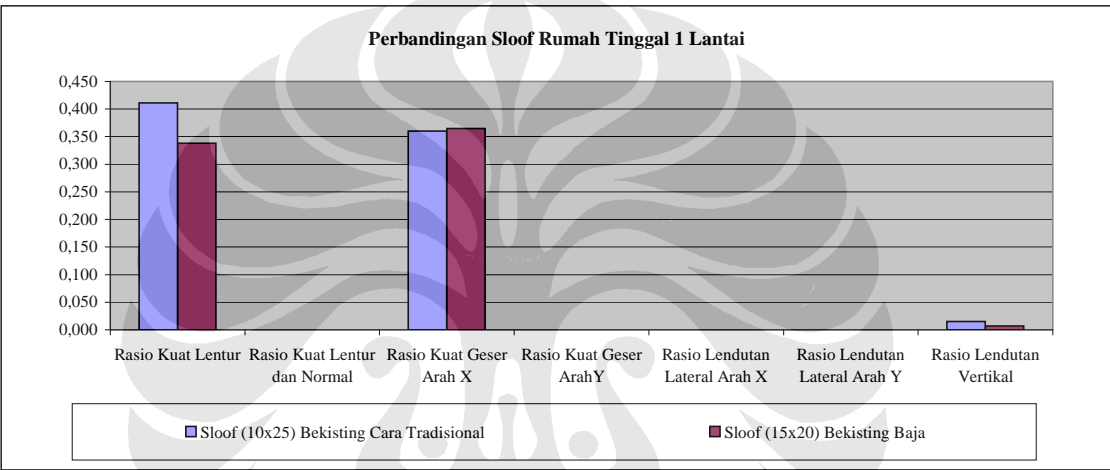
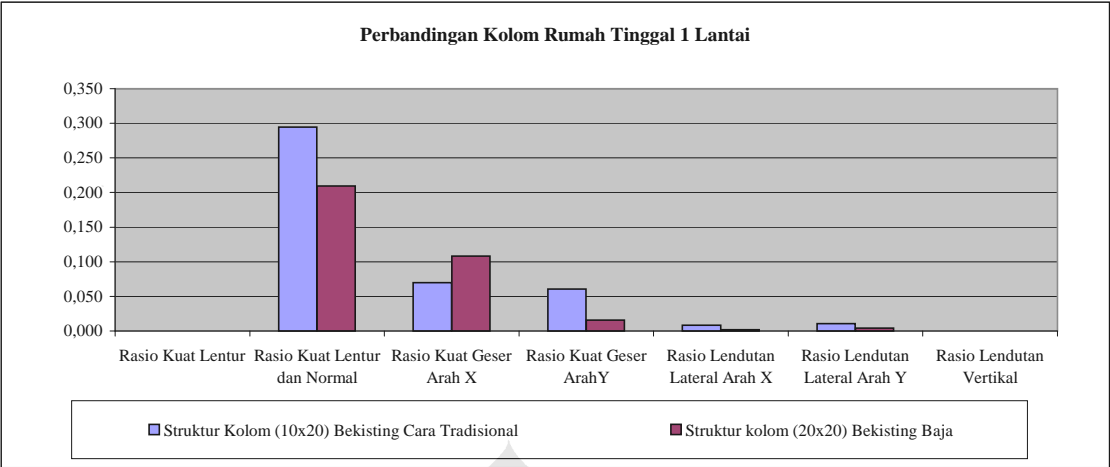
Rumah tinggal 1 Lantai

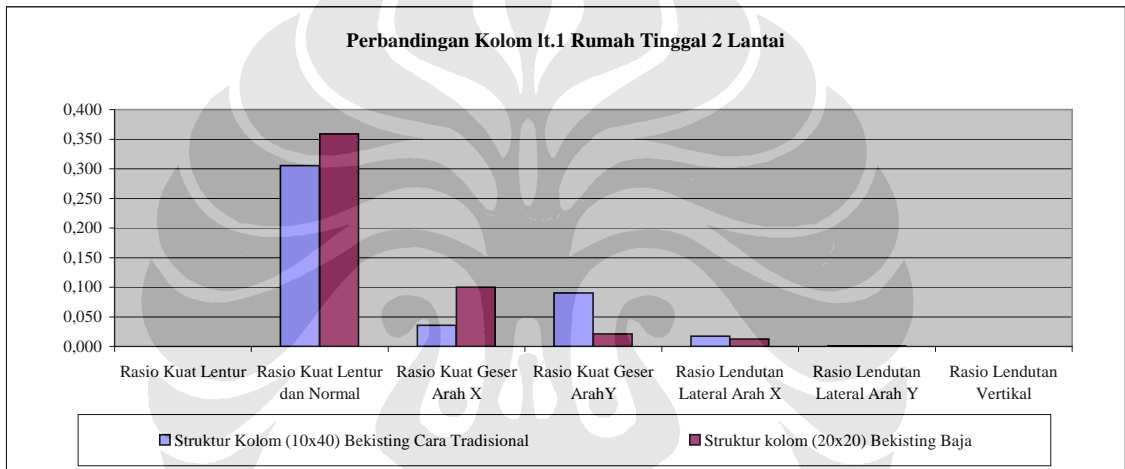
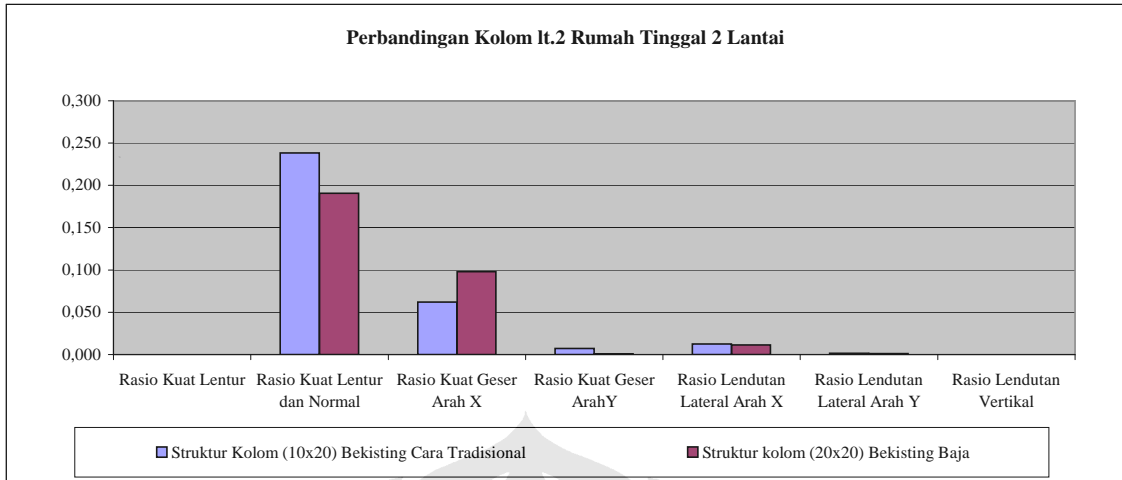
Dengan Bekisting Baja

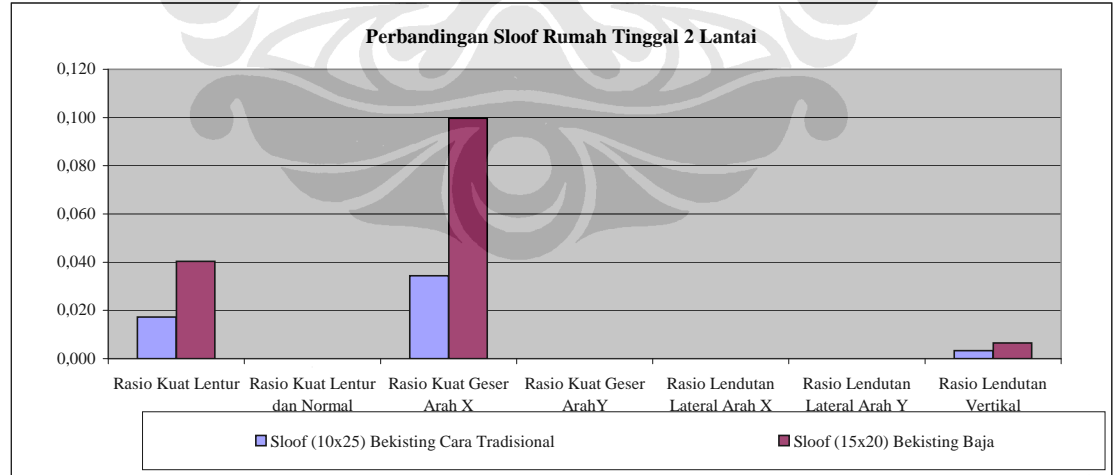
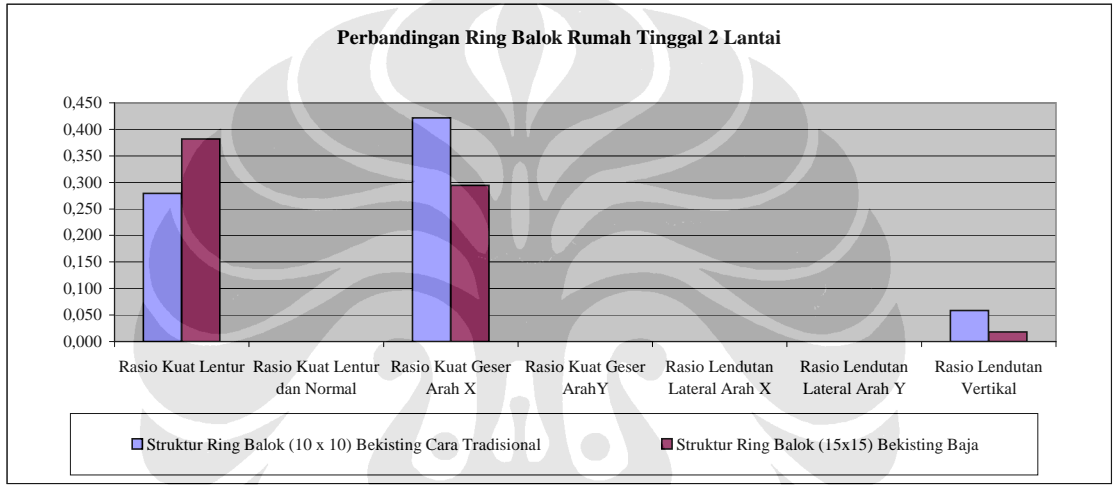
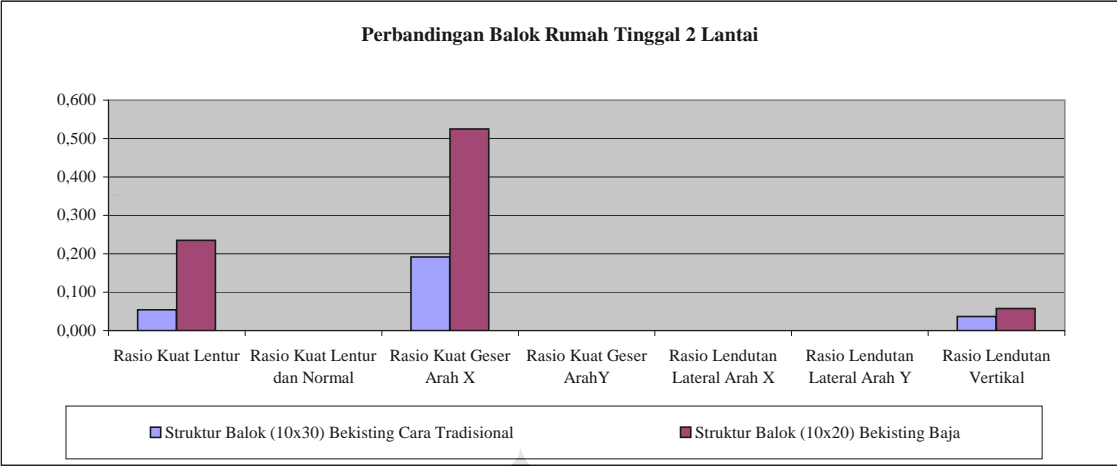
	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,210	0,108	0,016	0,002	0,004	-
Ring Balok	0,290	-	0,303	-	-	-	0,023
Sloof	0,338	-	0,365	-	-	-	0,007

Dengan Bekisting Cara Tradisional

	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,294	0,070	0,061	0,008	0,011	-
Ring Balok	0,270	-	0,405	-	-	-	0,067
Sloof	0,411	-	0,360	-	-	-	0,015







Rumah tinggal 2 Lantai

Dengan Bekisting Baja

	Elemen No.	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	23	-	0,359	0,100	0,021	0,012	0,001	-
	26	-	0,422	0,152	0,013	0,002	0,001	-
Kolom lt.2	52	-	0,191	0,098	0,001	0,011	0,001	-
	55	-	0,279	0,152	0,003	0,013	0,009	-
Ring Balok	65	0,382	-	0,295	-	-	-	0,018
	70	0,400	-	0,297	-	-	-	0,014
Balok	36	0,235	-	0,525	-	-	-	0,058
	41	0,435	-	0,968	-	-	-	0,079
Sloof	7	0,040	-	0,100	-	-	-	0,006
	12	0,049	-	0,098	-	-	-	0,055

Dengan Bekisting Cara Tradisional

	Elemen No.	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	23	-	0,305	0,036	0,090	0,017	0,000	-
	26	-	0,373	0,060	0,084	0,002	0,001	-
Kolom lt.2	52	-	0,238	0,062	0,007	0,012	0,002	-
	55	-	0,316	0,087	0,008	0,006	0,013	-
Ring Balok	65	0,279	-	0,422	-	-	-	0,058
	70	0,279	-	0,417	-	-	-	0,042
Balok	36	0,054	-	0,192	-	-	-	0,036
	41	0,124	-	0,394	-	-	-	0,036
Sloof	7	0,017	-	0,034	-	-	-	0,003
	12	0,025	-	0,035	-	-	-	0,037

Rumah tinggal 1 Lantai

Dengan Bekisting Baja

	Elemen No.	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	23	-	0,210	0,108	0,016	0,002	0,004	-
	26	-	0,321	0,192	0,014	0,019	0,015	-
Ring Balok	36	0,290	-	0,303	-	-	-	0,023
	41	0,321	-	0,306	-	-	-	0,013
Sloof	7	0,338	-	0,365	-	-	-	0,007
	12	0,593	-	0,805	-	-	-	0,059

Dengan Bekisting Cara Tradisional

	Elemen No.	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	23	-	0,294	0,070	0,061	0,008	0,011	-
	26	-	0,350	0,129	0,061	0,027	0,025	-
Ring Balok	36	0,270	-	0,405	-	-	-	0,067
	41	0,295	-	0,409	-	-	-	0,036
Sloof	7	0,411	-	0,360	-	-	-	0,015
	12	0,651	-	0,771	-	-	-	0,052

Penulangan Rumah Tinggal 1 Lantai dengan menggunakan bekisting Baja

		Sloof	Ring Balok	Kolom
		15x20	15x15	20x20
Tulangan Lentur	Tulangan Atas			
	Diameter Tulangan	D 12 mm	D 10 mm	D 12 mm
	Luas Tulangan Max	455 mm ²	127 mm ²	574 mm ²
	Jumlah Tulangan	5 bh	2 bh	6 bh
	Tulangan Bawah			
	Diameter Tulangan	D 12 mm	D 10 mm	
	Luas Tulangan Max	245 mm ²	83 mm ²	
Jumlah Tulangan	3 bh	2 bh		
Tulangan Geser	Tulangan Atas			
	Diameter Tulangan	D 8 mm	D 6 mm	D 6 mm
	Luas Tulangan Max	199 mm ² /m	0 mm ² /m	0 mm ² /m
	Jarak Tulangan	200 mm	200 bh	200 bh

Penulangan Rumah Tinggal 2 Lantai dengan menggunakan bekisting Baja

		Sloof	Balok	Ring Balok	Kolom It.1	Kolom It.2
		15x20	15x20	15x15	20x20	20x20
Tulangan Lentur	Tulangan Atas					
	Diameter Tulangan	D 12 mm	D 16 mm	D 10 mm	D 16 mm	D 12 mm
	Luas Tulangan Max	546 mm ²	617 mm ²	61 mm ²	1654 mm ²	350 mm ²
	Jumlah Tulangan	5 bh	4 bh	1 bh	9 bh	4 bh
	Tulangan Bawah					
	Diameter Tulangan	D 12 mm	D 16 mm	D 10 mm		
	Luas Tulangan Max	254 mm ²	289 mm ²	40 mm ²		
Jumlah Tulangan	3 bh	2 bh	1 bh			
Tulangan Geser	Tulangan Atas					
	Diameter Tulangan	D 8 mm	D 8 mm	D 8 mm	D 8 mm	D 6 mm
	Luas Tulangan Max /m	203 mm ²	227 mm ²	0 mm ²	125 mm ²	0 mm ²
	Jarak Tulangan	200 mm	200 mm	200 mm	150 mm	200 mm

Penulangan Rumah Tinggal 1 Lantai dengan menggunakan bekisting Cara Tradisional

		Sloof		Ring Balok		Kolom	
		10x25		10x10		10x20	
Tulangan Lentur	Tulangan Tarik						
	Diameter Tulangan	D 12 mm		D 10 mm		D 12 mm	
	Luas Tulangan Max	420 mm ²		112 mm ²		618 mm ²	
	Jumlah Tulangan	4 bh		2 bh		6 bh	
	Tulangan tekan						
	Diameter Tulangan	D 12 mm		D 10 mm		-	-
	Luas Tulangan Max	236 mm ²		54 mm ²		-	-
Jumlah Tulangan	3 bh		1 bh		-	-	
Tulangan Geser	Tulangan Geser						
	Diameter Tulangan	D 8 mm		D 6 mm		D 6 mm	
	Luas Tulangan Max	125 mm ² /m		0 mm ² /m		0 mm ² /m	
	Jarak Tulangan	200 mm		200 bh		200 bh	

Penulangan Rumah Tinggal 2 Lantai dengan menggunakan bekisting Cara Tradisional

		Sloof	Balok	Ring Balok	Kolom It.1	Kolom It.2
		10x25	10x30	10x10	10x40	10x20
Tulangan Lentur	Tulangan tarik					
	Diameter Tulangan	D 12 mm	D 12 mm	D 10 mm	D 16 mm	D 12 mm
	Luas Tulangan Max	639 mm ²	626 mm ²	109 mm ²	2155 mm ²	392 mm ²
	Jumlah Tulangan	6 bh	6 bh	2 bh	11 bh	4 bh
	Tulangan tekan					
	Diameter Tulangan	D 12 mm	D 12 mm	D 10 mm		
	Luas Tulangan Max	297 mm ²	293 mm ²	54 mm ²		
Jumlah Tulangan	3 bh	3 bh	1 bh			
Tulangan Geser	Tulangan Geser					
	Diameter Tulangan	D 10 mm	D 10 mm	D 10 mm	D 8 mm	D 6 mm
	Luas Tulangan Max	188 mm ² /m	235 mm ² /m	0 mm ² /m	125 mm ² /m	0 mm ² /m
	Jarak Tulangan	200 mm	200 mm	200 mm	200 mm	200 mm

Gaya Dalam Struktur

Rumah Tinggal Dengan Bekisting Baja 1 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Sloof	0	24,976	0,001044	0,0015	14,3512	0,08631	0
Ring Balok	0	2,688	5,204E-19	5,204E-19	1,7748	0,018674	0
Kolom	17,435	3,269	0,244	0,8031	7,8769	0,049348	0,039377

Rumah Tinggal Dengan Bekisting Baja 2 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Kolom lt.1	87,956	2,834	0,238	0,3444	2,0845	0,004018	0,001876
Kolom lt.2	17,353	2,581	0,058	0,2294	6,0209	0,033878	0,022954
Ring Balok	0	2,561	0	0	1,1315	0,019817	0
Balok	0	29,663	0	0	13,2389	0,115482	0
Sloof	0	3,052	0,0002007	0,0003124	1,1892	0,079641	0

Rumah Tinggal Dengan Bekisting Cara Tradisional 1 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Sloof	0	27,038	2,614E-05	3,773E-05	16,7073	0,076495	0
Ring Balok	0	1,387	0	0	0,8233	0,052537	0
Kolom	11	1,104	0,423	1,2539	2,4505	0,068481	0,065253

Rumah Tinggal Dengan Bekisting Cara Tradisional 2 lantai

	Pu KN	Vu-x KN	Vu-y KN	Mu-x KN-m	Mu-y KN-m	$\delta u-x$ cm	$\delta u-y$ cm
Kolom lt.1	80,085	1,236	1,208	1,496	1,0638	0,006307	0,003343
Kolom lt.2	10,97	0,746	0,058	0,1753	1,4847	0,016444	0,033845
Ring Balok	0	1,334	0	6,505E-20	0,7221	0,061488	0
Balok	0	23,504	0	0	5,5327	0,051987	0
Sloof	0	1,704	0,0005046	0,0007848	0,8364	0,05368	0

RT Baja 2 Lantai

Kolom lt.1

Arah - X

f_c' =	27,5	MPa	A_s =	5 D D 16	=	1005,30965	m ²	L =	3000	mm	
f_y =	400	MPa	A_s' =	4 D D 16	=	804,247719	m ²	b =	200	mm	
E_s =	200000	MPa	A_{st} =			1809,557368	m ²	h =	200	mm	
			A_g =			40000	m ²	d' =	36	mm	
								d =	164	mm	
D 8 - 150											
A_v =	50,265		ϵ_{Cu} =	0,003		a =	83,64	X_{Cc} =	122,18		
V_c =	33,17007	kN	ϵ_s =	0,002		C_c =	391,017	X_{Cs}' =	128		
V_s =	0,000	kN	C =	98,4		C_s' =	302,900	X_{Pn} =	64		
V_n =	24,878	kN	ϵ_b =	0,0031		T_s =	402,124				
$V_u \leq \phi V_n$			ϵ_s' =	0,0019		P_n =	291,793	M_n =	67,871		
2,834	\leq	18,658166ok!								
						87,956	\leq	233,43435ok!		
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$					
0,004018	\leq	2,5714286ok!								
						0,3444	\leq	54,2967065ok!		

Arah - Y

f_c' =	27,5	MPa	A_s =	4 D D 16	=	804,247719	m ²	L =	3000	mm	
f_y =	400	MPa	A_s' =	5 D D 16	=	1005,30965	m ²	b =	200	mm	
E_s =	200000	MPa	A_{st} =			1809,557368	m ²	h =	200	mm	
			A_g =			40000	m ²	d' =	36	mm	
								d =	164	mm	
D 8 - 150											
A_v =	50,265		ϵ_{Cu} =	0,003		a =	83,64	X_{Cc} =	122,18		
V_c =	33,17007	kN	ϵ_s =	0,002		C_c =	391,017	X_{Cs}' =	128		
V_s =	0,000	kN	C =	98,4		C_s' =	378,625	X_{Pn} =	64		
V_n =	24,878	kN	ϵ_b =	0,0031		T_s =	321,699				
$V_u \leq \phi V_n$			ϵ_s' =	0,0019		P_n =	447,943	M_n =	67,570		
0,238	\leq	18,658166ok!								
						87,956	\leq	358,354127ok!		
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$					
0,001876	\leq	2,5714286ok!								
						2,0845	\leq	54,0560756ok!		

Kolom lt.2

Arah - X

f_c'	=	27,5 MPa	A_s	=	2 D D 12 = 226,194671 ir	L	=	3000 mm
f_y	=	400 MPa	A_s'	=	2 D D 12 = 226,194671 ir	b	=	200 mm
E_s	=	200000 MPa	A_{st}	=	452,3893421 ir	h	=	200 mm
			A_g	=	40000 ir	d'	=	32 mm
						d	=	168 mm
D 6	-	200	ϵ_{Cu}	=	0,003	a	=	85,68
A_v	=	28,274	ϵ_s	=	0,002	C_c	=	400,554
V_c	=	30,27665 kN	C	=	100,8	C_s'	=	85,191
V_s	=	0,000 kN	ϵ_b	=	0,0030	T_s	=	90,478
V_n	=	22,707 kN	ϵ_s'	=	0,0020	P_n	=	395,267
V_u	\leq	ϕV_n			M_n	=	34,841	
2,581	\leq	17,030614ok!			P_u	\leq	ϕP_n	
					17,353	\leq	316,21336ok!	
δ_u	\leq	δ_n			M_u	\leq	ϕM_n	
0,033878	\leq	2,5714286ok!			0,2294	\leq	27,8728963ok!	

Arah - Y

f_c'	=	27,5 MPa	A_s	=	2 D D 12 = 226,194671 ir	L	=	3000 mm
f_y	=	400 MPa	A_s'	=	2 D D 12 = 226,194671 ir	b	=	200 mm
E_s	=	200000 MPa	A_{st}	=	452,3893421 ir	h	=	200 mm
			A_g	=	40000 ir	d'	=	32 mm
						d	=	168 mm
D 6	-	200	ϵ_{Cu}	=	0,003	a	=	85,68
A_v	=	28,274	ϵ_s	=	0,002	C_c	=	400,554
V_c	=	30,27665 kN	C	=	100,8	C_s'	=	85,191
V_s	=	0,000 kN	ϵ_b	=	0,0030	T_s	=	90,478
V_n	=	22,707 kN	ϵ_s'	=	0,0020	P_n	=	395,267
V_u	\leq	ϕV_n			M_n	=	34,841	
0,058	\leq	17,030614ok!			P_u	\leq	ϕP_n	
					17,353	\leq	316,21336ok!	
δ_u	\leq	δ_n			M_u	\leq	ϕM_n	
0,022954	\leq	2,5714286ok!			6,0209	\leq	27,8728963ok!	

Ring balok

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 1 \text{ D } 10 = 78,5398163 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 150 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 8 & d' &= 33 \text{ mm} \\
 & & & & d &= 117 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{D } 8 & - 200 \\
 A_v &= 50,265 & a &= 8,95997905 \\
 V_c &= 15,339 \text{ kN} & M_n &= 3,53492038 \text{ kNm} \\
 V_s &= 0,000 \text{ kN} \\
 V_n &= 11,504 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 2,561 &\leq 8,6280915 \text{ok!} & 1,1315 &\leq 2,82793631 \text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,019817 &\leq 1,4583333 \text{ok!}
 \end{aligned}$$

Balok

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 4 \text{ D } 16 = 804,247719 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 200 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 8 & d' &= 36 \text{ mm} \\
 & & & & d &= 164 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{D } 8 & - 200 \\
 A_v &= 50,265 & a &= 91,7501854 \\
 V_c &= 21,501 \text{ kN} & M_n &= 38,0006749 \text{ kNm} \\
 V_s &= 32,974 \text{ kN} \\
 V_n &= 40,856 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 29,663 &\leq 30,64204 \text{ok!} & 13,2389 &\leq 30,4005399 \text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,115482 &\leq 1,4583333 \text{ok!}
 \end{aligned}$$

Sloof

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 5 \text{ D } 12 = 565,486678 \text{ nr} & b &= 150 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 200 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 8 & d' &= 34 \text{ mm} \\
 & & & & d &= 166 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \text{D } 8 & - 200 \\
 A_v &= 50,265 & a &= 64,5118491 \\
 V_c &= 21,763 \text{ kN} & M_n &= 30,2521971 \text{ kNm} \\
 V_s &= 33,376 \text{ kN} \\
 V_n &= 41,354 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 3,052 &\leq 31,015723 \text{ok!} & 1,1892 &\leq 24,2017577 \text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,079641 &\leq 1,4583333 \text{ok!}
 \end{aligned}$$

RT Baja 2 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt.1			
Rasio Aksial			
P_u	=	87,956	
ϕP_n	=	233,4343501	
R	=	0,376791162	
Rasio Lentur			
Arah X		Arah Y	
M_u	=	0,3444	M_u = 2,0845
ϕM_n	=	54,29670648	ϕM_n = 54,05607557
R	=	0,006342926	R = 0,038561808
Rasio Geser			
Arah X		Arah Y	
V_u	=	2,834	V_u = 0,238
ϕV_n	=	18,65816613	ϕV_n = 18,65816613
R	=	0,151890597	R = 0,012755809
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,004018	δu = 0,001876
δn	=	2,571428571	δn = 2,571428571
R	=	0,001562556	R = 0,000729556

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Kolom lt.2

Rasio Aksial

$$P_u = 17,353$$

$$\phi P_n = 316,2133597$$

$$R = 0,054877504$$

Rasio Lentur

Arah X

$$M_u = 0,2294$$

$$\phi M_n = 27,87289625$$

$$R = 0,008230218$$

Arah Y

$$M_u = 6,0209$$

$$\phi M_n = 27,87289625$$

$$R = 0,216012715$$

Rasio Geser

Arah X

$$V_u = 2,581$$

$$\phi V_n = 17,03061379$$

$$R = 0,151550615$$

Arah Y

$$V_u = 0,058$$

$$\phi V_n = 17,03061379$$

$$R = 0,003405632$$

Rasio Lendutan

Arah X

$$\delta u = 0,033878$$

$$\delta n = 2,571428571$$

$$R = 0,013174778$$

Arah Y

$$\delta u = 0,022954$$

$$\delta n = 2,571428571$$

$$R = 0,008926556$$

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\text{Mu} = 1,1315$$

$$\phi \text{ Mn} = 2,827936306$$

$$\text{R} = 0,400115094$$

Rasio Lendutan

$$\delta u = 0,019817$$

$$\delta n = 1,458333333$$

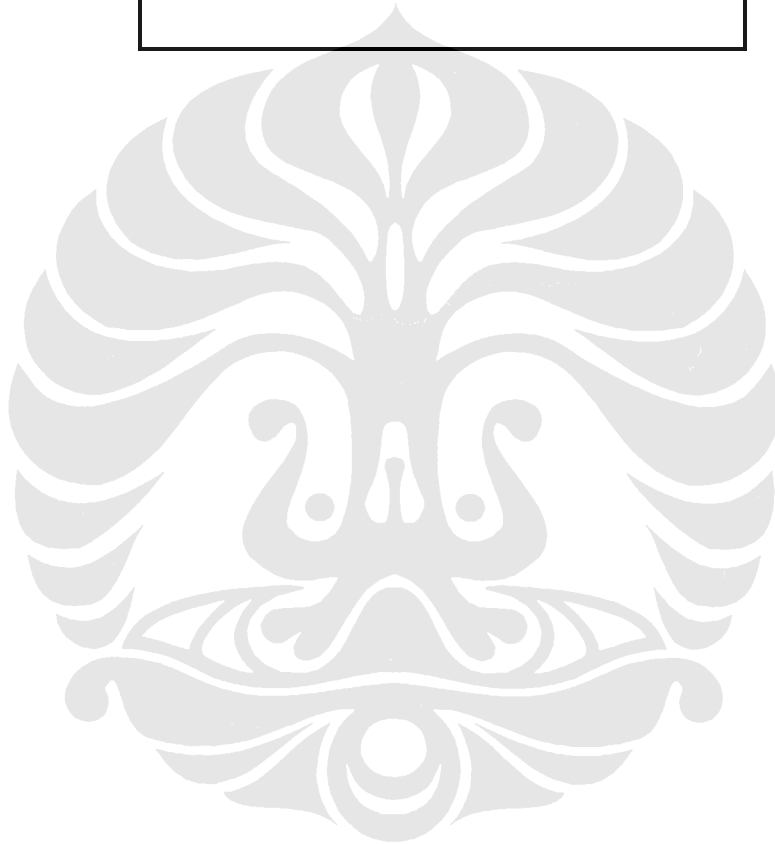
$$\text{R} = 0,0135888$$

Rasio Geser

$$\text{Vu} = 2,561$$

$$\phi \text{ Vn} = 8,62809154$$

$$\text{R} = 0,296821144$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Balok

Rasio Lentur

Rasio Lendutan

$$M_u = 13,2389$$

$$\delta_u = 0,115482$$

$$\phi M_n = 30,40053993$$

$$\delta_n = 1,458333333$$

$$R = 0,435482397$$

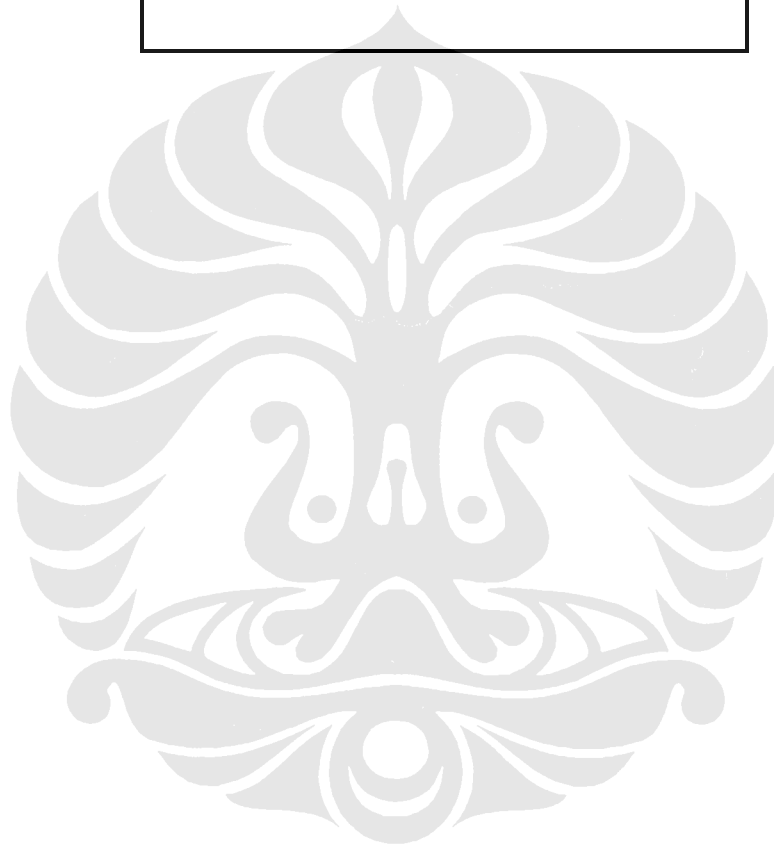
$$R = 0,079187657$$

Rasio Geser

$$V_u = 29,663$$

$$\phi V_n = 30,64204006$$

$$R = 0,968049123$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

Rasio Lendutan

$$M_u = 1,1892$$

$$\delta_u = 0,079641$$

$$\phi M_n = 24,20175772$$

$$\delta_n = 1,458333333$$

$$R = 0,049136927$$

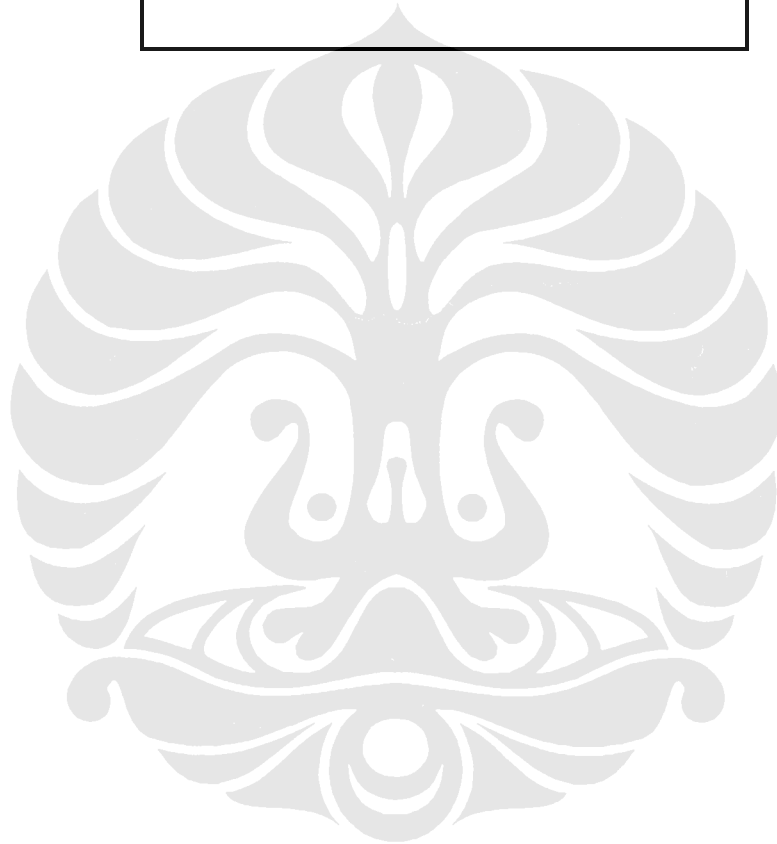
$$R = 0,054610971$$

Rasio Geser

$$V_u = 3,052$$

$$\phi V_n = 31,01572347$$

$$R = 0,098401703$$



RT Cara Tradisional 2 Lantai

Kolom lt.1

Arah - X

f_c' =	27,5	MPa	A_s =	6 D D 16	=	1206,37158	ir	L =	3000	mm
f_y =	400	MPa	A_s' =	5 D D 16	=	1005,30965	ir	b =	100	mm
E_s =	200000	MPa	A_{st} =			2211,681228	ir	h =	400	mm
			A_g =			40000	ir	d' =	36	mm
								d =	364	mm
D 8 - 200										
A_v =	50,265		ϵ_{Cu} =	0,003		a =	185,64	X_{Cc} =	271,18	
V_c =	36,36354	kN	ϵ_s =	0,002		C_c =	433,9335	$X_{Cs'}$ =	328	
V_s =	0,000	kN	C =	218,4		C_s' =	378,625	X_{Pn} =	164	
V_n =	27,273	kN	ϵ_b =	0,0025		T_s =	482,549			
$V_u \leq \phi V_n$			ϵ_s' =	0,0025		P_n =	330,010	M_n =	187,741	
1,236	\leq	20,454489ok!							
						80,085	\leq	264,007692ok!	
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$				
0,006307	\leq	2,5714286ok!							
						1,496	\leq	150,193141ok!	

Arah - Y

f_c' =	27,5	MPa	A_s =	5 D D 16	=	1005,30965	ir	L =	3000	mm
f_y =	400	MPa	A_s' =	6 D D 16	=	1206,37158	ir	b =	400	mm
E_s =	200000	MPa	A_{st} =			2211,681228	ir	h =	100	mm
			A_g =			40000	ir	d' =	36	mm
								d =	64	mm
D 8 - 200										
A_v =	50,265		ϵ_{Cu} =	0,003		a =	32,64	X_{Cc} =	47,68	
V_c =	25,57435	kN	ϵ_s =	0,002		C_c =	305,184	$X_{Cs'}$ =	28	
V_s =	0,000	kN	C =	38,4		C_s' =	454,350	X_{Pn} =	14	
V_n =	19,181	kN	ϵ_b =	0,0048		T_s =	402,124			
$V_u \leq \phi V_n$			ϵ_s' =	0,0002		P_n =	357,410	M_n =	22,269	
1,208	\leq	14,385575ok!							
						80,085	\leq	285,927869ok!	
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$				
0,003343	\leq	2,5714286ok!							
						1,0638	\leq	17,8153815ok!	

Kolom lt.2

Arah - X

f_c'	=	27,5	MPa	A_s	=	2 D D 12	=	226,194671	mm ²	L	=	3000	mm	
f_y	=	400	MPa	A_s'	=	2 D D 12	=	226,194671	mm ²	b	=	100	mm	
E_s	=	200000	MPa	A_{st}	=		=	452,3893421	mm ²	h	=	200	mm	
				A_g	=		=	20000	mm ²	d'	=	32	mm	
										d	=	168	mm	
D 6	-	200		ϵ_{Cu}	=	0,003		a	=	85,68		X_{Cc}	=	125,16
A_v	=	28,274		ϵ_s	=	0,002		C_c	=	200,277		$X_{Cs'}$	=	136
V_c	=	15,2586	kN	C	=	100,8		C_s'	=	85,191		X_{Pn}	=	68
V_s	=	0,000	kN	ϵ_b	=	0,0030		T_s	=	90,478				
V_n	=	11,444	kN	ϵ_s'	=	0,0020		P_n	=	194,990		M_n	=	23,393
V_u	\leq	ϕV_n						P_u	\leq	ϕP_n				
		0,746	\leq	8,58296ok!					10,97	\leq	155,99176ok!	
δ_u	\leq	δ_n						M_u	\leq	ϕM_n				
		0,016444	\leq	2,5714286ok!					0,1753	\leq	18,7146296ok!	

Arah - Y

f_c'	=	27,5	MPa	A_s	=	2 D D 12	=	226,194671	mm ²	L	=	3000	mm	
f_y	=	400	MPa	A_s'	=	2 D D 12	=	226,194671	mm ²	b	=	200	mm	
E_s	=	200000	MPa	A_{st}	=		=	452,3893421	mm ²	h	=	100	mm	
				A_g	=		=	20000	mm ²	d'	=	32	mm	
										d	=	68	mm	
D 6	-	200		ϵ_{Cu}	=	0,003		a	=	34,68		X_{Cc}	=	50,66
A_v	=	28,274		ϵ_s	=	0,002		C_c	=	162,129		$X_{Cs'}$	=	36
V_c	=	12,3522	kN	C	=	40,8		C_s'	=	85,191		X_{Pn}	=	18
V_s	=	0,000	kN	ϵ_b	=	0,0044		T_s	=	90,478				
V_n	=	9,264	kN	ϵ_s'	=	0,0006		P_n	=	156,842		M_n	=	8,457
V_u	\leq	ϕV_n						P_u	\leq	ϕP_n				
		0,058	\leq	6,9481105ok!					10,97	\leq	125,47336ok!	
δ_u	\leq	δ_n						M_u	\leq	ϕM_n				
		0,033845	\leq	2,5714286ok!					1,4847	\leq	6,765732ok!	

Ring balok

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 2 \text{ D } 10 = 157,079633 \text{ nr} & b &= 100 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 100 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 10 & d' &= 35 \text{ mm} \\
 & & & & d &= 65 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 D \ 10 &= 200 \\
 A_v &= 78,540 & a &= 26,8799371 \\
 V_c &= 5,681 \text{ kN} & M_n &= 3,23961232 \text{ kNm} \\
 V_s &= 0,000 \text{ kN} \\
 V_n &= 4,261 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 1,334 &\leq 3,1955895 \dots \text{ok!} & 0,7221 &\leq 2,59168986 \dots \text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,061488 &\leq 1,4583333 \dots \text{ok!}
 \end{aligned}$$

Balok

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 6 \text{ D } 12 = 678,584013 \text{ nr} & b &= 100 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 300 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 10 & d' &= 36 \text{ mm} \\
 & & & & d &= 264 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 D \ 10 &= 200 \\
 A_v &= 78,540 & a &= 116,121328 \\
 V_c &= 23,074 \text{ kN} & M_n &= 55,8988564 \text{ kNm} \\
 V_s &= 82,938 \text{ kN} \\
 V_n &= 79,509 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 23,504 &\leq 59,63166 \dots \text{ok!} & 5,5327 &\leq 44,7190851 \dots \text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,051987 &\leq 1,4583333 \dots \text{ok!}
 \end{aligned}$$

Sloof

$$\begin{aligned}
 f_c' &= 27,5 \text{ MPa} & A_s &= 6 \text{ D } 12 = 678,584013 \text{ nr} & b &= 100 \text{ mm} \\
 f_y &= 400 \text{ MPa} & & & h &= 250 \text{ mm} \\
 E_s &= 200000 \text{ MPa} & A_v &= \text{D } 10 & d' &= 36 \text{ mm} \\
 & & & & d &= 214 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 D \ 10 &= 200 \\
 A_v &= 78,540 & a &= 116,121328 \\
 V_c &= 18,704 \text{ kN} & M_n &= 42,3271761 \text{ kNm} \\
 V_s &= 67,230 \text{ kN} \\
 V_n &= 64,450 \text{ kN}
 \end{aligned}$$

$$\begin{aligned}
 V_u &\leq \phi V_n & M_u &\leq \phi M_n \\
 1,704 &\leq 48,337785 \dots \text{ok!} & 0,8364 &\leq 33,8617409 \dots \text{ok!} \\
 \delta_u &\leq \delta_n \\
 0,05368 &\leq 1,4583333 \dots \text{ok!}
 \end{aligned}$$

RT Cara Tradisional 2 Lantai

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Kolom lt.1

Rasio Aksial

$$\begin{aligned} P_u &= 80,085 \\ \phi P_n &= 264,007692 \\ R &= 0,303343434 \end{aligned}$$

Rasio Lentur

Arah X

$$\begin{aligned} M_u &= 1,496 \\ \phi M_n &= 150,1931412 \\ R &= 0,009960508 \end{aligned}$$

Arah Y

$$\begin{aligned} M_u &= 1,0638 \\ \phi M_n &= 17,81538152 \\ R &= 0,059712446 \end{aligned}$$

Rasio Geser

Arah X

$$\begin{aligned} V_u &= 1,236 \\ \phi V_n &= 20,45448879 \\ R &= 0,060426834 \end{aligned}$$

Arah Y

$$\begin{aligned} V_u &= 1,208 \\ \phi V_n &= 14,38557453 \\ R &= 0,08397301 \end{aligned}$$

Rasio Lendutan

Arah X

$$\begin{aligned} \delta u &= 0,006307 \\ \delta n &= 2,571428571 \\ R &= 0,002452722 \end{aligned}$$

Arah Y

$$\begin{aligned} \delta u &= 0,003343 \\ \delta n &= 2,571428571 \\ R &= 0,001300056 \end{aligned}$$

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Kolom lt.2

Rasio Aksial

$$P_u = 10,97$$

$$\phi P_n = 125,4733597$$

$$R = 0,087428917$$

Rasio Lentur

Arah X

$$M_u = 0,1753$$

$$\phi M_n = 18,7146296$$

$$R = 0,009367003$$

Arah Y

$$M_u = 1,4847$$

$$\phi M_n = 6,765731996$$

$$R = 0,219444105$$

Rasio Geser

Arah X

$$V_u = 0,746$$

$$\phi V_n = 8,582959984$$

$$R = 0,086916402$$

Arah Y

$$V_u = 0,058$$

$$\phi V_n = 6,948110463$$

$$R = 0,008347593$$

Rasio Lendutan

Arah X

$$\delta u = 0,016444$$

$$\delta n = 2,571428571$$

$$R = 0,006394889$$

Arah Y

$$\delta u = 0,033845$$

$$\delta n = 2,571428571$$

$$R = 0,013161944$$

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\mu_u = 0,7221$$

$$\phi M_n = 2,591689855$$

$$R = 0,278621301$$

Rasio Lendutan

$$\delta_u = 0,061488$$

$$\delta_n = 1,458333333$$

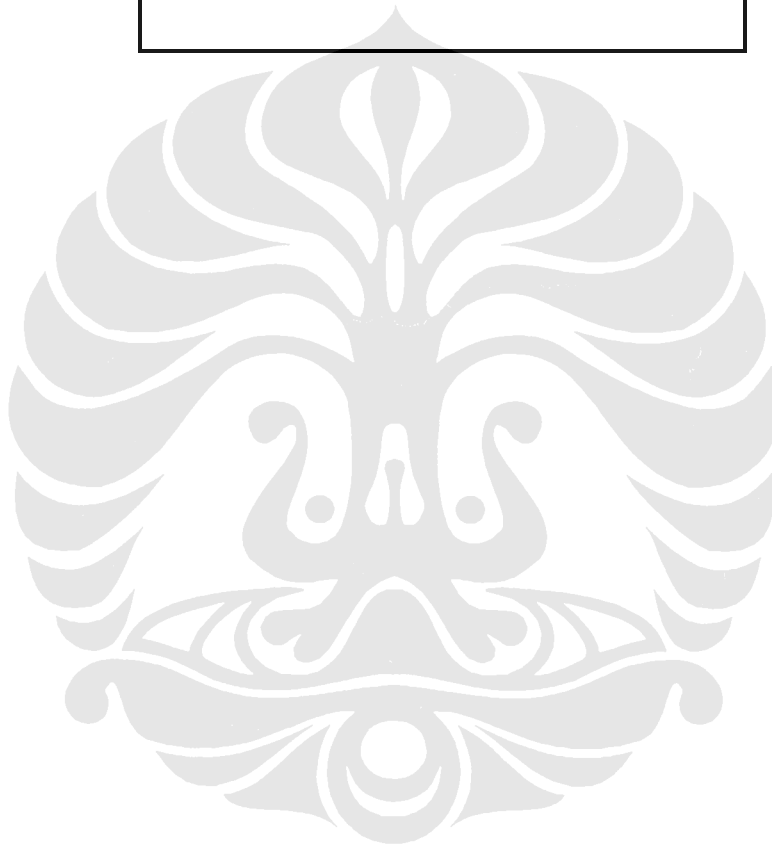
$$R = 0,0421632$$

Rasio Geser

$$V_u = 1,334$$

$$\phi V_n = 3,195589459$$

$$R = 0,417450369$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Balok

Rasio Lentur

Rasio Lendutan

$$\mu_u = 5,5327$$

$$\delta_u = 0,051987$$

$$\phi M_n = 44,7190851$$

$$\delta_n = 1,458333333$$

$$R = 0,123721225$$

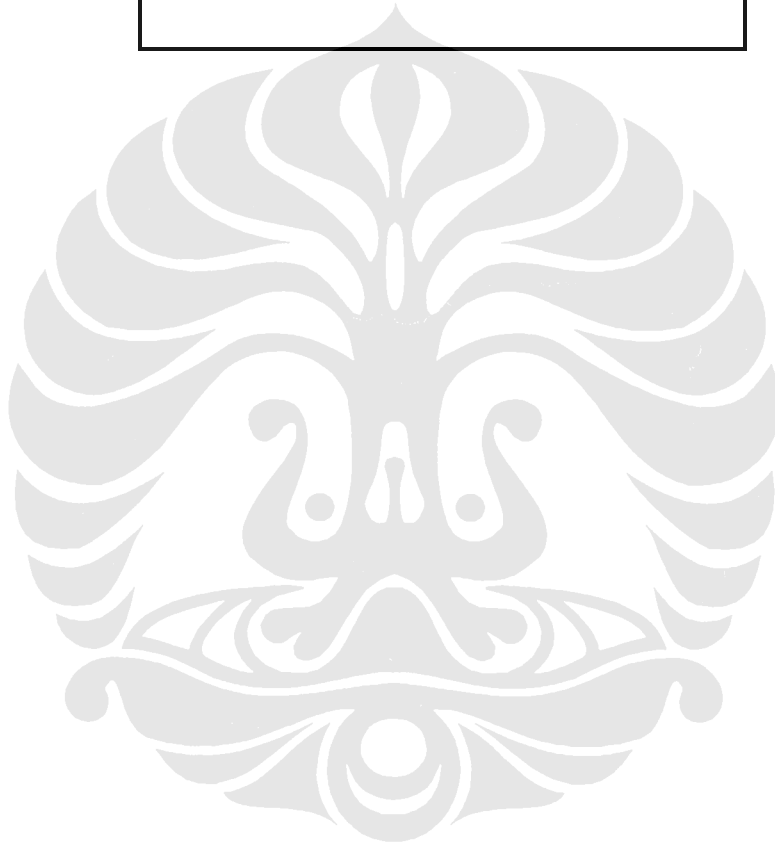
$$R = 0,035648229$$

Rasio Geser

$$V_u = 23,504$$

$$\phi V_n = 59,6316604$$

$$R = 0,394153036$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

Rasio Lendutan

$$\mu_u = 0,8364$$

$$\delta_u = 0,05368$$

$$\phi M_n = 33,86174089$$

$$\delta_n = 1,458333333$$

$$R = 0,024700443$$

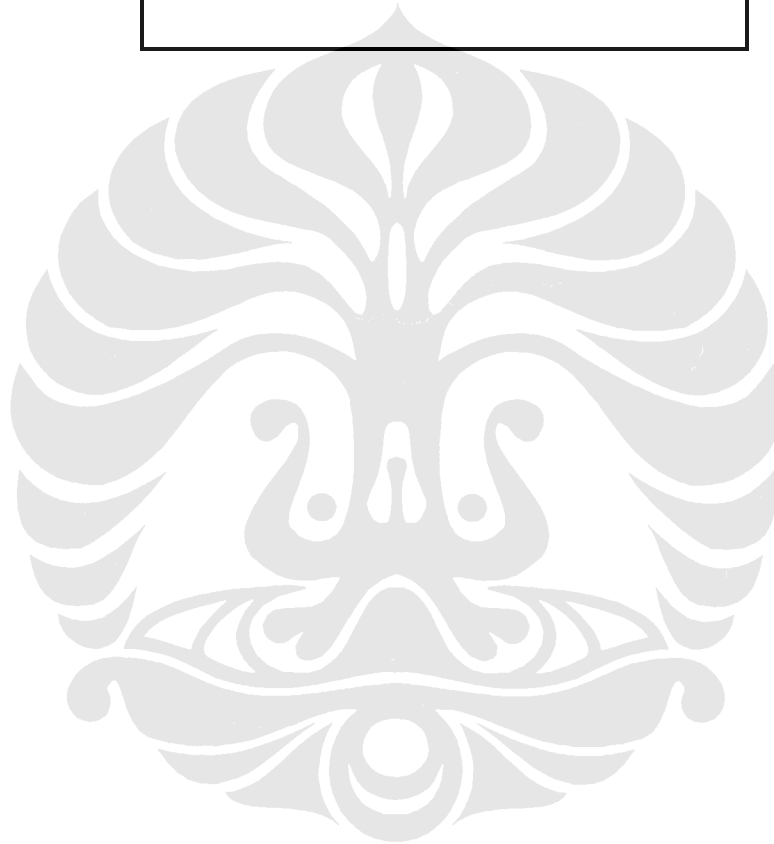
$$R = 0,036809143$$

Rasio Geser

$$V_u = 1,704$$

$$\phi V_n = 48,33778533$$

$$R = 0,035251925$$



RT Baja 1 Lantai

Kolom lt.1

Arah - X

f_c'	=	27,5	MPa	A_s	=	3 D D 12	=	339,292007	π	L	=	3000	mm																																																				
f_y	=	400	MPa	A_s'	=	3 D D 12	=	339,292007	π	b	=	200	mm																																																				
E_s	=	200000	MPa	A_{st}	=	678,5840132	π	h	=	200	=	32	mm																																																				
				A_g	=	40000	π	d'	=	168	=	168	mm																																																				
<p>D 6 - 200</p> <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 25%;">Av = 28,274</td> <td style="width: 25%;">E_{Cu} = 0,003</td> <td style="width: 25%;">a = 85,68</td> <td style="width: 25%;">XC_c = 125,16</td> </tr> <tr> <td>V_c = 30,28095 kN</td> <td>ε_s = 0,002</td> <td>C_c = 400,554</td> <td>XC_{s'} = 136</td> </tr> <tr> <td>V_s = 0,000 kN</td> <td>C = 100,8</td> <td>C_{s'} = 127,786</td> <td>XP_n = 68</td> </tr> <tr> <td>V_n = 22,711 kN</td> <td>ε_b = 0,0030</td> <td>T_s = 135,717</td> <td></td> </tr> <tr> <td>V_u ≤ φV_n</td> <td>ε_{s'} = 0,0020</td> <td>P_n = 392,623</td> <td>M_n = 40,814</td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">3,269</td> <td style="text-align: center;">≤</td> <td style="text-align: center;">17,033033</td> <td style="text-align: center;">.....ok!</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td style="border: 1px solid black; text-align: center;">17,435</td> <td style="text-align: center;">≤</td> </tr> <tr> <td></td> <td></td> <td style="text-align: center;">314,098439</td> <td style="text-align: center;">.....ok!</td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">0,049348</td> <td style="text-align: center;">≤</td> <td style="text-align: center;">2,5714286</td> <td style="text-align: center;">.....ok!</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td style="border: 1px solid black; text-align: center;">7,8769</td> <td style="text-align: center;">≤</td> </tr> <tr> <td></td> <td></td> <td style="text-align: center;">32,6510777</td> <td style="text-align: center;">.....ok!</td> </tr> </table>														Av = 28,274	E _{Cu} = 0,003	a = 85,68	XC _c = 125,16	V _c = 30,28095 kN	ε _s = 0,002	C _c = 400,554	XC _{s'} = 136	V _s = 0,000 kN	C = 100,8	C _{s'} = 127,786	XP _n = 68	V _n = 22,711 kN	ε _b = 0,0030	T _s = 135,717		V _u ≤ φV _n	ε _{s'} = 0,0020	P _n = 392,623	M _n = 40,814	3,269	≤	17,033033ok!							17,435	≤			314,098439ok!	0,049348	≤	2,5714286ok!							7,8769	≤			32,6510777ok!
Av = 28,274	E _{Cu} = 0,003	a = 85,68	XC _c = 125,16																																																														
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0,049348	≤	2,5714286ok!																																																														
		7,8769	≤																																																														
		32,6510777ok!																																																														

Arah - Y

f_c'	=	27,5	MPa	A_s	=	3 D D 12	=	339,292007	π	L	=	3000	mm																																																				
f_y	=	400	MPa	A_s'	=	3 D D 12	=	339,292007	π	b	=	200	mm																																																				
E_s	=	200000	MPa	A_{st}	=	678,5840132	π	h	=	200	=	32	mm																																																				
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Av = 28,274	E _{Cu} = 0,003	a = 85,68	XC _c = 125,16																																																														
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0,039377	≤	2,5714286ok!																																																														
		0,8031	≤																																																														
		32,6510777ok!																																																														

Ring balok

$$\begin{array}{lcl}
 f_c' & = & 27,5 \text{ MPa} \\
 f_y & = & 400 \text{ MPa} \\
 E_s & = & 200000 \text{ MPa}
 \end{array}
 \quad
 \begin{array}{lcl}
 A_s & = & 2 \text{ D D } 10 = 157,079633 \pi \\
 A_v & = & \text{D D } 6
 \end{array}
 \quad
 \begin{array}{lcl}
 b & = & 150 \text{ mm} \\
 h & = & 150 \text{ mm} \\
 d' & = & 31 \text{ mm} \\
 d & = & 119 \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 6 & - & 200 \\
 A_v & = & 28,274 \\
 V_c & = & 15,601 \text{ kN} \\
 V_s & = & 0,000 \text{ kN} \\
 V_n & = & 11,701 \text{ kN} \\
 V_u & \leq & \phi V_n
 \end{array}
 \quad
 \begin{array}{lcl}
 a & = & 17,9199581 \\
 M_n & = & 6,91401843 \text{ kNm} \\
 M_u & \leq & \phi M_n
 \end{array}$$

$$\begin{array}{lcl}
 2,688 & \leq & 8,7755803 \dots\dots\dots\text{ok!} \\
 \delta_u & \leq & \delta_n \\
 0,018674 & \leq & 1,4583333 \dots\dots\dots\text{ok!}
 \end{array}
 \quad
 \begin{array}{lcl}
 1,7748 & \leq & 5,53121474 \dots\dots\dots\text{ok!}
 \end{array}$$

Sloof

$$\begin{array}{lcl}
 f_c' & = & 27,5 \text{ MPa} \\
 f_y & = & 400 \text{ MPa} \\
 E_s & = & 200000 \text{ MPa}
 \end{array}
 \quad
 \begin{array}{lcl}
 A_s & = & 5 \text{ D D } 12 = 565,486678 \pi \\
 A_v & = & \text{D D } 8
 \end{array}
 \quad
 \begin{array}{lcl}
 b & = & 150 \text{ mm} \\
 h & = & 200 \text{ mm} \\
 d' & = & 34 \text{ mm} \\
 d & = & 166 \text{ mm}
 \end{array}$$

$$\begin{array}{lcl}
 \text{D } 8 & - & 200 \\
 A_v & = & 50,265 \\
 V_c & = & 21,763 \text{ kN} \\
 V_s & = & 33,376 \text{ kN} \\
 V_n & = & 41,354 \text{ kN} \\
 V_u & \leq & \phi V_n
 \end{array}
 \quad
 \begin{array}{lcl}
 a & = & 64,5118491 \\
 M_n & = & 30,2521971 \text{ kNm} \\
 M_u & \leq & \phi M_n
 \end{array}$$

$$\begin{array}{lcl}
 24,976 & \leq & 31,015723 \dots\dots\dots\text{ok!} \\
 \delta_u & \leq & \delta_n \\
 0,08631 & \leq & 1,4583333 \dots\dots\dots\text{ok!}
 \end{array}
 \quad
 \begin{array}{lcl}
 14,3512 & \leq & 24,2017577 \dots\dots\dots\text{ok!}
 \end{array}$$

RT Baja 1 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt.1			
Rasio Aksial			
Pu	=	17,435	
ϕP_n	=	314,0984395	
R	=	0,055508076	
Rasio Lentur			
Arah X		Arah Y	
Mu	=	7,8769	Mu = 0,8031
ϕM_n	=	32,65107772	$\phi M_n = 32,65107772$
R	=	0,241244717	R = 0,024596432
Rasio Geser			
Arah X		Arah Y	
Vu	=	3,269	Vu = 0,244
ϕV_n	=	17,03303261	$\phi V_n = 17,03303261$
R	=	0,191921197	R = 0,014325106
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,049348	$\delta u = 0,039377$
δn	=	2,571428571	$\delta n = 2,571428571$
R	=	0,019190889	R = 0,015313278

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\mu_u = 1,7748$$

$$\phi M_n = 5,531214743$$

$$R = 0,320869842$$

Rasio Lendutan

$$\delta_u = 0,018674$$

$$\delta_n = 1,458333333$$

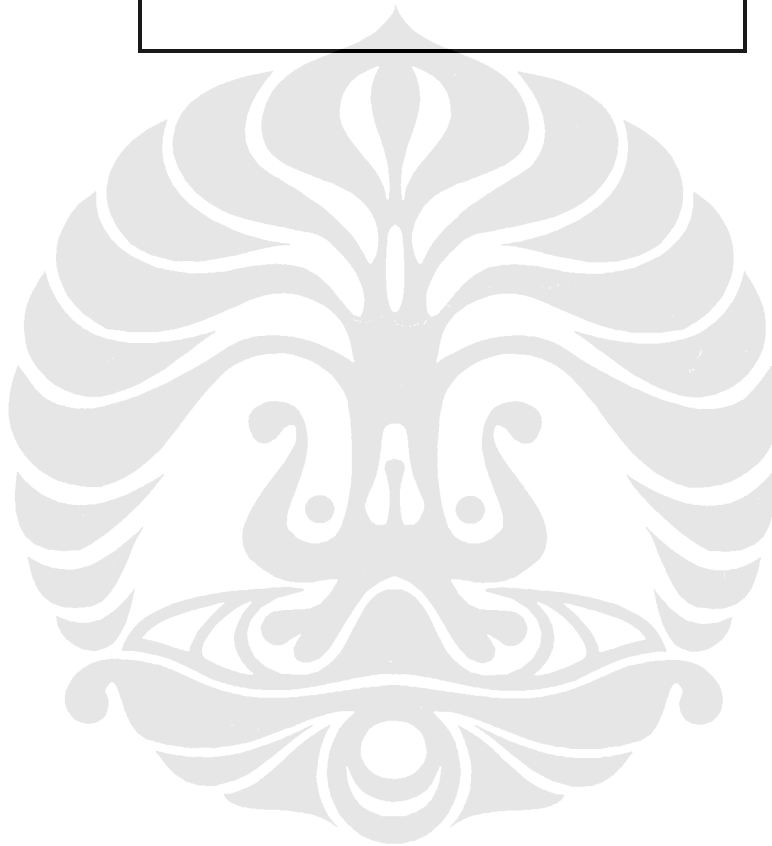
$$R = 0,012805029$$

Rasio Geser

$$V_u = 2,688$$

$$\phi V_n = 8,775580284$$

$$R = 0,306304531$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

Rasio Lendutan

$$M_u = 14,3512$$

$$\delta u = 0,08631$$

$$\phi M_n = 24,20175772$$

$$\delta n = 1,458333333$$

$$R = 0,592981723$$

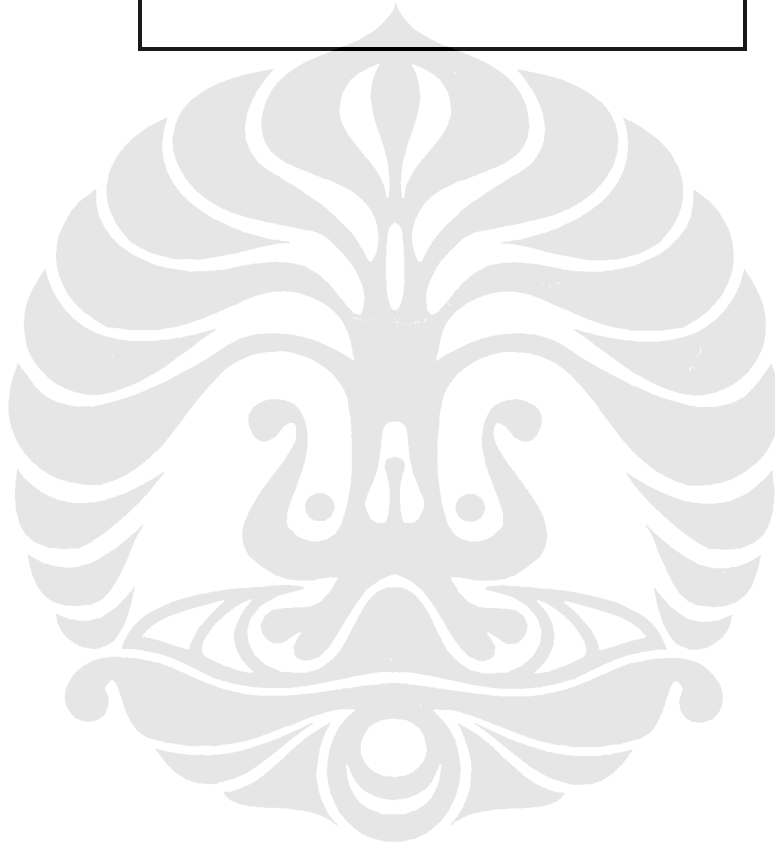
$$R = 0,059184$$

Rasio Geser

$$V_u = 24,976$$

$$\phi V_n = 31,01572347$$

$$R = 0,80526898$$



RT Cara Tradisional 1 Lantai

Kolom lt.1

Arah - X

f_c' =	27,5	MPa	A_s =	3 D D 12	=	339,292007	ir	L =	3000	mm
f_y =	400	MPa	A_s' =	3 D D 12	=	339,292007	ir	b =	100	mm
E_s =	200000	MPa	A_{st} =			678,5840132	ir	h =	200	mm
			A_g =			20000	ir	d' =	32	mm
								d =	168	mm
D 6	- 200									
A_v =	28,274		ϵ_{Cu} =	0,003		a =	85,68	X_{Cc} =	125,16	
V_c =	15,26017	kN	ϵ_s =	0,002		C_c =	200,277	X_{Cs}' =	136	
V_s =	0,000	kN	C =	100,8		C_s' =	127,786	X_{Pn} =	68	
V_n =	11,445	kN	ϵ_b =	0,0030		T_s =	135,717			
$V_u \leq \phi V_n$			ϵ_s' =	0,0020		P_n =	192,346	M_n =	29,366	
1,104	≤	8,5838449ok!							
						$P_u \leq \phi P_n$				
						11	≤	153,876839ok!	
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$				
0,068481	≤	2,5714286ok!							
						2,4505	≤	23,4928111ok!	

Arah - Y

f_c' =	27,5	MPa	A_s =	3 D D 12	=	339,292007	ir	L =	3000	mm
f_y =	400	MPa	A_s' =	3 D D 12	=	339,292007	ir	b =	200	mm
E_s =	200000	MPa	A_{st} =			678,5840132	ir	h =	100	mm
			A_g =			20000	ir	d' =	32	mm
								d =	68	mm
D 6	- 200									
A_v =	28,274		ϵ_{Cu} =	0,003		a =	34,68	X_{Cc} =	50,66	
V_c =	12,35347	kN	ϵ_s =	0,002		C_c =	162,129	X_{Cs}' =	36	
V_s =	0,000	kN	C =	40,8		C_s' =	127,786	X_{Pn} =	18	
V_n =	9,265	kN	ϵ_b =	0,0044		T_s =	135,717			
$V_u \leq \phi V_n$			ϵ_s' =	0,0006		P_n =	154,198	M_n =	10,038	
0,423	≤	6,9488268ok!							
						$P_u \leq \phi P_n$				
						11	≤	123,358439ok!	
$\delta_u \leq \delta_n$						$M_u \leq \phi M_n$				
0,065253	≤	2,5714286ok!							
						1,2539	≤	8,03054474ok!	

Ring balok

f_c'	=	<input type="text" value="27,5"/> MPa	A_s	=	<input type="text" value="2"/> D <input type="text" value="D 10"/>	=	<input type="text" value="157,079633"/> tr	b	=	<input type="text" value="100"/> mm
f_y	=	<input type="text" value="400"/> MPa	A_v	=	<input type="text" value="D"/> D <input type="text" value="D 6"/>			h	=	<input type="text" value="100"/> mm
E_s	=	<input type="text" value="200000"/> MPa						d'	=	<input type="text" value="31"/> mm
								d	=	<input type="text" value="69"/> mm

D 6	-	200								
A_v	=	<input type="text" value="28,274"/>			a	=	<input type="text" value="26,8799371"/>			
V_c	=	<input type="text" value="6,031"/> kN			M_n	=	<input type="text" value="3,49093973"/> kNm			
V_s	=	<input type="text" value="0,000"/> kN								
V_n	=	<input type="text" value="4,523"/> kN								
V_u	≤	ϕV_n			M_u	≤	ϕM_n			

<input type="text" value="1,387"/>	≤	<input type="text" value="3,3922411"/>ok!	<input type="text" value="0,8233"/>	≤	<input type="text" value="2,79275179"/>ok!
δ_u	≤	δ_n					
<input type="text" value="0,052537"/>	≤	<input type="text" value="1,4583333"/>ok!				

Sloof

f_c'	=	<input type="text" value="27,5"/> MPa	A_s	=	<input type="text" value="4"/> D <input type="text" value="D 12"/>	=	<input type="text" value="452,389342"/> tr	b	=	<input type="text" value="100"/> mm
f_y	=	<input type="text" value="400"/> MPa	A_v	=	<input type="text" value="D"/> D <input type="text" value="D 8"/>			h	=	<input type="text" value="250"/> mm
E_s	=	<input type="text" value="200000"/> MPa						d'	=	<input type="text" value="34"/> mm
								d	=	<input type="text" value="216"/> mm

D 8	-	200								
A_v	=	<input type="text" value="50,265"/>			a	=	<input type="text" value="77,414219"/>			
V_c	=	<input type="text" value="18,879"/> kN			M_n	=	<input type="text" value="32,0821656"/> kNm			
V_s	=	<input type="text" value="43,429"/> kN								
V_n	=	<input type="text" value="46,731"/> kN								
V_u	≤	ϕV_n			M_u	≤	ϕM_n			

<input type="text" value="27,038"/>	≤	<input type="text" value="35,048214"/>ok!	<input type="text" value="16,7073"/>	≤	<input type="text" value="25,6657325"/>ok!
δ_u	≤	δ_n					
<input type="text" value="0,076495"/>	≤	<input type="text" value="1,4583333"/>ok!				

RT Cara Tradisional 1 Lantai			
Perhitungan struktur terhadap kekuatan dan daya layan struktur			
Kolom lt. 1			
Rasio Aksial			
Pu	=	11	
ϕP_n	=	123,3584395	
R	=	0,089171037	
Rasio Lentur			
Arah X		Arah Y	
Mu	=	2,4505	Mu = 1,2539
ϕM_n	=	23,49281107	$\phi M_n = 8,030544738$
R	=	0,104308505	R = 0,156141338
Rasio Geser			
Arah X		Arah Y	
Vu	=	1,104	Vu = 0,423
ϕV_n	=	8,583844917	$\phi V_n = 6,948826837$
R	=	0,128613694	R = 0,060873585
Rasio Lendutan			
Arah X		Arah Y	
δu	=	0,068481	$\delta u = 0,065253$
δn	=	2,571428571	$\delta n = 2,571428571$
R	=	0,0266315	R = 0,025376167

Perhitungan struktur terhadap kekuatan dan daya layan struktur

Ring balok

Rasio Lentur

$$\mu_u = 0,8233$$

$$\phi M_n = 2,792751785$$

$$R = 0,294798845$$

Rasio Lendutan

$$\delta_u = 0,052537$$

$$\delta_n = 1,458333333$$

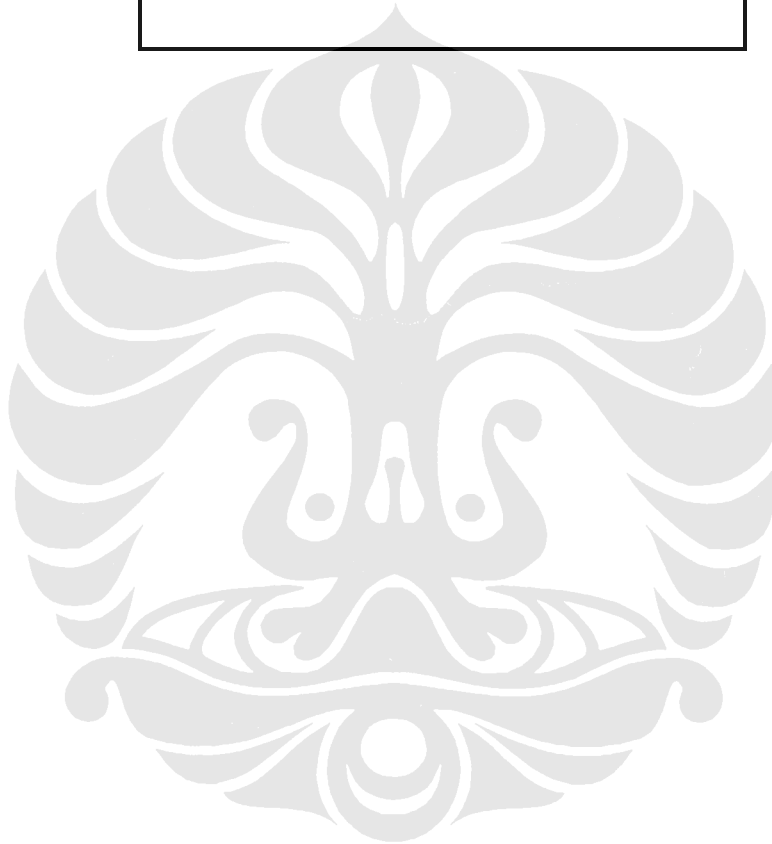
$$R = 0,036025371$$

Rasio Geser

$$V_u = 1,387$$

$$\phi V_n = 3,392241118$$

$$R = 0,408874237$$



Perhitungan struktur terhadap kekuatan dan daya layan struktur

Sloof

Rasio Lentur

Rasio Lendutan

$$M_u = 16,7073$$

$$\delta u = 0,076495$$

$$\phi M_n = 25,66573251$$

$$\delta n = 1,458333333$$

$$R = 0,650957458$$

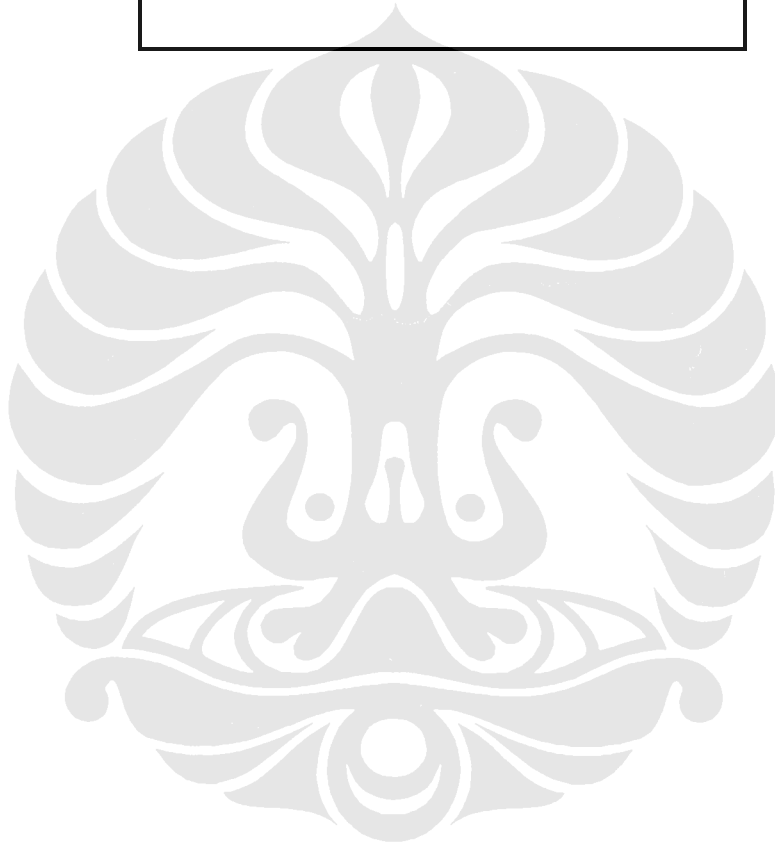
$$R = 0,052453714$$

Rasio Geser

$$V_u = 27,038$$

$$\phi V_n = 35,04821406$$

$$R = 0,771451577$$



Rumah tinggal 2 Lantai

Dengan Bekisting Baja

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	87,956	233,43435	0,3767912	0,3444	54,296706	0,0063429
Kolom lt.2	17,353	316,21336	0,0548775	0,2294	27,872896	0,0082302

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δ u	δ n	R	δ u	δ n	R
Kolom lt.1	2,834	18,658166	0,1518906	0,238	18,658166	0,0127558	0,004018	2,5714286	0,0015626	0,001876	2,5714286	0,0007296
Kolom lt.2	2,581	17,030614	0,1515506	0,058	17,030614	0,0034056	0,033878	2,5714286	0,0131748	0,022954	2,5714286	0,0089266

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δ u	δ n	R
Ring Balok	1,1315	2,8279363	0,4001151	2,561	8,6280915	0,2968211	0,019817	1,4583333	0,0135888
Balok	13,2389	30,40054	0,4354824	29,663	30,64204	0,9680491	0,115482	1,4583333	0,0791877
Sloof	1,1892	24,201758	0,0491369	3,052	31,015723	0,0984017	0,079641	1,4583333	0,054611

Dengan Bekisting Cara Tradisional

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	80,085	264,00769	0,3033434	1,496	150,19314	0,0099605
Kolom lt.2	10,97	125,47336	0,0874289	0,1753	18,71463	0,009367

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δ u	δ n	R	δ u	δ n	R
Kolom lt.1	1,236	20,454489	0,0604268	1,208	14,385575	0,083973	0,006307	2,5714286	0,0024527	0,003343	2,5714286	0,0013001
Kolom lt.2	0,746	8,58296	0,0869164	0,058	6,9481105	0,0083476	0,016444	2,5714286	0,0063949	0,033845	2,5714286	0,0131619

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δ u	δ n	R
Ring Balok	0,7221	2,5916899	0,2786213	1,334	3,1955895	0,4174504	0,061488	1,4583333	0,0421632
Balok	5,5327	44,719085	0,1237212	23,504	59,63166	0,394153	0,051987	1,4583333	0,0356482
Sloof	0,8364	33,861741	0,0247004	1,704	48,337785	0,0352519	0,05368	1,4583333	0,0368091

Rumah tinggal 1 Lantai

Dengan Bekisting Baja

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	17,435	314,09844	0,0555081	7,8769	32,651078	0,2412447

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δu	δn	R	δu	δn	R
Kolom lt.1	3,269	17,033033	0,1919212	0,244	17,033033	0,0143251	0,049348	2,5714286	0,0191909	0,039377	2,5714286	0,0153133

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δu	δn	R
	Ring Balok	1,7748	5,5312147	0,3208698	2,688	8,7755803	0,3063045	0,018674	1,4583333
Sloof	14,3512	24,201758	0,5929817	24,976	31,015723	0,805269	0,08631	1,4583333	0,059184

Dengan Bekisting Cara Tradisional

	Arah X			Arah Y		
	Pu	ϕ Pn	R	Mu	ϕ Mn	R
Kolom lt.1	11	123,35844	0,089171	2,4505	23,492811	0,1043085

	Arah X			Arah Y			Arah X			Arah Y		
	Vu	ϕ Vn	R	Vu	ϕ Vn	R	δu	δn	R	δu	δn	R
Kolom lt.1	1,104	8,5838449	0,1286137	0,423	6,9488268	0,0608736	0,068481	2,5714286	0,0266315	0,065253	2,5714286	0,0253762

	Mu	ϕ Mn	R	Vu	ϕ Vn	R	δu	δn	R
	Ring Balok	0,8233	2,7927518	0,2947988	1,387	3,3922411	0,4088742	0,052537	1,4583333
Sloof	16,7073	25,665733	0,6509575	27,038	35,048214	0,7714516	0,076495	1,4583333	0,0524537

Rumah tinggal 2 Lantai

Dengan Bekisting Baja

	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,422	0,152	0,013	0,002	0,001	-
Kolom lt.2	-	0,279	0,152	0,003	0,013	0,009	-
Ring Balok	0,400	-	0,297	-	-	-	0,014
Balok	0,435	-	0,968	-	-	-	0,079
Sloof	0,049	-	0,098	-	-	-	0,055

Dengan Bekisting Cara Tradisional

	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,373	0,060	0,084	0,002	0,001	-
Kolom lt.2	-	0,316	0,087	0,008	0,006	0,013	-
Ring Balok	0,279	-	0,417	-	-	-	0,042
Balok	0,124	-	0,394	-	-	-	0,036
Sloof	0,025	-	0,035	-	-	-	0,037

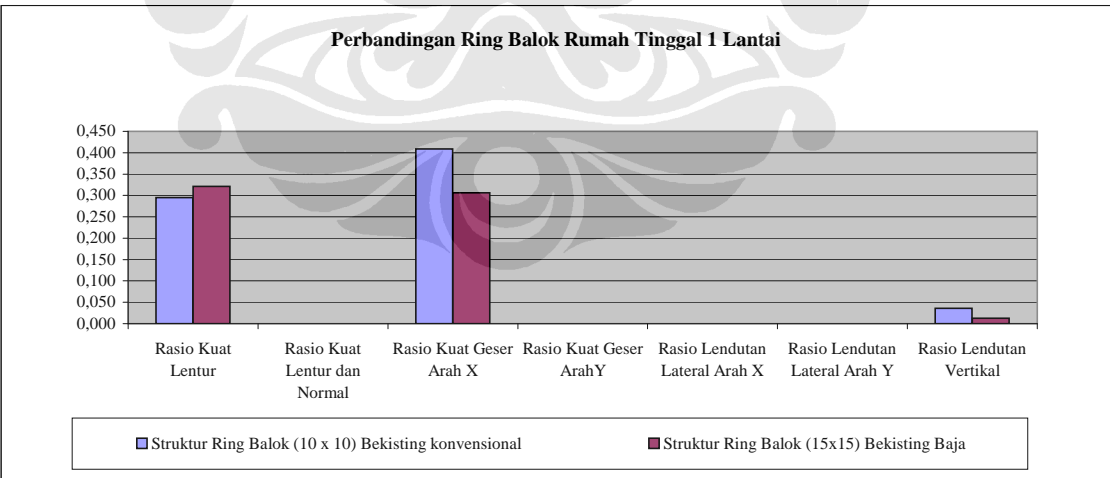
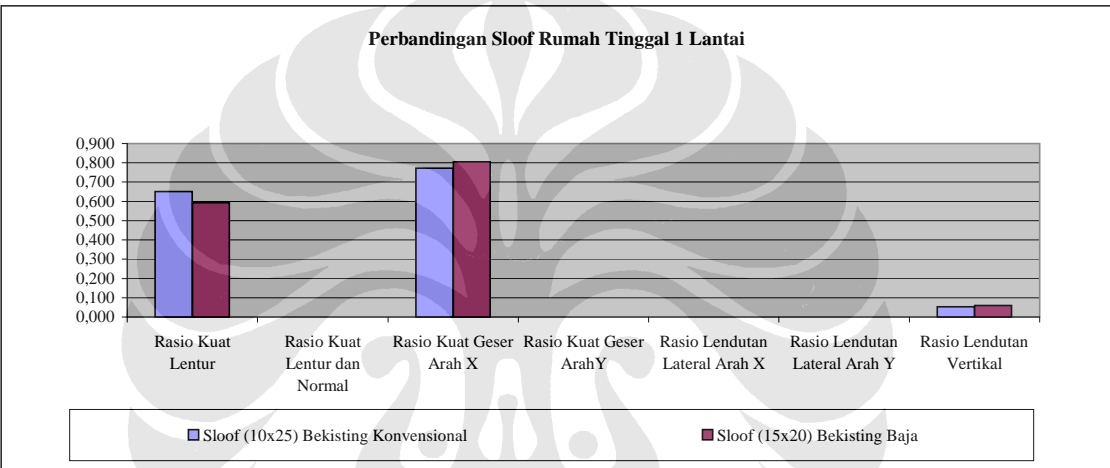
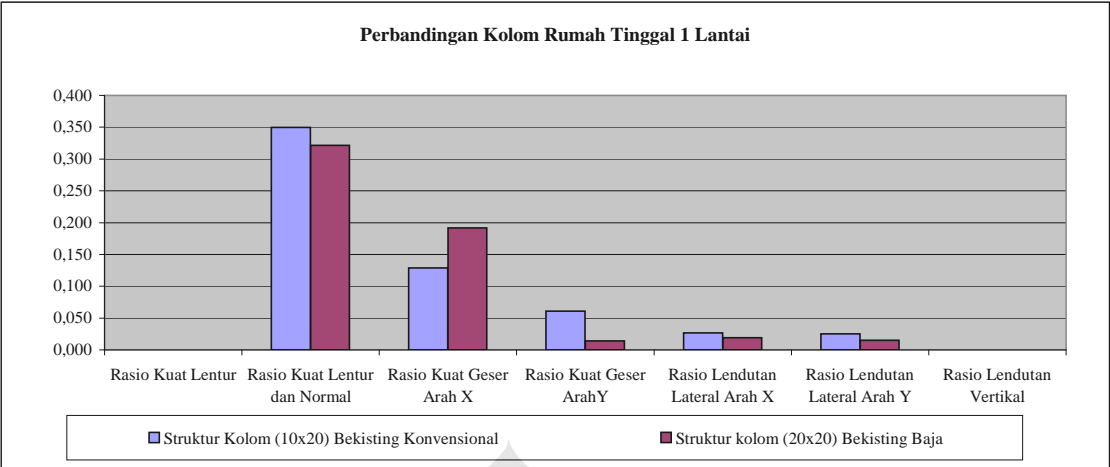
Rumah tinggal 1 Lantai

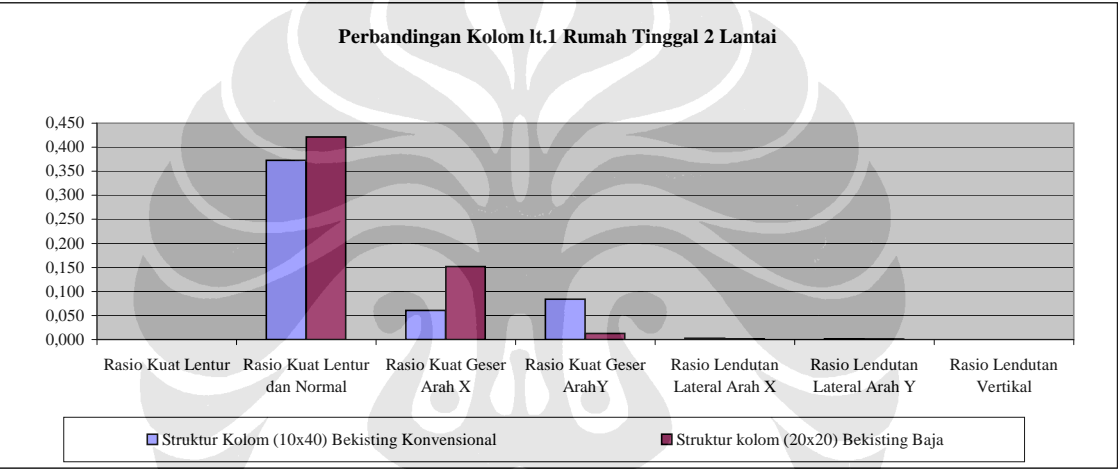
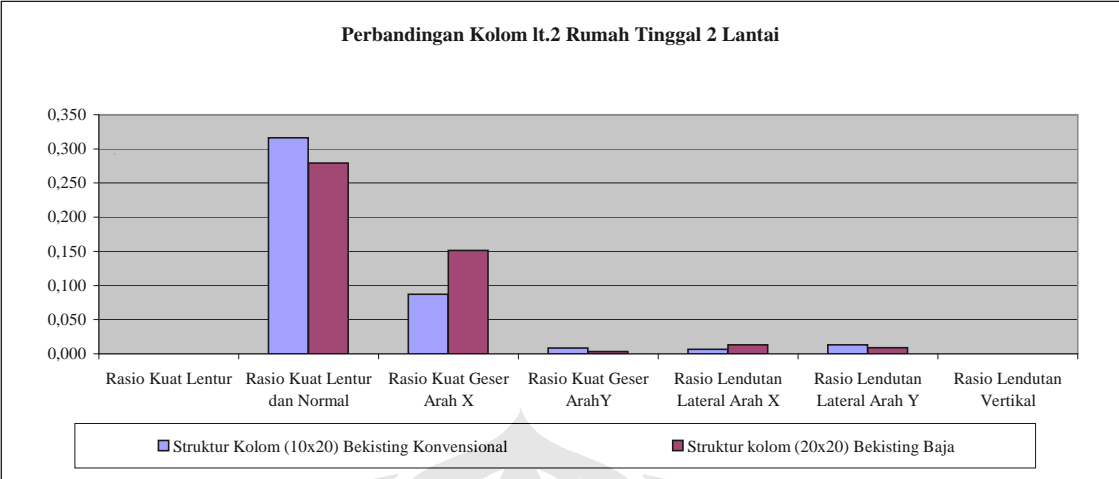
Dengan Bekisting Baja

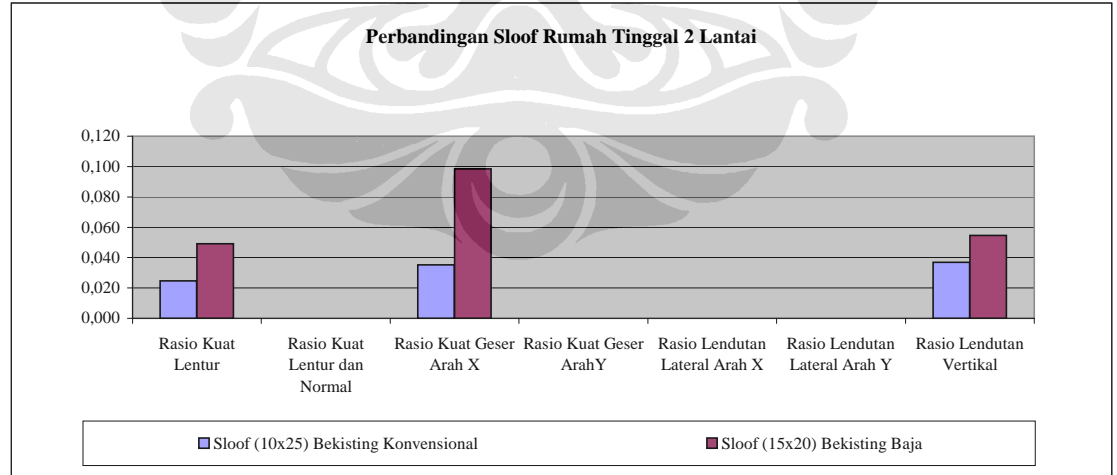
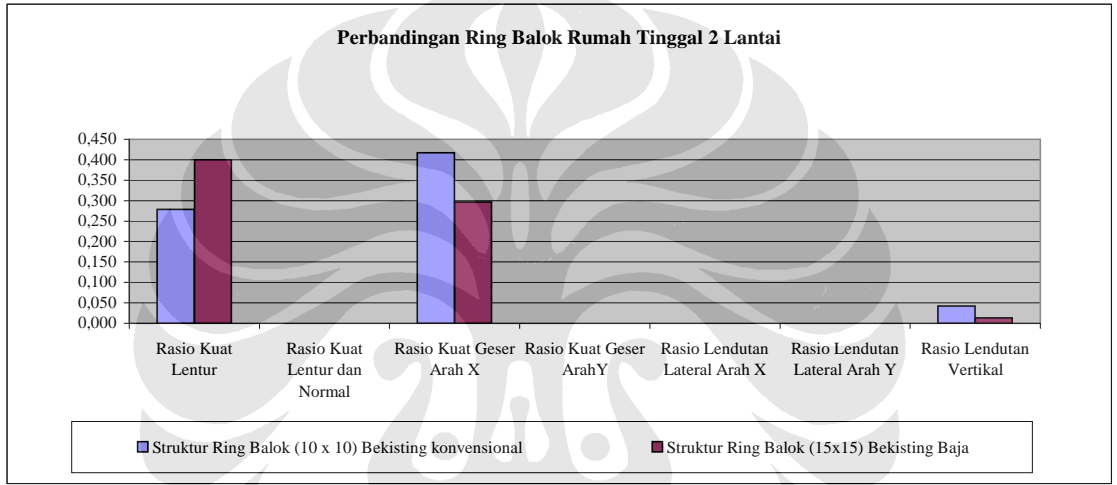
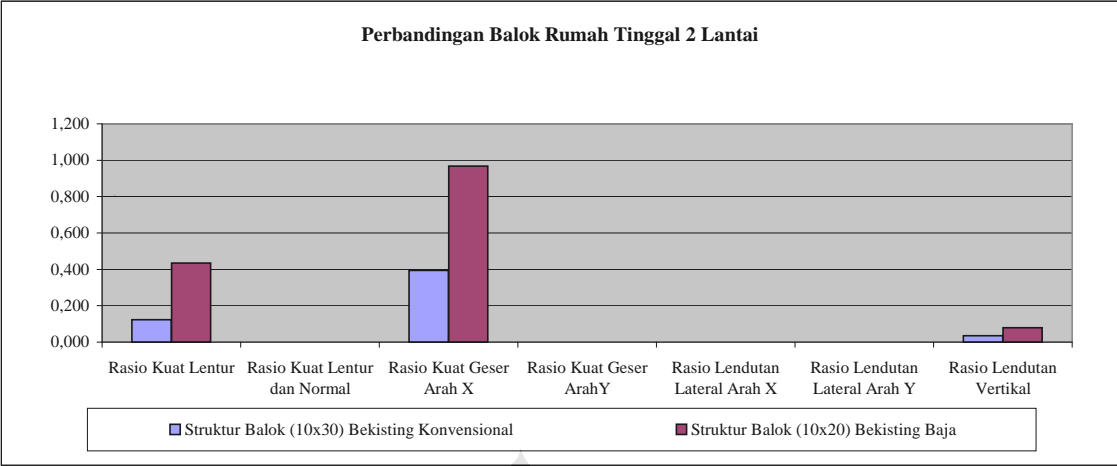
	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,321	0,192	0,014	0,019	0,015	-
Ring Balok	0,321	-	0,306	-	-	-	0,013
Sloof	0,593	-	0,805	-	-	-	0,059

Dengan Bekisting Cara Tradisional

	Rasio Kuat lentur	Rasio kuat lentur dan normal	Rasio kuat geser arah X	Rasio kuat geser arah Y	Rasio lendutan lateral arah X	Rasio lendutan lateral arah Y	Rasio lendutan vertikal
Kolom lt.1	-	0,350	0,129	0,061	0,027	0,025	-
Ring Balok	0,295	-	0,409	-	-	-	0,036
Sloof	0,651	-	0,771	-	-	-	0,052

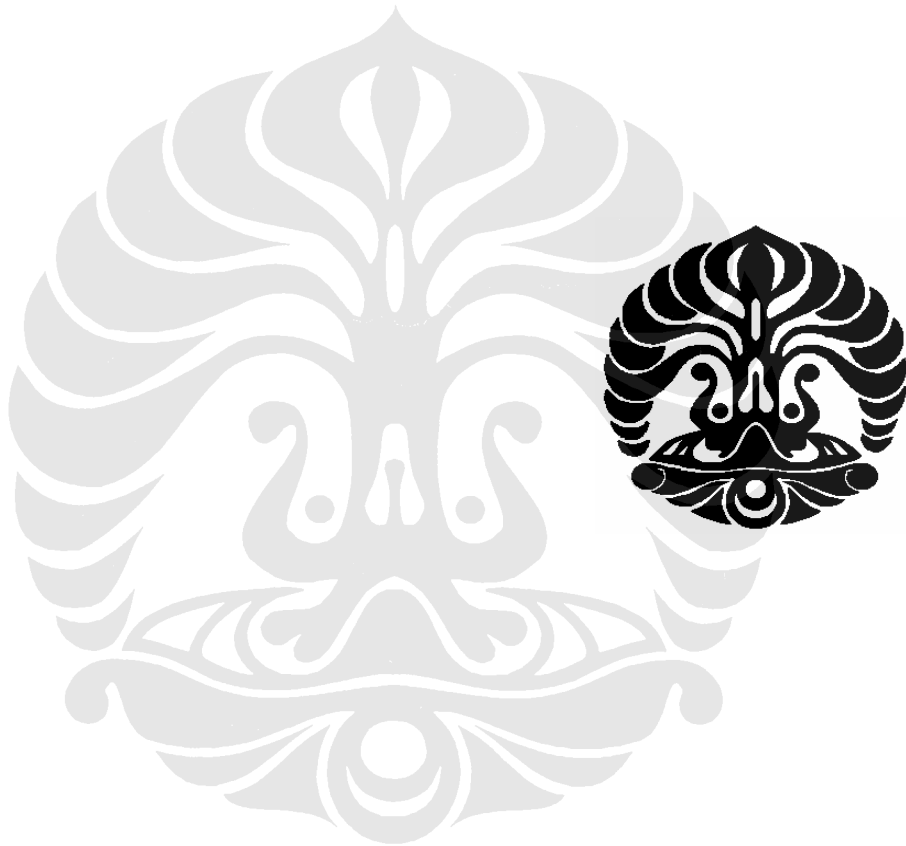






LAMPIRAN C1

Perhitungan Statika Bekisting Konvensional (Pondasi, Sloof, Kolom, Balok dan Ring Balok)



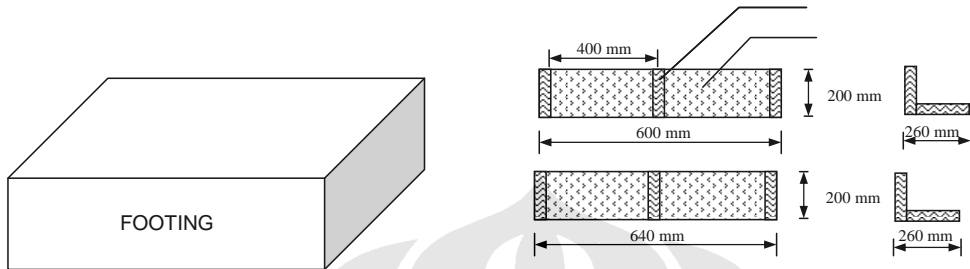
DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING FOOTING PONDASI

Bekisting cara tradisional untuk Pondasi

A. Data Dimensi Pondasi

- a. Tinggi Pondasi : 0,2 m
b. Lebar Pondasi : 0,6 m
c. Panjang Pondasi : 0,6 m

B. Data Rencana Material



Gambar Bekisting Footing Pondasi

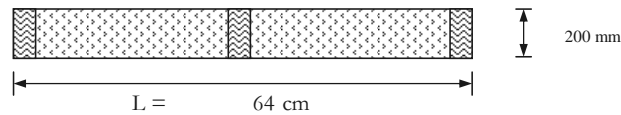
Keterangan Gambar :

- A : Bekisting kontak pipi
B : Rangka pipi horisontal
C : Rangka pipi vertikal

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Type
a.	Bekisting kontak pipi	Plat Baja	BJ 37
b.	Rangka pipi Horisontal	Plat Baja	BJ 37
c.	Rangka pipi Vertikal	Plat Baja	BJ 37

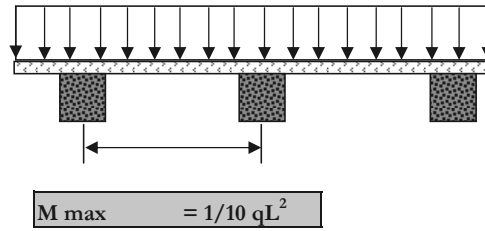
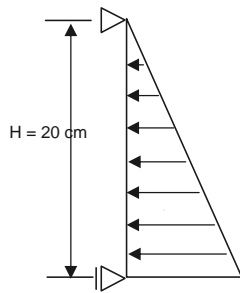
DESAIN SIDE BEAM
Tinjauan Plat Baja



1. Data teknis

A. - Kelas Kuat		=	III		
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	75	kg/cm ²	
- Tegangan geser ijin	$\bar{\tau}$	=	8	kg/cm ²	
- Berat jenis maksimum	γ_{max}	=	0,6	gr/cm ³	= 600 kg/m ³
- Berat jenis minimum	γ_{min}	=	0,4	gr/cm ³	= 400 kg/m ³
- Lendutan Maksimum	δ	=	$L / 300$	cm	= 0,2133333 cm
- Momen Inersia	I	=	$1/12 b h^3$	cm ⁴	= 13,333 cm ⁴
- Momen Lawan	W	=	$1/6 b h^2$	cm ³	= 13,333 cm ³
- Modulus elastisitas	E	=	80000	kg/cm ²	
B. Dimensi Tinjauan :					
- Tebal Papan	h	=	2	cm	= 0,02 m
- Lebar tinjauan	b	=	20	cm	= 0,2 m
C. Spec. Beton					
- Berat jenis beton basah	γ_{bt}	=	2500	kg/m ³	
- Tinggi pondasi	H	=	20	cm	= 0,2 m
- Lebar pondasi	B	=	60	cm	= 0,6 m
D. Asumsi Beban Kerja					
- Komposisi beban kerja		=	150	kg/m ²	
E. Faktor Koreksi material kayu					
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat		=	5/6		
		=	0,833		
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap		=	5/4		
		=	1,25		
F. Beban yang bekerja					
- Beban beton	q beton	=	$(2500 \times 0,2 \times 0,6)$	=	300 kg/m
- Beban kerja	q kerja	=	$(150 \times 0,2)$	=	30 kg/m
- Beban Plat kontak pipi	q plat pipi	=	$(600 \times 0,02 \times 0,2)$	=	2,4 kg/m
	q total	=		=	332,4 kg/m
		=		=	3,324 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned}
 M_{\max}/W &< \sigma_{\text{lt ijin}} \\
 1/8 qL^2 &< \sigma_{\text{lt ijin}} \times W \\
 1/10 \times 3,324 \times L^2 &< 1041,640625 \text{ kg/cm} \\
 L^2 &< 3133,70 \text{ cm}^2 \\
 L &< 55,979 \text{ cm}
 \end{aligned}$$

B. Lendutan

$$\begin{aligned}
 \frac{5 q \text{ tot } L^4}{384 \times E \times I} &< \frac{L}{300} \text{ cm} \\
 \frac{1 \times 3,324 \times L^3}{145 \times 80000 \times 13,333} &< \frac{1}{300} \text{ cm} \\
 L^3 &< \frac{154662800}{997,2} \text{ cm}^4 \\
 L &< 53,728 \text{ cm}
 \end{aligned}$$

jarak maksimal = 54 cm

4. Kesimpulan

kurang dari 54 cm

Pada perencanaan lapangan akan dipakai rangka vertikal dengan jarak 30 cm

DESAIN SIDE BEAM

Tinjauan rangka kaso vertikal 4/6 cm

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Tebal Papan	=	2 cm	=	0,02 m

B. Mutu balok 5/7 :

- Kelas Kuat	=	III	=	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	75 kg/cm ²	=	
- Tegangan geser ijin $\bar{\tau}$	=	8 kg/cm ²	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum δ	=	L / 300	=	cm
- Momen Inersia I	=	1/12 b h ³	=	72,000 cm ⁴
- Momen Lawan W	=	1/6 b h ²	=	24,000 cm ³
- Modulus elastisitas E	=	80000 kg/cm ²	=	

C. Dimensi Tinjauan :

- Tinggi kayu h	=	6 cm	=	0,06 m
- Lebar kayu b	=	4 cm	=	0,04 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	=	
- Tinggi pondasi H	=	20 cm	=	0,2 m
- Lebar Pondasi d	=	60 cm	=	0,6 m
- Jarak rangka vertikal L	=	30 cm	=	0,3 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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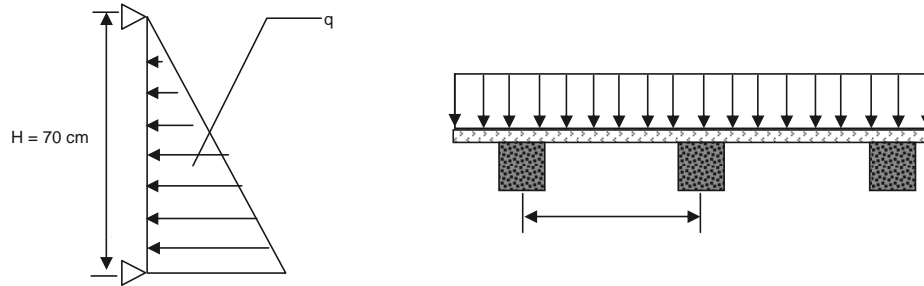
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1,25

G. Beban yang bekerja

- Beban beton q beton	=	(2500 x 0,2 x 0,6)	=	300 kg/m
- Beban kerja q kerja	=	(150 x 0,6)	=	90 kg/m
- Beban plywood q plywood	=	(600 x 0,2 x 0,02)	=	2,4 kg/m
- Beban sendiri 5/7 q 5/7	=	(600 x 0,06 x 0,04)	=	1,44 kg/m
		q total	=	393,84 kg/m
			=	3,938 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{10} qL^2 \\
 &= \frac{1}{10} \times 393,84 \times (0,3)^2 \\
 &= 4,431 \text{ kg.m} = 443,07 \text{ kg.cm}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 393,84 \times 0,3 \\
 &= 59,076 \text{ kg}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{1}{145} \frac{q \text{ tot } L^4}{E \times I} \\
 &= \frac{1 \times 3,9384 \times 60^4}{145 \times 80000 \times 72} = \frac{51041664}{83520000} \\
 &= 0,06111 \text{ cm}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 443,07 / 24 &< 75 \text{ kg/cm}^2 \\
 18,4613 &< 75 \text{ kg/cm}^2 \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

B. Tegangan Geser

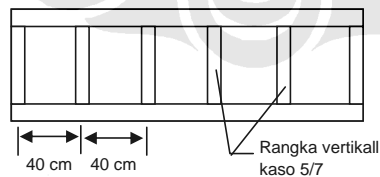
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 59,076 / 24 &< 8 \text{ kg/cm}^2 \\
 3,69225 &< 8 \text{ kg/cm}^2 \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

C. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 0,06111 &< 0,200 \text{ cm} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

4. Kesimpulan

Jadi rangka pipi vertikal kaso 5/7 kelas III dengan jarak pasangan 40 cm **AMAN !!!**



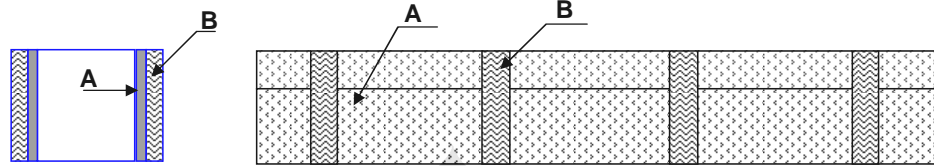
DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING SLOOF

Metode Sloof cara tradisional

A. Data Dimensi Balok

a. Tinggi Balok	:	0,2	m
b. Lebar balok	:	0,1	m
c. Panjang bentang balok	:	1	m
d. Tinggi lantai ke lantai	:	3	m

B. Data Rencana Material



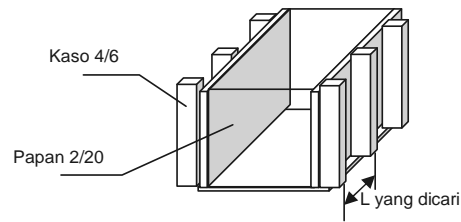
Potongan Penampang Bekisting Sloof

Tampak Samping Bekisting Sloof

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas Kuat Kayu
a.	Bekisting kontak pipi	Papan 2/20	III
b.	Rangka pipi Vertikal	Kaso 4/6	III

DESAIN SIDE BEAM
Tinjauan papan 2/20



1. Data teknis

A. Mutu plywood :

- Kelas Kuat		=	III		
- Tegangan lentur ijin	$\bar{\sigma}$ lt	=	75 kg/cm ²		
- Tegangan geser ijin	$\bar{\tau}$	=	8 kg/cm ²		
- Berat jenis maksimum	γ max	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum	γ min	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	=	cm
- Momen Inersia	I	=	1/12 b h ³	=	16,667 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	=	16,667 cm ³
- Modulus elastisitas	E	=	80000 kg/cm ²		

B. Dimensi Tinjauan :

- Tebal Plywood	h	=	2 cm	=	0,02 m
- Lebar tinjauan	b	=	25 cm	=	0,25 m

C. Spec. Beton

- Berat jenis beton basah	γ bt	=	2500 kg/m ³		
- Tinggi Sloof	H	=	20 cm	=	0,2 m
- Lebar Sloof	B	=	10 cm	=	0,1 m

D. Asumsi Beban Kerja

- Komposisi beban kerja		=	150 kg/m ²
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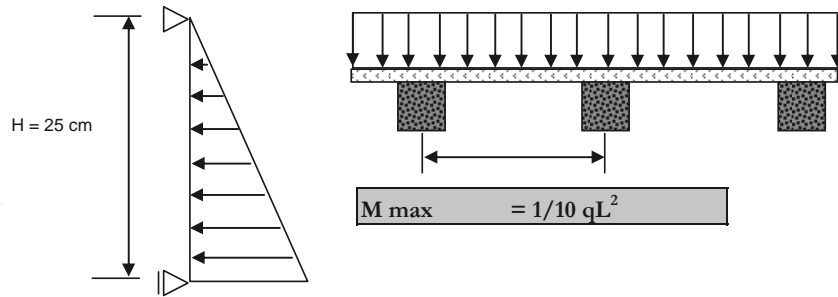
E. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat		=	5/6
		=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap		=	5/4
		=	1,25

F. Beban yang bekerja

- Beban beton	q beton	=	(2500 x 0,2 x 0,1)	=	50 kg/m
- Beban kerja	q kerja	=	(150 x 0,2)	=	30 kg/m
- Beban Plywood	q plywood	=	(600 x 0,02 x 0,25)	=	3 kg/m
	q total	=		=	83 kg/m
		=		=	0,83 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned} M_{\max}/W &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \\ \frac{1}{10} qL^2 &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \times W \\ \frac{1}{10} \times 0,83 \times L^2 &< 1302,109375 \text{ kg/cm}^2 \\ L^2 &< 1302,109375 / (1/10 \times 0,83) \\ L^2 &< 15688,06 \text{ cm}^2 \\ L &< 125,252 \text{ cm} \end{aligned}$$

B. Lendutan

$$\begin{aligned} \frac{1 q_{\text{tot}} L^4}{145 \times E \times I} &< \frac{L}{300} \text{ cm} \\ \frac{1 \times 0,83 \times L^3}{145 \times 80000 \times 16,667} &< \frac{1}{300} \text{ cm} \\ L^3 &< \frac{193337200}{249} \text{ cm}^4 \\ L &< 91,912 \text{ cm} \end{aligned}$$

jarak maksimal = 92 cm

4. Kesimpulan

Digunakan Rangka Vertikal Kaso 4/6 dengan jarak kurang dari 92 cm

Pada perencanaan lapangan akan dipakai rangka vertikal kaso 4/6 dengan jarak 80 cm

DESAIN SIDE BEAM

Tinjauan rangka kaso vertikal 4/6 cm

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Tebal Papan	=	2 cm	=	0,02 m

B. Mutu balok 5/7 :

- Kelas Kuat	=	III	=	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	75 kg/cm ²	=	
- Tegangan geser ijin $\bar{\tau}$	=	8 kg/cm ²	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum δ	=	L / 300	=	cm
- Momen Inersia I	=	1/12 b h ³	=	72,000 cm ⁴
- Momen Lawan W	=	1/6 b h ²	=	24,000 cm ³
- Modulus elastisitas E	=	80000 kg/cm ²	=	

C. Dimensi Tinjauan :

- Tinggi kayu h	=	6 cm	=	0,06 m
- Lebar kayu b	=	4 cm	=	0,04 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	=	
- Tinggi balok H	=	20 cm	=	0,2 m
- Lebar Balok d	=	15 cm	=	0,15 m
- Jarak rangka vertikal L	=	80 cm	=	0,8 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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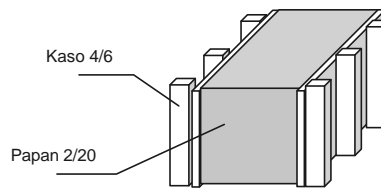
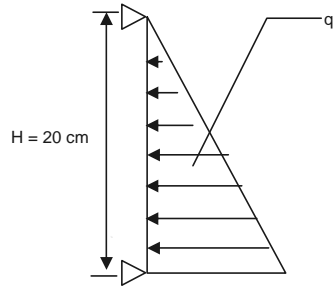
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1,25

G. Beban yang bekerja

- Beban beton q beton	=	0,5 x (2500 x 0,2 x 0,15)	=	37,5 kg/m
- Beban kerja q kerja	=	0,5 x (150 x 0,15)	=	11,25 kg/m
- Beban plywood q plywood	=	0,5 x (600 x 0,2 x 0,02)	=	1,2 kg/m
- Beban sendiri 5/7 q 5/7	=	0,5 x (600 x 0,06 x 0,04)	=	0,72 kg/m
		q total	=	50,67 kg/m
			=	0,507 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 50,67 \times (0,8)^2 \\
 &= 4,054 \text{ kg.m} = 405,36 \text{ kg.cm}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 50,67 \times 0,8 \\
 &= 20,268 \text{ kg}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 0,5067 \times 15^4}{384 \times 80000 \times 72} = \frac{128258,4375}{2211840000} \\
 &= 0,00006 \text{ cm}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 405,36 / 24 &< 75 \text{ kg/cm}^2 \\
 16,8900 &< 75 \text{ kg/cm}^2 \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

B. Tegangan Geser

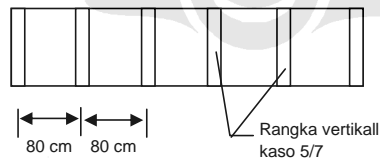
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 20,268 / 24 &< 8 \text{ kg/cm}^2 \\
 1,26675 &< 8 \text{ kg/cm}^2 \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

C. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 0,00006 &< 0,050 \text{ cm} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

4. Kesimpulan

Jadi rangka pipi vertikal kaso 5/7 kelas III dengan jarak pasangan 80 cm **AMAN !!!**

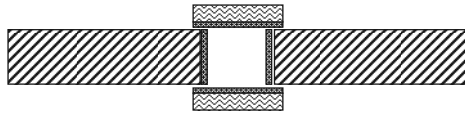


PERHITUNGAN PENGECEKAN KOMPOSISI BEKISTING KOLOM

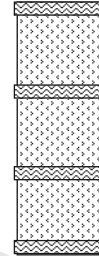
Bekisting cara tradisional untuk kolom

1. Data Umum

Tinggi Kolom	=	300	cm
Lebar Kolom	=	10	cm
Panjang Kolom	=	20	cm
Berat Jenis Beton Basah	=	2500	kg/m ³
Beban Kerja	=	150	kg/m ²
Beban Bekisting	=	43	kg/m ²



Potongan Rencana Penampang Bekisting Kolom



Gambar Bekisting Kolom Pada Sisi Kolom

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas kayu
A	Bekisting kontak	Papan 2/20	III
B	Balok tiang	Balok 4/6	III
C	Balok perangkai	Balok 4/6	III

2. Tinjauan Bekisting Kontak

a. Data Properti Material

Jenis Material	Kelas Kuat	Properti Material			Dimensi Tinjauan		Properti Penampang	
		Teg. Lentur Ijin	Berat Jenis	Modulus E	Lebar	Tebal	Momen Inersia	Momen Lawan
		$\overline{\sigma_{lt}}$ (kg/cm ²)	γ (kg/cm ³)	E (kg/cm ²)	L (cm)	t (cm)	I (cm ⁴)	W (cm ³)
Papan 2/20	III	75	600	80000	20	2	13,33333333	13,33333333

b. Data Teknis Pendukung

a. Spesi beton		
- Berat jenis beton	=	2500 kg/m ³
- Tebal beton	=	0,1 m
b. Faktor koreksi material		
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1,250

- c. Beban kerja dan Beban bekisting
- Beban kerja = 150 kg/m²
 - Beban bekisting = 45 kg/m²
 - Faktor pengali beban = 1/0,7 = 1,429

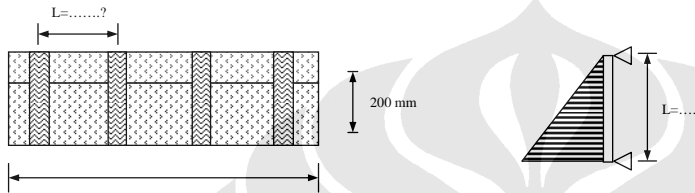
c. Data Pembebanan

- Beban Beton = (0,5*2500*0,1*3) = 375 kg/m
 - Beban Kerja = (0,5*150*3) = 225 kg/m
 - Beban Bekisting = (0,5*45*3*1/0,7) = 96,4287143 kg/m
-
- Pembebanan Total **q total** = 696,429 kg/m = 6,964 kg/cm

d. Rumus-rumus Pendukung

- a. Momen maksimum $M_{max} = 1/8 \cdot q \cdot L^2$
- b. Lendutan $f_{max} = \frac{5 \cdot q \cdot L^4}{384 \cdot E \cdot I}$

3. Menentukan jarak balok perangkai



a. Data Properti Material

Jenis Material	Kelas Kuat	Properti Material			Dimensi Tinjauan		Properti Penampang	
		Teg. Lentur Ijin σ_{II} (kg/cm ²)	Berat Jenis γ (kg/cm ³)	Modulus E E (kg/cm ²)	Lebar L (cm)	Tinggi t (cm)	Momen Inersia I (cm ⁴)	Momen Lawan W (cm ³)
Balok 4/6	III	75	600	80000	20	2	13,33333333	13,33333333

b. Data Teknis Pendukung

- a. Spesi beton
- Berat jenis beton = 2500 kg/m³
 - Tebal beton = 0,1 m
- b. Faktor koreksi material
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat = 5/6
 - = 0,833
 - Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap = 5/4
 - = 1,250

- c. Beban kerja dan Beban bekisting
- Beban kerja = 150 kg/m²
 - Beban bekisting = 45 kg/m²
 - Faktor pengali beban = 1/0,7 = 1,429

c. Data Pembebanan

- Beban yang terjadi = 696,429 kg/m²
- = 0,070 kg/cm²
- Lebar kolom = 20 cm

Sehingga muatan yang terjadi pada balok perangkai = 1,393 kg/cm

e. Menentukan Jarak Balok tiang

Dari segi kekuatan

$$\begin{aligned}
 M_{max}/W_x &< \frac{\bar{\sigma}_t}{\sigma_{lt} \times W_x} \times \text{faktor koreksi} \\
 M_{max} &< 1041,666667 \text{ kg.cm} \\
 1/10q.L^2 &< 7478,63 \\
 L^2 &< 86,5 \\
 L &< 86,5 \text{ cm}
 \end{aligned}$$

Lendutan Yang Terjadi

$$\begin{aligned}
 1/145.(q.L^4)/EI &< L/300 \\
 L^3 &< (145 \cdot EI)/300.q \\
 L^3 &< 370142,45 \text{ cm}^3 \\
 L &< 71,80 \text{ cm}
 \end{aligned}$$

f. Menentukan Jarak Balok tiang

Jarak balok tiang yang diperkenankan kurang dari **71,8** cm

Di lapangan digunakan jarak = **60** cm

g. Pengecekan terhadap jarak yang diambil

Dari lendutan yang terjadi

$$\begin{aligned}
 \text{Lendutan Ijin} &= 0,200 \text{ cm} \\
 \text{Lendutan yang terjadi} &= 0,11671 \text{ cm}
 \end{aligned}$$

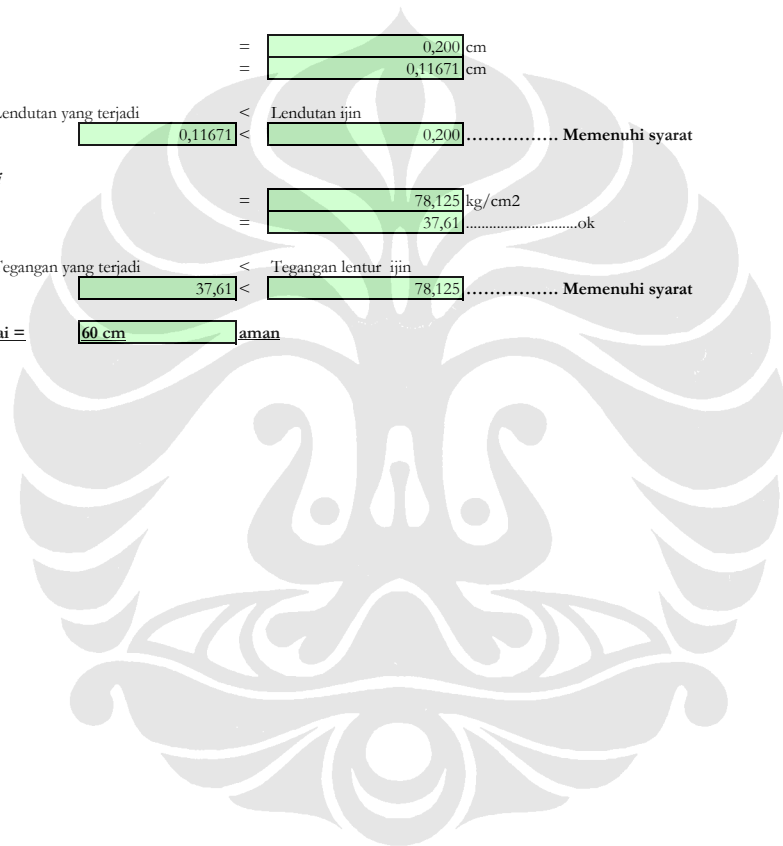
$$\text{Lendutan yang terjadi } 0,11671 < \text{Lendutan ijin } 0,200 \dots \text{Memenuhi syarat}$$

Dari tegangan yang terjadi

$$\begin{aligned}
 \text{Tegangan Ijin} &= 78,125 \text{ kg/cm}^2 \\
 \text{Tegangan yang terjadi} &= 37,61 \dots \text{ok}
 \end{aligned}$$

$$\text{Tegangan yang terjadi } 37,61 < \text{Tegangan lentur ijin } 78,125 \dots \text{Memenuhi syarat}$$

Maka jarak balok perangkai = **60** cm aman



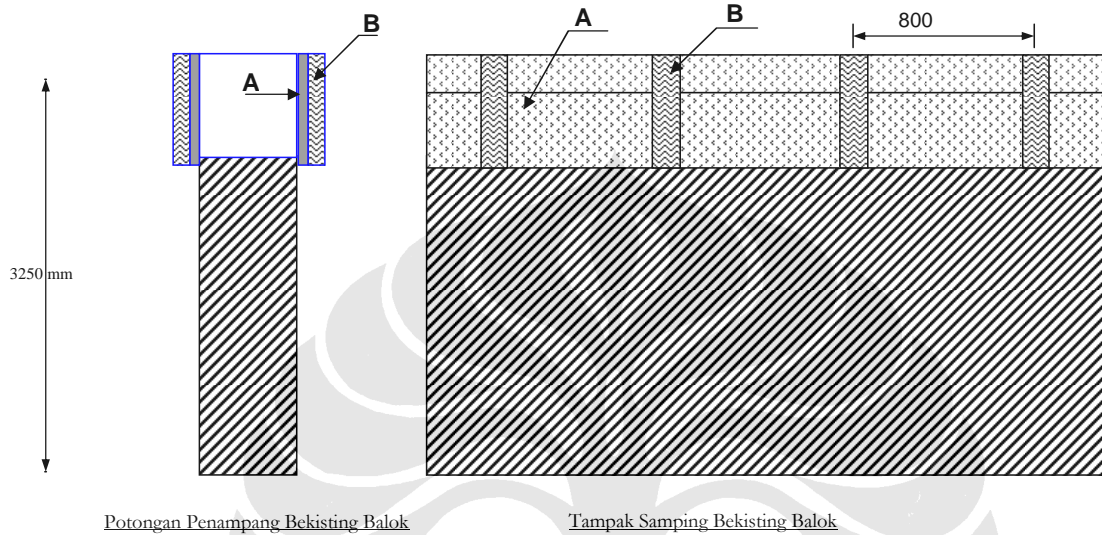
DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING BALOK

Metode Balok cara tradisional

A. Data Dimensi Balok

a. Tinggi Balok	:	0,25	m
b. Lebar balok	:	0,1	m
c. Panjang bentang balok	:	1	m
d. Tinggi lantai ke lantai	:	3	m

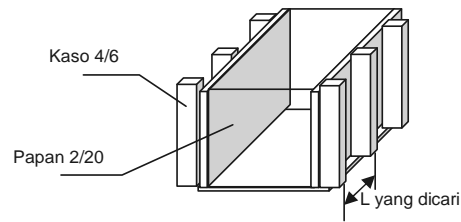
B. Data Rencana Material



Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas Kuat Kayu
a.	Bekisting kontak pipi	Papan 2/20	III
b.	Rangka pipi Vertikal	Kaso 4/6	III

DESAIN SIDE BEAM
Tinjauan papan 2/20



1. Data teknis

A. Mutu plywood :

- Kelas Kuat		=	III		
- Tegangan lentur ijin	$\bar{\sigma}$ lt	=	75 kg/cm ²		
- Tegangan geser ijin	$\bar{\tau}$	=	8 kg/cm ²		
- Berat jenis maksimum	γ max	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum	γ min	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	=	cm
- Momen Inersia	I	=	1/12 b h ³	=	16,667 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	=	16,667 cm ³
- Modulus elastisitas	E	=	80000 kg/cm ²		

B. Dimensi Tinjauan :

- Tebal Plywood	h	=	2 cm	=	0,02 m
- Lebar tinjauan	b	=	25 cm	=	0,25 m

C. Spec. Beton

- Berat jenis beton basah	γ bt	=	2500 kg/m ³		
- Tinggi balok	H	=	25 cm	=	0,25 m
- Lebar balok	B	=	10 cm	=	0,1 m

D. Asumsi Beban Kerja

- Komposisi beban kerja		=	150 kg/m ²		
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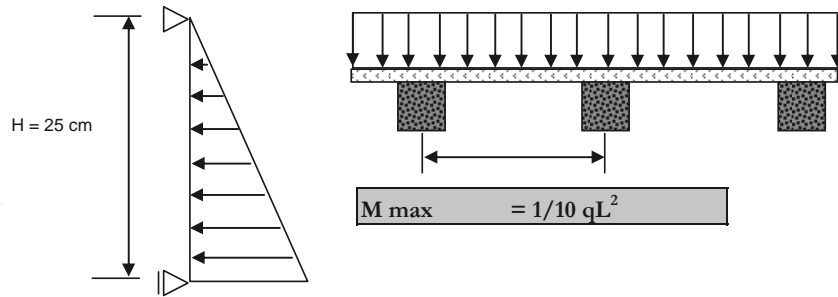
E. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat		=	5/6		
		=	0,833		
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap		=	5/4		
		=	1,25		

F. Beban yang bekerja

- Beban beton	q beton	=	(2500 x 0,25 x 0,1)	=	62,5 kg/m
- Beban kerja	q kerja	=	(150 x 0,25)	=	37,5 kg/m
- Beban Plywood	q plywood	=	(600 x 0,02 x 0,25)	=	3 kg/m
	q total	=		=	103 kg/m
		=		=	1,03 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned}
 M_{\max}/W &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \\
 \frac{1}{10} qL^2 &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \times W \\
 \frac{1}{10} \times 1,03 \times L^2 &< 1302,109375 \text{ kg/cm}^2 \\
 L^2 &< 1302,109375 / (\frac{1}{10} \times 1,03) \\
 L^2 &< 12641,84 \text{ cm}^2 \\
 L &< \mathbf{112,436 \text{ cm}}
 \end{aligned}$$

B. Lendutan

$$\begin{aligned}
 \frac{1 q_{\text{tot}} L^4}{145 \times E \times I} &< \frac{L}{300} \text{ cm} \\
 \frac{1 \times 1,03 \times L^3}{145 \times 80000 \times 16,667} &< \frac{1}{300} \text{ cm} \\
 L^3 &< \frac{193337200}{309} \text{ cm}^4 \\
 L &< \mathbf{85,530 \text{ cm}}
 \end{aligned}$$

jarak maksimal = **86 cm**

4. Kesimpulan

Digunakan Rangka Vertikal Kaso 4/6 dengan jarak kurang dari **86 cm**

Pada perencanaan lapangan akan dipakai rangka vertikal kaso 4/6 dengan jarak 80 cm

D.DESAIN SIDE BEAM

Tinjauan rangka kaso vertikal 4/6 cm

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Tebal Papan	=	2 cm	=	0,02 m

B. Mutu balok 5/7 :

- Kelas Kuat	=	III	=	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	75 kg/cm ²	=	
- Tegangan geser ijin $\bar{\tau}$	=	8 kg/cm ²	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum δ	=	L / 300	=	cm
- Momen Inersia I	=	1/12 b h ³	=	72,000 cm ⁴
- Momen Lawan W	=	1/6 b h ²	=	24,000 cm ³
- Modulus elastisitas E	=	80000 kg/cm ²	=	

C. Dimensi Tinjauan :

- Tinggi kayu h	=	6 cm	=	0,06 m
- Lebar kayu b	=	4 cm	=	0,04 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	=	
- Tinggi balok H	=	25 cm	=	0,25 m
- Lebar Balok d	=	15 cm	=	0,15 m
- Jarak rangka vertikal L	=	80 cm	=	0,8 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²	=	
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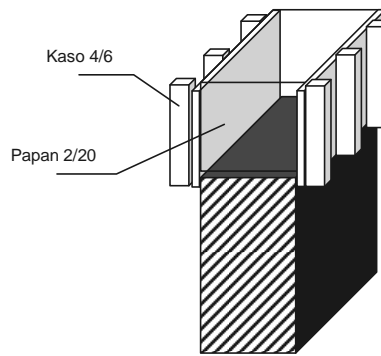
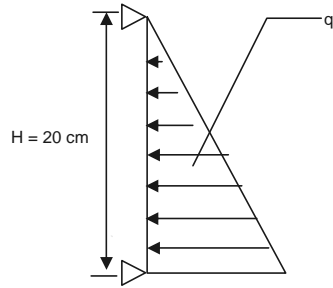
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6	=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4	=	1,25

G. Beban yang bekerja

- Beban beton q beton	=	0,5 x (2500 x 0,25 x 0,15)	=	46,875 kg/m
- Beban kerja q kerja	=	0,5 x (150 x 0,15)	=	11,25 kg/m
- Beban plywood q plywood	=	0,5 x (600 x 0,25 x 0,02)	=	1,5 kg/m
- Beban sendiri 5/7 q 5/7	=	0,5 x (600 x 0,06 x 0,04)	=	0,72 kg/m
q total			=	60,345 kg/m
			=	0,603 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 60,345 \times (0,8)^2 \\
 &= 4,828 \text{ kg.m} = 482,76 \text{ kg.cm}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 60,345 \times 0,8 \\
 &= 24,138 \text{ kg}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 0,60345 \times 15^4}{384 \times 80000 \times 72} = \frac{152748,2813}{2211840000} \\
 &= 0,00007 \text{ cm}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 482,76 / 24 &< 75 \text{ kg/cm}^2 \\
 20,1150 &< 75 \text{ kg/cm}^2 \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

B. Tegangan Geser

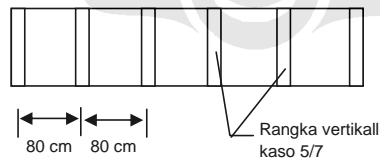
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 24,138 / 24 &< 8 \text{ kg/cm}^2 \\
 1,508625 &< 8 \text{ kg/cm}^2 \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

C. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 0,00007 &< 0,050 \text{ cm} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

4. Kesimpulan

Jadi rangka pipi vertikal kaso 5/7 kelas III dengan jarak pasangan 40 cm **AMAN !!!**

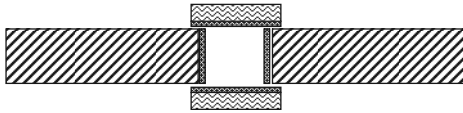


PERHITUNGAN PENGECEKAN KOMPOSISI BEKISTING KOLOM

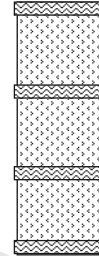
Bekisting cara tradisional untuk kolom

1. Data Umum

Tinggi Kolom	=	300	cm
Lebar Kolom	=	10	cm
Panjang Kolom	=	35	cm
Berat Jenis Beton Basah	=	2500	kg/m ³
Beban Kerja	=	150	kg/m ²
Beban Bekisting	=	43	kg/m ²



Potongan Rencana Penampang Bekisting Kolom



Gambar Bekisting Kolom Pada Sisi Kolom

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas kayu
A	Bekisting kontak	Papan 2/20	III
B	Balok tiang	Balok 4/6	III
C	Balok perangkai	Balok 4/6	III

2. Tinjauan Bekisting Kontak

a. Data Properti Material

Jenis Material	Kelas Kuat	Properti Material			Dimensi Tinjauan		Properti Penampang	
		Teg. Lentur Ijin $\overline{\sigma_{II}}$ (kg/cm ²)	Berat Jenis γ (kg/cm ³)	Modulus E E (kg/cm ²)	Lebar L (cm)	Tebal t (cm)	Momen Inersia I (cm ⁴)	Momen Lawan W (cm ³)
Papan 2/20	III	75	600	80000	35	2	23,33333333	23,33333333

b. Data Teknis Pendukung

a. Spesi beton		
- Berat jenis beton	=	2500 kg/m ³
- Tebal beton	=	0,1 m
b. Faktor koreksi material		
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1,250

- c. Beban kerja dan Beban bekisting
- Beban kerja = 150 kg/m²
 - Beban bekisting = 45 kg/m²
 - Faktor pengali beban = $1/0,7 = 1,429$

c. Data Pembebanan

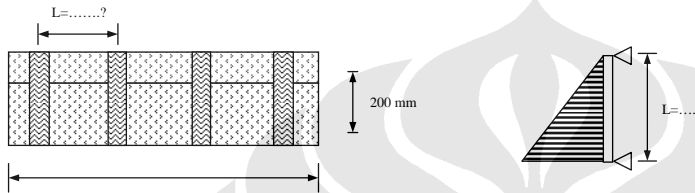
- Beban Beton = $(0,5 \times 2500 \times 0,1 \times 3) = 375$ kg/m
- Beban Kerja = $(0,5 \times 150 \times 3) = 225$ kg/m
- Beban Bekisting = $(0,5 \times 45 \times 3 \times 1/0,7) = 96,4287143$ kg/m

- Pembebanan Total q total = $696,429$ kg/m
- = $6,964$ kg/cm

d. Rumus-rumus Pendukung

- a. Momen maksimum $M_{max} = 1/8 \cdot q \cdot L^2$
- b. Lendutan $f_{max} = \frac{5 \cdot q \cdot L^4}{384 \cdot E \cdot I}$

3. Menentukan jarak balok perangkai



a. Data Properti Material

Jenis Material	Kelas Kuat	Properti Material			Dimensi Tinjauan		Properti Penampang	
		Teg. Lentur Ijin σ_{II} (kg/cm ²)	Berat Jenis γ (kg/cm ³)	Modulus E E (kg/cm ²)	Lebar L (cm)	Tinggi t (cm)	Momen Inersia I (cm ⁴)	Momen Lawan W (cm ³)
Balok 4/6	III	75	600	80000	35	2	23,33333333	23,33333333

b. Data Teknis Pendukung

- a. Spesi beton
- Berat jenis beton = 2500 kg/m³
 - Tebal beton = 0,1 m
- b. Faktor koreksi material
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat = 5/6
 - = 0,833
 - Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap = 5/4
 - = 1,250
- c. Beban kerja dan Beban bekisting
- Beban kerja = 150 kg/m²
 - Beban bekisting = 45 kg/m²
 - Faktor pengali beban = $1/0,7 = 1,429$

c. Data Pembebanan

- Beban yang terjadi = 696,429 kg/m²
 = 0,070 kg/cm²
 - Lebar kolom = 20 cm

Sehingga muatan yang terjadi pada balok perangkai
 = 1,393 kg/cm

e. Menentukan Jarak Balok tiang

Dari segi kekuatan

$M_{max}/W_x < \frac{\sigma_{lt}}{\sigma_{lt} \times W_x}$ x faktor koreksi
 $M_{max} < \frac{\sigma_{lt}}{\sigma_{lt} \times W_x}$
 $1/10q.L^2 < 1822,916667$ kg.cm
 $L^2 < 13087,61$
 $L < 114,4$ cm

Lendutan Yang Terjadi

$1/145.(q.L^4)/EI < L/300$
 $L^3 < (145 \cdot EI)/300.q$
 $L^3 < 647749,29$ cm³
 $L < 86,52$ cm

f. Menentukan Jarak Balok tiang

Jarak balok tiang yang diperkenankan kurang dari 86,5 cm

Di lapangan digunakan jarak = 70 cm

g. Pengecekan terhadap jarak yang diambil

Dari lendutan yang terjadi

Lendutan Ijin = 0,233 cm
 Lendutan yang terjadi = 0,12356 cm

Lendutan yang terjadi < Lendutan ijin
 0,12356 < 0,233 Memenuhi syarat

Dari tegangan yang terjadi

Tegangan Ijin = 78,125 kg/cm²
 Tegangan yang terjadi = 29,25ok

Tegangan yang terjadi < Tegangan lentur ijin
 29,25 < 78,125 Memenuhi syarat

Maka jarak balok perangkai = 70 cm aman

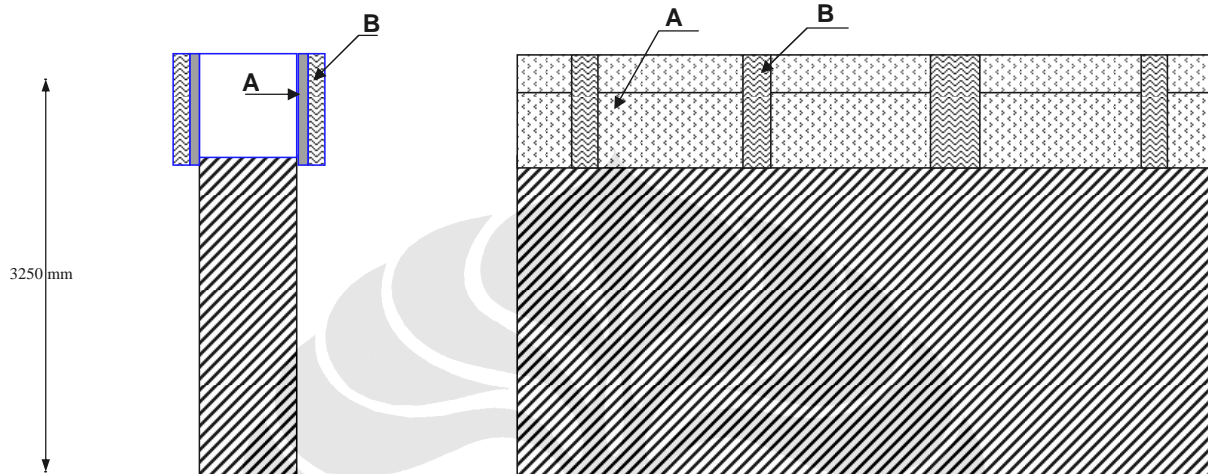
DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING RING BALOK

Metode Ring Balok cara tradisional

A. Data Dimensi Balok

a. Tinggi Balok	:	0,1	m
b. Lebar balok	:	0,1	m
c. Panjang bentang balok	:	1	m
d. Tinggi lantai ke lantai	:	3	m

B. Data Rencana Material



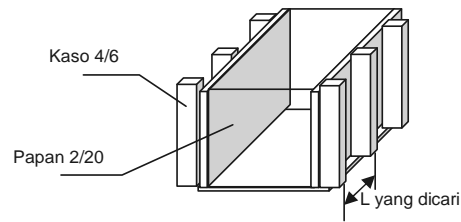
Potongan Penampang Bekisting Balok

Tampak Samping Bekisting Balok

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas Kuat Kayu
a.	Bekisting kontak pipi	Papan 2/20	III
b.	Rangka pipi Vertikal	Kaso 4/6	III

DESAIN SIDE BEAM
Tinjauan papan 2/20



1. Data teknis

A. Mutu plywood :

- Kelas Kuat		=	III		
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	75 kg/cm ²		
- Tegangan geser ijin	$\bar{\tau}$	=	8 kg/cm ²		
- Berat jenis maksimum	γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum	γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	=	cm
- Momen Inersia	I	=	1/12 b h ³	=	16,667 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	=	16,667 cm ³
- Modulus elastisitas	E	=	80000 kg/cm ²		

B. Dimensi Tinjauan :

- Tebal Plywood	h	=	2 cm	=	0,02 m
- Lebar tinjauan	b	=	25 cm	=	0,25 m

C. Spec. Beton

- Berat jenis beton basah	γ_{bt}	=	2500 kg/m ³		
- Tinggi balok	H	=	10 cm	=	0,1 m
- Lebar balok	B	=	10 cm	=	0,1 m

D. Asumsi Beban Kerja

- Komposisi beban kerja		=	150 kg/m ²		
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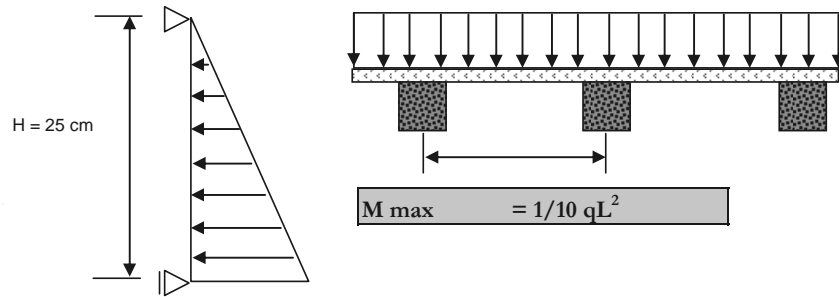
E. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat		=	5/6		
		=	0,833		
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap		=	5/4		
		=	1,25		

F. Beban yang bekerja

- Beban beton	q beton	=	(2500 x 0,1 x 0,1)	=	25 kg/m
- Beban kerja	q kerja	=	(150 x 0,1)	=	15 kg/m
- Beban Plywood	q plywood	=	(600 x 0,02 x 0,25)	=	3 kg/m
	q total	=		=	43 kg/m
		=		=	0,43 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned} M_{\max}/W &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \\ \frac{1}{10} qL^2 &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \times W \\ \frac{1}{10} \times 0,43 \times L^2 &< 1302,109375 \text{ kg/cm}^2 \\ L^2 &< 1302,109375 / (1/10 \times 0,43) \\ L^2 &< 30281,61 \text{ cm}^2 \\ L &< \mathbf{174,016 \text{ cm}} \end{aligned}$$

B. Lendutan

$$\begin{aligned} \frac{1 \times q_{\text{tot}} L^4}{145 \times E \times I} &< \frac{L}{300} \text{ cm} \\ \frac{1 \times 0,43 \times L^3}{145 \times 80000 \times 16,667} &< \frac{1}{300} \text{ cm} \\ L^3 &< \frac{193337200}{129} \text{ cm}^4 \\ L &< \mathbf{114,439 \text{ cm}} \end{aligned}$$

jarak maksimal = **114 cm**

4. Kesimpulan

Digunakan Rangka Vertikal Kaso 4/6 dengan jarak kurang dari **114 cm**

Pada perencanaan lapangan akan dipakai rangka vertikal kaso 4/6 dengan jarak 100 cm

DESAIN SIDE BEAM

Tinjauan rangka kaso vertikal 4/6 cm

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Tebal Papan	=	2 cm	=	0,02 m

B. Mutu balok 5/7 :

- Kelas Kuat	=	III	=	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	75 kg/cm ²	=	
- Tegangan geser ijin $\bar{\tau}$	=	8 kg/cm ²	=	
- Berat jenis maksimum γ_{max}	=	0,6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0,4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum δ	=	L / 300	=	cm
- Momen Inersia I	=	1/12 b h ³	=	72,000 cm ⁴
- Momen Lawan W	=	1/6 b h ²	=	24,000 cm ³
- Modulus elastisitas E	=	80000 kg/cm ²	=	

C. Dimensi Tinjauan :

- Tinggi kayu h	=	6 cm	=	0,06 m
- Lebar kayu b	=	4 cm	=	0,04 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	=	
- Tinggi balok H	=	10 cm	=	0,1 m
- Lebar Balok d	=	15 cm	=	0,15 m
- Jarak rangka vertikal L	=	100 cm	=	1 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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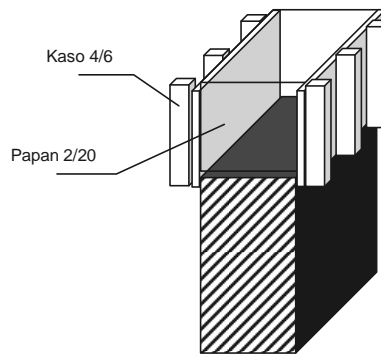
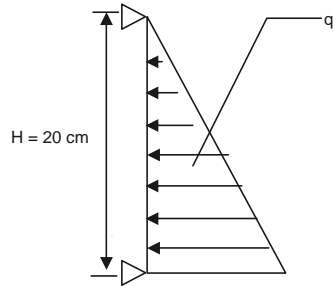
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0,833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1,25

G. Beban yang bekerja

- Beban beton q beton	=	0,5 x (2500 x 0,1 x 0,15)	=	18,75 kg/m
- Beban kerja q kerja	=	0,5 x (150 x 0,15)	=	11,25 kg/m
- Beban plywood q plywood	=	0,5 x (600 x 0,1 x 0,02)	=	0,6 kg/m
- Beban sendiri 5/7 q 5/7	=	0,5 x (600 x 0,06 x 0,04)	=	0,72 kg/m
		q total	=	31,32 kg/m
			=	0,313 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 31,32 \times (1)^2 \\
 &= \mathbf{3,915 \text{ kg.m}} = \mathbf{391,5 \text{ kg.cm}}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 31,32 \times 1 \\
 &= \mathbf{15,66 \text{ kg}}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 0,3132 \times 15^4}{384 \times 80000 \times 72} = \frac{79278,75}{2211840000} \\
 &= \mathbf{0,00004 \text{ cm}}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

A. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 391,5 / 24 &< 75 \text{ kg/cm}^2 \\
 \mathbf{16,3125} &< \mathbf{75 \text{ kg/cm}^2} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

B. Tegangan Geser

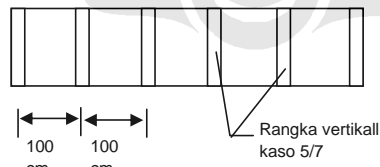
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 15,66 / 24 &< 8 \text{ kg/cm}^2 \\
 \mathbf{0,97875} &< \mathbf{8 \text{ kg/cm}^2} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

C. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 \mathbf{0,00004} &< \mathbf{0,050 \text{ cm}} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

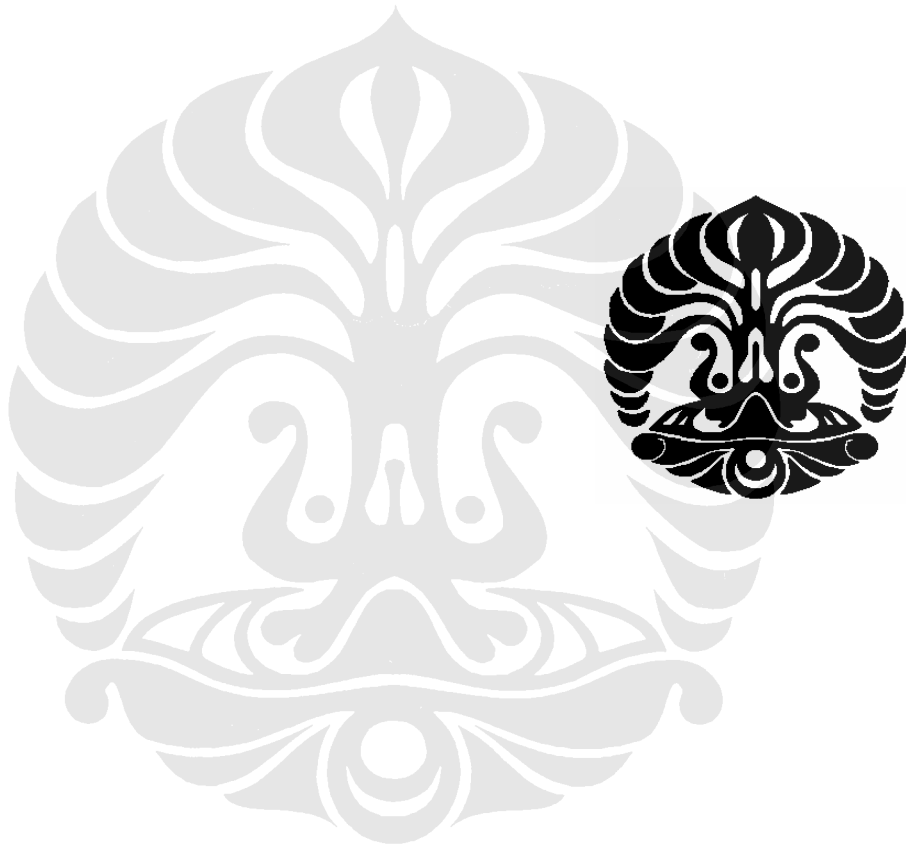
4. Kesimpulan

Jadi rangka pipi vertikal kaso 5/7 kelas III dengan jarak pasangan 100 cm **AMAN !!!**



LAMPIRAN C2

Perhitungan Statika Bekisting Baja (Pondasi, Sloof, Kolom, Balok dan Ring Balok)



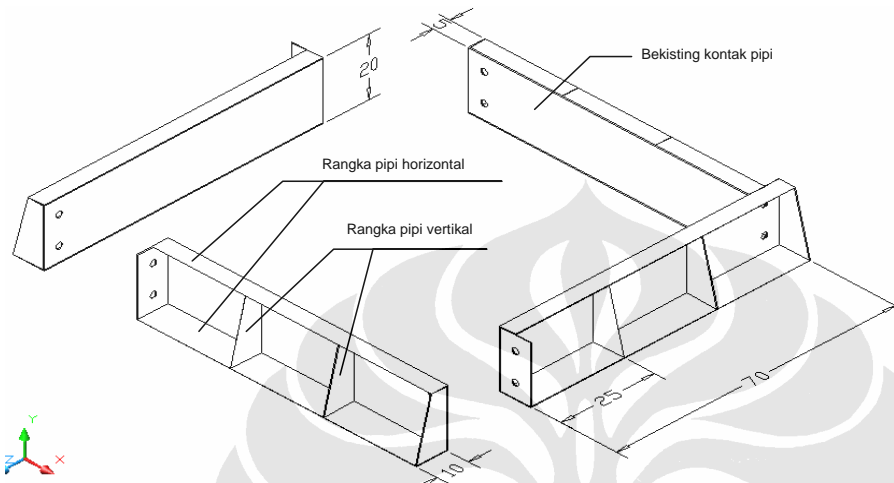
DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING PONDASI

Bekisting Baja untuk Pondasi

A. Data Dimensi Pondasi

- a. Tinggi Pondasi : 0.2 m
b. Lebar Pondasi : 0.6 m
c. Panjang Pondasi : 0.6 m

B. Data Rencana Material



Keterangan Gambar :

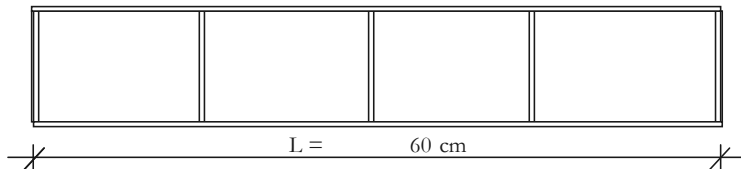
- A : Bekisting kontak pipi
B : Rangka pipi horisontal
C : Rangka pipi vertikal

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Type
a.	Bekisting kontak pipi	Plat Baja	BJ 37
b.	Rangka pipi Vertikal	Plat Baja	BJ 37
c.	Rangka pipi horisontal	Plat Baja	BJ 37

C. DESAIN SIDE BEAM

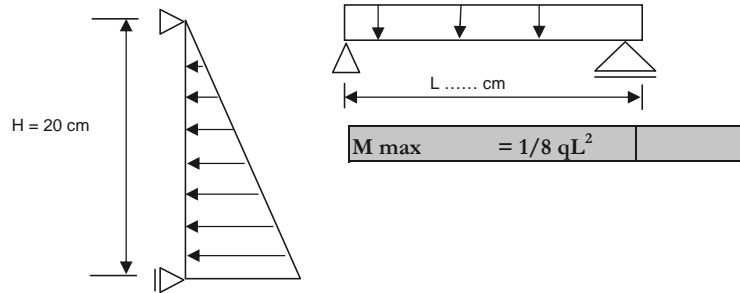
Tinjauan Plat Baja



1. Data teknis

A. Mutu baja :		BJ37			
- Tegangan Leleh	f_y	=	2400	kg/cm ²	
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	1440	kg/cm ²	0.6 x f_y
- Tegangan geser ijin	$\bar{\tau}$	=	960	kg/cm ²	0.4 x f_y
- Berat jenis maksimum	γ_{max}	=	7.85	gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	cm	= 0.2 cm
- Momen Inersia	I	=	1/12 b h ³	cm ⁴	= 0.045 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	cm ³	= 0.3 cm ³
- Modulus elastisitas	E	=	2000000	kg/cm ²	
B. Dimensi Tinjauan :					
- Tebal Baja	h	=	0.3	cm	= 0.003 m
- Lebar tinjauan	b	=	20	cm	= 0.2 m
C. Spec. Beton					
- Berat jenis beton basah	γ_{bt}	=	2500	kg/m ³	
- Tinggi pondasi	H	=	20	cm	= 0.2 m
- Lebar pondasi	B	=	60	cm	= 0.6 m
D. Asumsi Beban Kerja					
- Komposisi beban kerja		=	150	kg/m ²	
E. Beban yang bekerja					
- Beban beton	q beton	=	(2500 x 0,2 x 0,6) / 4	=	75 kg/m
- Beban kerja	q kerja	=	(150 x 0,2)	=	30 kg/m
- Beban Plat kontak pipi	q plat pipi	=	(7850 x 0,003 x 0,2)	=	4.71 kg/m
	q total	=		=	109.71 kg/m
		=		=	1.0971 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M_{\text{max}}/W &< \sigma_{\text{lt ijin}} \\
 \frac{1}{8} qL^2 &< \sigma_{\text{lt ijin}} \times W \\
 \frac{1}{8} \times 1,0971 \times L^2 &< 432 \text{ kg/cm} \\
 L^2 &< \\
 L^2 &< 3150.12 \text{ cm}^2 \\
 L &< 56.126 \text{ cm}
 \end{aligned}$$

b. Lendutan

$$\begin{aligned}
 \frac{5 q \text{ tot } L^4}{384 \times E \times I} &< \frac{L}{300} \text{ cm} \\
 \frac{5 \times 1,0971 \times L^3}{384 \times 2000000 \times 0,045} &< \frac{1}{300} \text{ cm} \\
 L^3 &< \frac{34560000}{1645.65} \text{ cm}^4 \\
 L &< 27.590 \text{ cm}
 \end{aligned}$$

jarak maksimal = 28 cm

4. Kesimpulan

Jadi Baja dengan tebal 3 mm BJ37 dapat digunakan dengan jarak pengaku kaso vertikal kurang dari 28 cm

Pada perencanaan lapangan akan dipakai rangka vertikal dengan jarak 25 cm

DESAIN SIDE BEAM

Tinjauan Plat Baja

1. Data teknis

A. Mutu Baja kontak pipi :

- Type	=	BJ 37	
- Berat jenis maksimum γ max	=	7.85 gr/cm ³	= 7850 kg/m ³
- Tebal baja	=	0.3 cm	= 0.003 m

B. Mutu Baja :

- Type	=	BJ 37	
- Tegangan Leleh f_y	=	2400 kg/cm ²	
- Tegangan lentur ijin $\bar{\sigma}$ lt	=	1440 kg/cm ²	
- Tegangan geser ijin $\bar{\tau}$	=	960 kg/cm ²	
- Berat jenis maksimum γ max	=	7.85 gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum δ	=	L / 300 cm	= 0.0833333 cm
- Momen Inersia I	=	1/12 b h ³ cm ⁴	= 16.667 cm ⁴
- Momen Lawan W	=	1/6 b h ² cm ³	= 3.333 cm ³
- Modulus elastisitas E	=	2000000 kg/cm ²	

D. Dimensi Tinjauan :

- Tinggi baja h	=	10 cm	= 0.1 m
- Lebar baja b	=	0.2 cm	= 0.002 m

D. Spec. Beton

- Berat jenis beton basah γ bt	=	2500 kg/m ³	
- Tinggi pondasi H	=	20 cm	= 0.2 m
- Lebar pondasi d	=	60 cm	= 0.6 m
- Jarak rangka vertikal L	=	25 cm	= 0.25 m

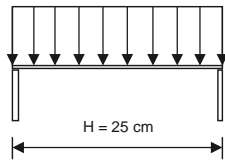
E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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F. Beban yang bekerja

- Beban beton q beton	=	0.5 x (2500 x 0,2 x 0,6)	=	150 kg/m
- Beban kerja q kerja	=	0.5 x (150 x 0,6)	=	45 kg/m
- Beban plat pipi q plat pipi	=	0.5 x (7850 x 0,2 x 0,003)	=	2.355 kg/m
- Beban plat rangka q plat rangka	=	0.5 x (7850 x 0,1 x 0,002)	=	0.785 kg/m
		q total	=	198.14 kg/m
			=	1.981 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 198,14 \times (0,25)^2 \\
 &= \mathbf{1.548 \text{ kg.m}} = \mathbf{154.796875 \text{ kg.cm}}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 198,14 \times 0,25 \\
 &= \mathbf{24.7675 \text{ kg}}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 1,9814 \times 25^4}{384 \times 2000000 \times 16,666666} = \frac{3869921.875}{12800000000} \\
 &= \mathbf{0.000 \text{ cm}}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 154,796875 / 3 &< 1440 \text{ kg/cm}^2 \\
 \mathbf{46.4391} &< \mathbf{1440 \text{ kg/cm}^2} \quad \text{.....ok !!!}
 \end{aligned}$$

b. Tegangan Geser

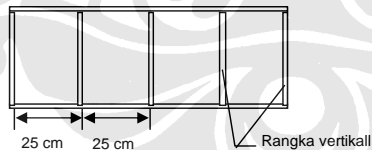
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 24,7675 / 2 &< 960 \text{ kg/cm}^2 \\
 \mathbf{18.575625} &< \mathbf{960 \text{ kg/cm}^2} \quad \text{.....ok !!!}
 \end{aligned}$$

c. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 \mathbf{0.0003} &< \mathbf{0.200 \text{ cm}} \quad \text{.....ok !!!}
 \end{aligned}$$

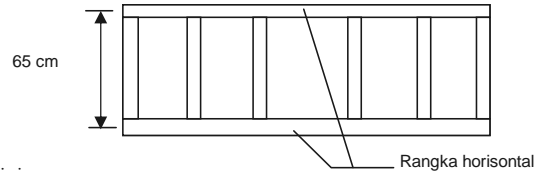
4. Kesimpulan

Jadi rangka pipi vertikal Plat baja BJ37 dengan jarak pemasangan 25 cm **AMAN !!!**



DESAIN SIDE BEAM

Tinjauan Plat Baja



1. Data teknis

A. Mutu Baja kontak pipi :

- Type	=	BJ37	
- Berat jenis maksimum γ_{max}	=	7.85 gr/cm ³	= 7850 kg/m ³
- Tebal baja	=	0.3 cm	= 0.003 m

B. Mutu baja rangka :

- Kelas Kuat	=	BJ 37	
- Tegangan Leleh f_y	=	2400 kg/cm ²	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	1440 kg/cm ²	
- Tegangan geser ijin $\bar{\tau}$	=	960 kg/cm ²	
- Berat jenis maksimum γ_{max}	=	7.85 gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum δ	=	L / 300 cm	= 0.0666667 cm
- Momen Inersia I	=	1/12 b h ³ cm ⁴	= 0.45 cm ⁴
- Momen Lawan W	=	1/6 b h ² cm ³	= 0.3 cm ³
- Modulus elastisitas E	=	2000000 kg/cm ²	

D. Dimensi Tinjauan :

- Tinggi baja h	=	3 cm	= 0.03 m
- Lebar baja b	=	0.2 cm	= 0.002 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	
- Tinggi beton H	=	20 cm	= 0.2 m
- Lebar Beton d	=	50 cm	= 0.5 m
- Jarak rangka vertikal L1	=	25 cm	= 0.25 m
- Jarak rangka horisontal L2	=	20 cm	= 0.2 m

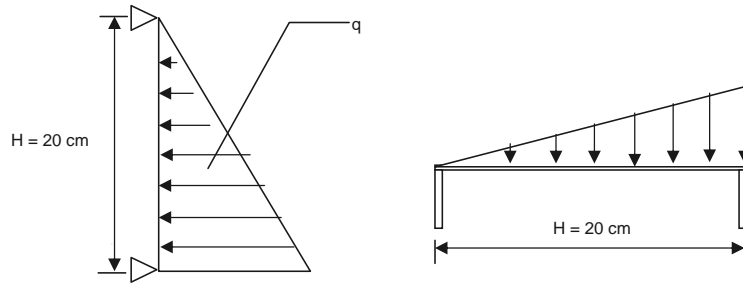
E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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F. Beban yang bekerja

- Beban beton q beton	=	0.5(2500 x 0.2 x 0.5)	=	125 kg/m
- Beban kerja q kerja	=	0.5(150 x 0.5)	=	37.5 kg/m
- Beban plat pipi q plat pipi	=	(7850 x 0.25 x 0.003)	=	5.8875 kg/m
- Beban plat rangka q plat rangka	=	(7850 x 0.03 x 0.002)	=	0.471 kg/m
			q total	= 168.8585 kg/m
				= 1.689 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 168,8585 \times (0,2)^2 \\
 &= \mathbf{0.844 \text{ kg.m}} = \mathbf{84.42925 \text{ kg.cm}}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{3} q \times L \\
 &= \frac{1}{3} \times 168,8585 \times 0,2 \\
 &= \mathbf{11.2572333 \text{ kg}}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 1,688585 \times 20^4}{384 \times 2000000 \times 0,45} = \frac{1350868}{345600000} \\
 &= \mathbf{0.004 \text{ cm}}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 84,42925/0,3 &< 1440 \text{ kg/cm}^2 \\
 \mathbf{281.431} &< \mathbf{1440 \text{ kg/cm}^2} \quad \text{.....ok !!!}
 \end{aligned}$$

b. Tegangan Geser

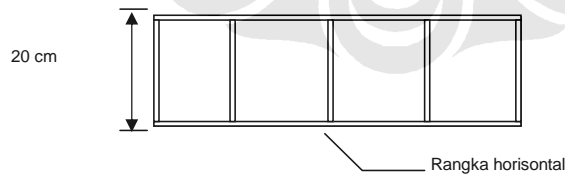
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 11,26 / 0,6 &< 960 \text{ kg/cm}^2 \\
 \mathbf{28.143} &< \mathbf{960 \text{ kg/cm}^2} \quad \text{.....ok !!!}
 \end{aligned}$$

c. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 \mathbf{0.00391} &< \mathbf{0.167 \text{ cm}} \quad \text{.....ok !!!}
 \end{aligned}$$

4. Kesimpulan

Jadi rangka pipi horisontal baja 2 mm BJ37 dengan jarak pasangan 20 cm **AMAN !!!**

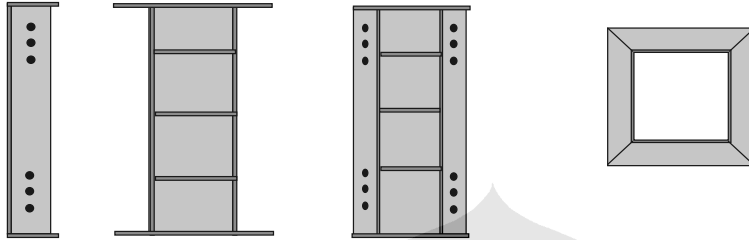


PERHITUNGAN PENGECEKAN KOMPOSISI BEKISTING KOLOM

Bekisting baja untuk kolom

1. DATA UMUM

Tinggi Kolom	=	100	cm
Lebar Kolom	=	20	cm
Panjang Kolom	=	20	cm
Berat Jenis Beton Basah	=	2500	kg/m ³
Beban Kerja	=	150	kg/m ²
Beban Bekisting	=	45	kg/m ²



Potongan Rencana Penampang Bekisting Kolom

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Type
A	Bekisting kontak	Plat Baja	BJ 37 Tebal 0,3
B	Balok tiang	Plat Baja	BJ 37 Tebal 0,2
C	Balok perangkai	Plat Baja	BJ 37 Tebal 0,2

2. Tinjauan Bekisting Kontak

a. Data Properti Material

A. Mutu baja : BJ37

- Tegangan Leleh	f_y	=	2400	kg/cm ²	
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	1440	kg/cm ²	0.6 x f_y
- Tegangan geser ijin	$\bar{\tau}$	=	960	kg/cm ²	0.4 x f_y
- Berat jenis maksimum	γ_{max}	=	7.85	gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	cm	=
- Momen Inersia	I	=	1/12 b h ³	cm ⁴	= 0.225 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	cm ³	= 1.5 cm ³
- Modulus elastisitas	E	=	2000000	kg/cm ²	

B. Dimensi Penampang :

- Tebal Baja	h	=	0.3	cm	= 0.003 m
- Lebar tinjauan	b	=	100	cm	= 1 m

b. Data Teknis Pendukung

a. Spesi beton

- Berat jenis beton	=	2500	kg/m ³
- Tebal beton	=	0.2	m

c. Beban kerja dan Beban bekisting	=		
- Beban kerja	=	150	kg/m ²
- Beban bekisting	=	45	kg/m ²
- Faktor pengali beban	=	1/0,7 =	1.429

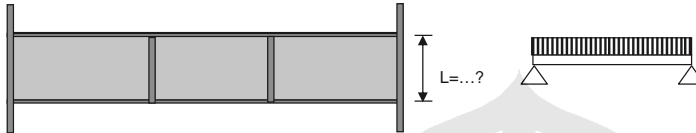
c. Data Pembebanan

- Beban Beton	=	(2500*0,2*1)	=	500	kg/m
- Beban Kerja	=	(150*1)	=	150	kg/m
- Beban Bekisting	=	(45*1*1/0,7)	=	64.286	kg/m
Pembebanan Total	q total		=	714.286	kg/m
			=	7.143	kg/cm

d. Rumus-rumus Pendukung

a. Momen maksimum	$M_{max} =$	$1/8 \cdot q \cdot L^2$
b. Lendutan	$f_{max} =$	$\frac{5 \cdot q \cdot L^4}{384 \cdot E \cdot I}$

e. Menentukan Jarak Balok tiang



Dari segi kekuatan

$$\frac{M_{max}}{W_x} < \frac{\sigma_{lt}}{\sigma_{lt} \cdot W_x} \times \text{faktor koreksi}$$

$$\frac{1/8 \cdot q \cdot L^2}{L^2} < \frac{2160}{2419,20} \text{ kg/cm}$$

$$L < 49,2 \text{ cm}$$

Lendutan Yang Terjadi

$$\frac{(5 \cdot q \cdot L^4)/(384 \cdot E \cdot I)}{L^3} < L/300$$

$$\frac{(384 \cdot E \cdot I)/300 \cdot 5 \cdot q}{L^3} < L/300$$

$$L < 16128,00 \text{ cm}^3$$

$$L < 25,27 \text{ cm}$$

f. Menentukan Jarak Balok tiang

Jarak balok tiang yang diperkenankan kurang dari **25,3 cm**

Di lapangan digunakan jarak = **20 cm**

g. Pengecekan terhadap jarak yang diambil

Dari lendutan yang terjadi

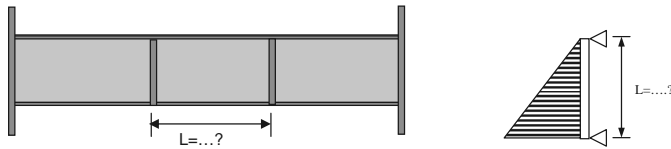
Lendutan Ijin	=	0,067	cm
Lendutan yang terjadi	=	0,03307	cm
Lendutan yang terjadi	<	Lendutan ijin	0,06667ok !!!

Dari tegangan yang terjadi

Tegangan Ijin	=	1440	kg/cm ²
Tegangan yang terjadi	=	190.4761905ok
Tegangan yang terjadi	<	Tegangan lentur ijin	1440ok !!!

Maka jarak balok tiang = **20 cm** aman dipakai

3. Menentukan jarak balok perangkai



a. Data Properti Material

A. Mutu baja :		BJ37			
- Tegangan Leleh	f_y	=	2400	kg/cm ²	
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	1440	kg/cm ²	0.6 x f_y
- Tegangan geser ijin	$\bar{\tau}$	=	960	kg/cm ²	0.4 x f_y
- Berat jenis maksimum	γ_{max}	=	7.85	gr/cm ³	=
- Lendutan Maksimum	δ	=	L / 300	cm	=
- Momen Inersia	I	=	1/12 b h ³	cm ⁴	=
- Momen Lawan	W	=	1/6 b h ²	cm ³	=
- Modulus elastisitas	E	=	2000000	kg/cm ²	=
					7850 kg/m ³
					0.045 cm ⁴
					0.3 cm ³

B. Dimensi Penampang :					
- Tebal Baja	h	=	0.3	cm	=
- Lebar tinjauan	b	=	20	cm	=
					0.003 m
					0.2 m

b. Data Teknis Pendukung

a. Spesi beton					
- Berat jenis beton	=	2500	kg/m ³		
- Tebal beton	=	0.2	m		
b. Faktor koreksi material					
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6			
	=	0.833			
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4			
	=	1.250			
c. Beban kerja dan Beban bekisting					
- Beban kerja	=	150	kg/m ²		
- Beban bekisting	=	45	kg/m ²		
- Faktor pengali beban	=	1/0.7			
	=	1.429			

c. Data Pembebanan

- Beban Beton	=	(2500*0.2*0.2)	=	100	kg/m
- Beban Kerja	=	(150*0.2)	=	30	kg/m
- Beban Bekisting	=	(45*0.2*1/0.7)	=	12.857	kg/m
Pembebanan Total	q total	=	142.857	kg/m	
		=	1.429	kg/cm	

e. Menentukan Jarak Balok tiang

Dari segi kekuatan

$$\frac{M_{max}}{W_x} < \frac{\bar{\sigma}_{lt}}{\sigma_{lt} \times W_x} \times \text{faktor koreksi}$$

$$M_{max} < \frac{\bar{\sigma}_{lt}}{\sigma_{lt}} \times W_x$$

$$\frac{1}{10} q L^2 < 450 \text{ kg.cm}$$

$$L^2 < 3150.00$$

$$L < 56.1 \text{ cm}$$

Lendutan Yang Terjadi

$$\frac{1}{145} \cdot (q L^4) / EI < L / 300$$

$$L^3 < (145 \cdot EI) / 300 \cdot q$$

$$L^3 < 30450.00 \text{ cm}^3$$

$$L < 31.23 \text{ cm}$$

f. Menentukan Jarak Balok tiang

Jarak balok tiang yang diperkenankan kurang dari **31.2** cm

Di lapangan digunakan jarak = **25** cm

g. Pengecekan terhadap jarak yang diambil

Dari lendutan yang terjadi
 Lendutan Ijin = **0.083** cm
 Lendutan yang terjadi = **0.04276** cm

Lendutan yang terjadi < Lendutan Ijin

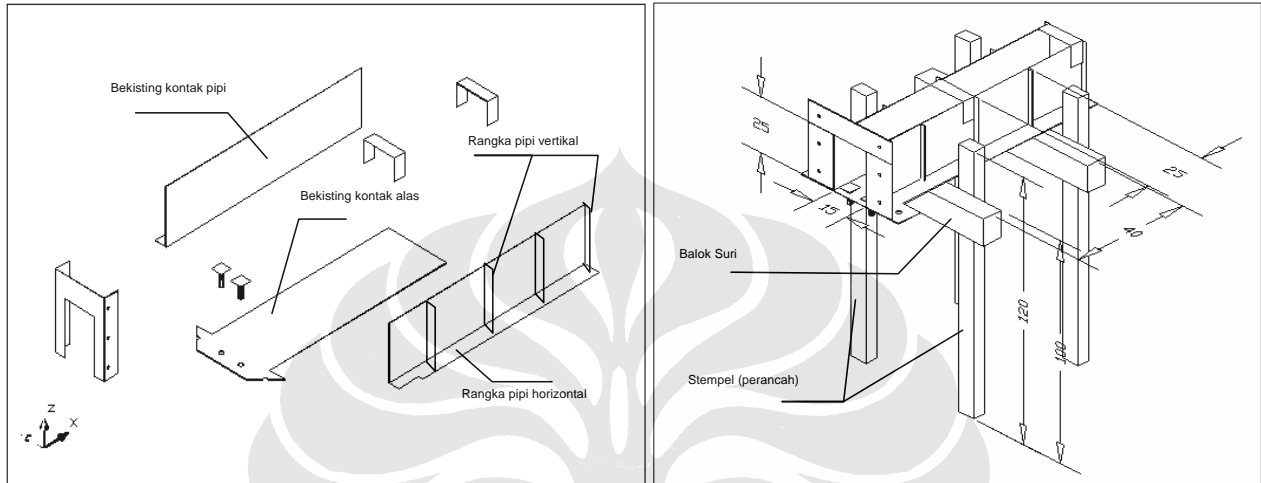
DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING BALOK

Bekisting Baja Untuk Balok

A. Data Dimensi Balok

a. Tinggi Balok	:	0.25	m
b. Lebar balok	:	0.2	m
c. Panjang bentang balok	:	1	m
d. Tinggi lantai ke lantai	:	3	m

B. Data Rencana Material



Keterangan Gambar :

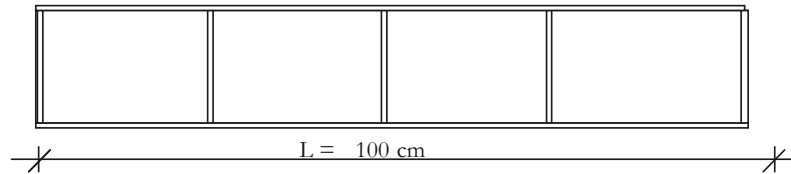
A	:	Bekisting kontak pipi
B	:	Bekisting kontak alas (bodeman)
C	:	Rangka pipi horisontal
D	:	Rangka pipi vertikal
E	:	Balok Suri
F	:	Stempel (Perancah)

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas Kuat Kayu
a.	Bekisting kontak pipi	Plat Baja	BJ 37 Tebal 0,3 mm
b.	Bekisting kontak alas (bodeman)	Plat Baja	BJ 37 Tebal 0,2 mm
c.	Rangka pipi Vertikal	Plat Baja	BJ 37 Tebal 0,2 mm
d.	Rangka pipi horisontal	Plat Baja	BJ 37 Tebal 0,2 mm
e.	Balok Suri	Balok 8/12	III
f.	Stempel (Perancah)	Kaso 5/7	III

DESAIN RANGKA PIPI

Tinjauan Bekisting Kontak Pipi



1. Data teknis

A. Mutu Plat Baja :

BJ37

- Tegangan Leleh	f_y	=	2400	kg/cm ²	
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	1440	kg/cm ²	0.6 x f_y
- Tegangan geser ijin	$\bar{\tau}$	=	960	kg/cm ²	0.4 x f_y
- Berat jenis maksimum	γ_{max}	=	7.85	gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	cm	= 0.0833333 m
- Momen Inersia	I	=	1/12 b h ³	cm ⁴	= 0.05625 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	cm ³	= 0.375 cm ³
- Modulus elastisitas	E	=	2000000	kg/cm ²	

B. Dimensi Tinjauan :

- Tebal Baja	h	=	0.3	cm	= 0.003 m
- Lebar tinjauan	b	=	25	cm	= 0.25 m

C. Spec. Beton

- Berat jenis beton basah	γ_{bt}	=	2500	kg/m ³	
- Tinggi balok	H	=	20	cm	= 0.2 m
- Lebar balok	B	=	15	cm	= 0.15 m

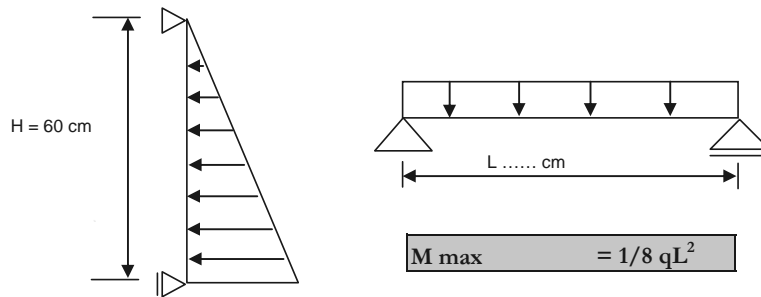
D. Asumsi Beban Kerja

- Komposisi beban kerja		=	150	kg/m ²
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E. Beban yang bekerja

- Beban beton	q beton	=	0,5 x (2500 x 0,2 x 0,15)	=	37.5 kg/m
- Beban kerja	q kerja	=	0,5 x (150 x 0,2)	=	15 kg/m
- Beban Plywood	q plywood	=	0,5 x (7850 x 0,003 x 0,25)	=	2.94375 kg/m
				q total	= 55.44375 kg/m
					= 0.5544375 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned} M_{\text{max}}/W &< \sigma_{\text{lt ijin}} \\ \frac{1}{8} qL^2 &< \sigma_{\text{lt ijin}} \times W \\ \frac{1}{8} \times 0,5544375 \times L^2 &< 540 \text{ kg/cm} \\ L^2 &< \\ L^2 &< 7791,68 \text{ cm}^2 \\ L &< 88,270 \text{ cm} \end{aligned}$$

b. Lendutan

$$\begin{aligned} \frac{5 q \text{ tot } L^4}{384 \times E \times I} &< \frac{L}{300} \text{ cm} \\ \frac{5 \times 0,5544375 \times L^3}{384 \times 2000000 \times 0,05625} &< \frac{1}{300} \text{ cm} \\ L^3 &< \frac{43200000}{831,65625} \text{ cm}^4 \\ L &< 37,312 \text{ cm} \end{aligned}$$

jarak maksimal = 37 cm

4. Kesimpulan

Jadi Baja dengan tebal 3 mm BJ37 dapat digunakan dengan jarak rangka pipi vertikal kurang dari **37 cm**

Pada perencanaan lapangan akan dipakai rangka pipi vertikal dengan jarak 30 cm

DESAIN DAN PENGECEKAN RANGKA PIPi

Tinjauan Plat Baja

1. Data teknis

A. Mutu Baja kontak pipi :

- Type	=	BJ 37	
- Berat jenis maksimum γ max	=	7.85 gr/cm ³	= 7850 kg/m ³
- Tebal baja	=	0.3 cm	= 0.003 m

B. Mutu Baja :

- Type	=	BJ 37	
- Tegangan Leleh f_y	=	2400 kg/cm ²	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	1440 kg/cm ²	
- Tegangan geser ijin $\bar{\tau}$	=	960 kg/cm ²	
- Berat jenis maksimum γ max	=	7.85 gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum δ	=	L / 300 cm	= 0.100 cm
- Momen Inersia I	=	1/12 b h ³ cm ⁴	= 2.083 cm ⁴
- Momen Lawan W	=	1/6 b h ² cm ³	= 0.833 cm ³
- Modulus elastisitas E	=	2000000 kg/cm ²	

D. Dimensi Tinjauan :

- Tinggi baja h	=	5 cm	= 0.05 m
- Lebar baja b	=	0.2 cm	= 0.002 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	
- Tinggi balok H	=	20 cm	= 0.2 m
- Lebar balok d	=	15 cm	= 0.15 m
- Jarak rangka vertikal L	=	30 cm	= 0.3 m

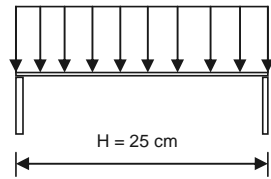
E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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F. Beban yang bekerja

- Beban beton q beton	=	0.5 x (2500 x 0,2 x 0,15)	=	37.5 kg/m
- Beban kerja q kerja	=	0.5 x (150 x 0,2)	=	15 kg/m
- Beban plat kontak pipi q plat kontak	=	0.5 x (7850 x 0,2 x 0,003)	=	2.355 kg/m
- Beban plat rangka vertikal q plat rangka	=	0.5 x (7850 x 0,05 x 0,002)	=	0.3925 kg/m
		q total	=	55.2475 kg/m
			=	0.552 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 55,2475 \times (0,3)^2 \\
 &= \mathbf{0.622 \text{ kg.m}} = \mathbf{62.1534375 \text{ kg.cm}}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 55,2475 \times 0,3 \\
 &= \mathbf{8.287125 \text{ kg}}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 0,552475 \times 30^4}{384 \times 2000000 \times 2,083} = \frac{2237523.75}{1599744000} \\
 &= \mathbf{0.001 \text{ cm}}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 62,1534375 / 1 &< 1440 \text{ kg/cm}^2 \\
 \mathbf{74.6140} &< \mathbf{1440 \text{ kg/cm}^2} \quad \text{.....ok !!!}
 \end{aligned}$$

b. Tegangan Geser

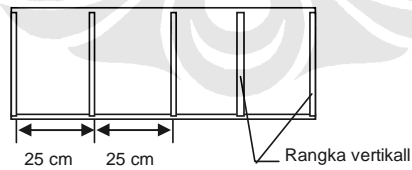
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 8,287125 / 1 &< 960 \text{ kg/cm}^2 \\
 \mathbf{12.4306875} &< \mathbf{960 \text{ kg/cm}^2} \quad \text{.....ok !!!}
 \end{aligned}$$

c. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 \mathbf{0.0014} &< \mathbf{0.100 \text{ cm}} \quad \text{.....ok !!!}
 \end{aligned}$$

4. Kesimpulan

Jadi rangka pipi vertikal Plat baja BJ37 dengan jarak pemasangan 25 cm **AMAN !!!**



DESAIN DAN PENGECEKAN RANGKA ALAS
DIMENSI BALOK 150 X 250

A. DESAIN BEKISTING ALAS

Tinjauan Plat Baja

1. Data teknis

- Tegangan Leleh	f_y	=	2400	kg/cm ²	
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	1440	kg/cm ²	0.6 x f_y
- Tegangan geser ijin	$\bar{\tau}$	=	960	kg/cm ²	0.4 x f_y
- Berat jenis maksimum	γ_{max}	=	7.85	gr/cm ³	= 7850 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	cm	=
- Momen Inersia	I	=	1/12 b h ³	cm ⁴	= 0.03375 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	cm ³	= 0.225 cm ³
- Modulus elastisitas	E	=	2000000	kg/cm ²	

B. Dimensi Tinjauan :

- Tebal Baja	h	=	0.3	cm	= 0.003 m
- Lebar tinjauan	b	=	15	cm	= 0.15 m

C. Spec. Beton

- Berat jenis beton basah	γ_{bt}	=	2500	kg/m ³	
- Tinggi balok	H	=	20	cm	= 0.2 m
- Lebar balok	B	=	15	cm	= 0.15 m

D. Asumsi Beban Kerja

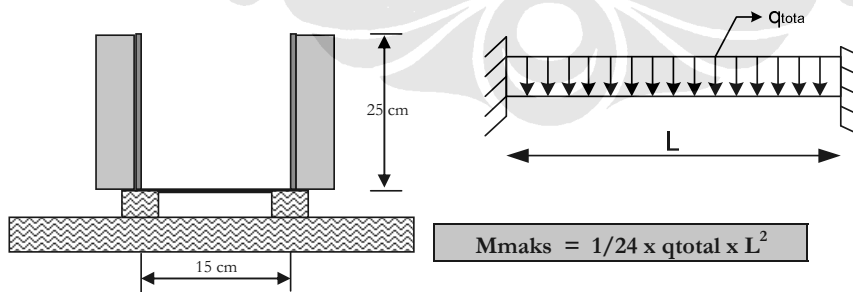
- Komposisi beban kerja	=	150	kg/m ²
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F. Beban yang bekerja

- Beban beton	q beton	=	(2500 x 0,2 x 0,15)	=	75	kg/m	
- Beban kerja	q kerja	=	(150 x 0,15)	=	22.5	kg/m	
- Beban Plywood	q plywood	=	(7850 x 0,15 x 0,003)	=	3.5325	kg/m	
				q total	=	101.0325	kg/m
					=	1.010325	kg/cm

2. Analisa Beban

Jarak antara kaso-kaso = L ?



3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

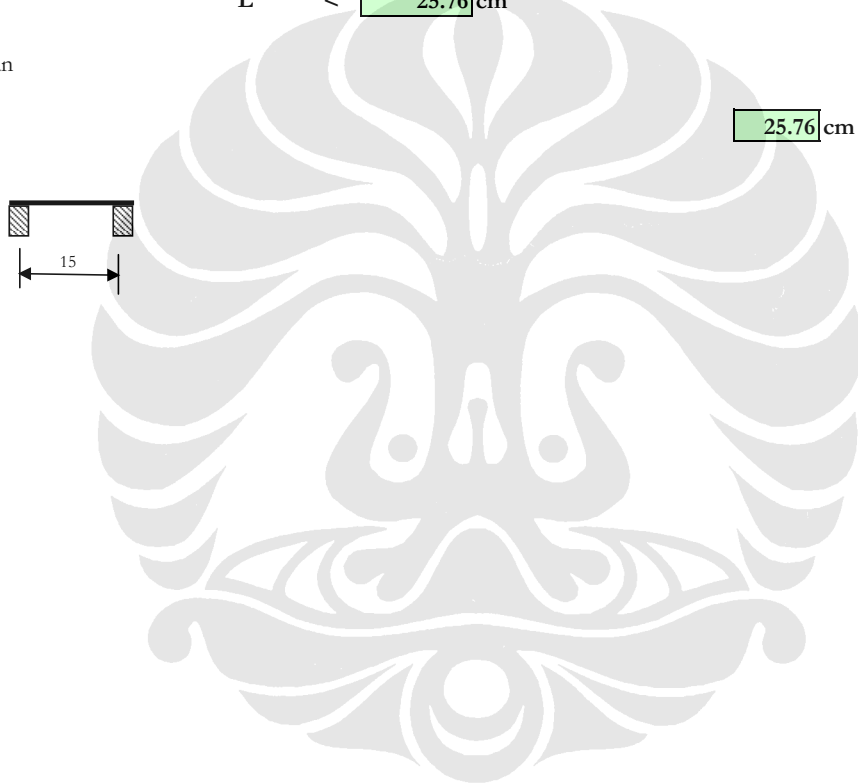
$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 M_{\text{max}} &< \sigma_{\text{ijin}} \times W \\
 1/8 \times q_{\text{total}} \times L^2 &< 1440 \times 0,225 \\
 L^2 &< (8 \times 1440 \times 0,225) / 1,010325 \\
 L^2 &< 2565,51 \text{ cm}^2 \\
 L &< 50,65 \text{ cm}
 \end{aligned}$$

b. Lendutan

$$\begin{aligned}
 \frac{5q_{\text{tot}} L^4}{384 \times E \times I} &< \frac{L}{300} \text{ cm} \\
 L^3 &< \frac{384 \times E \times I}{5 \times 300 \times q} \\
 L^3 &< \frac{384 \times 2000000 \times 0,0337^2}{5 \times 300 \times 1,010325} \\
 L^3 &< 17103,407 \\
 L &< 25,76 \text{ cm}
 \end{aligned}$$

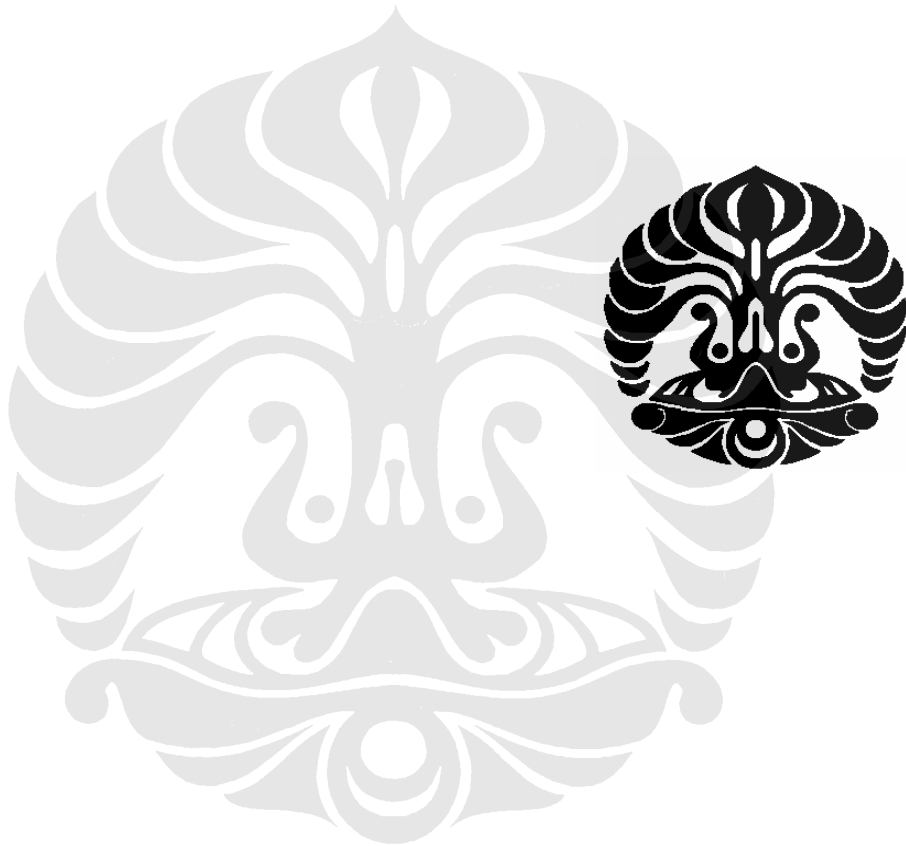
Jarak maksimal =
 = 25,76 cm

4. Kesimpulan



LAMPIRAN C3

Perhitungan Statika Bekisting Kayu (Pondasi, Sloof, Kolom, Balok dan Ring Balok)

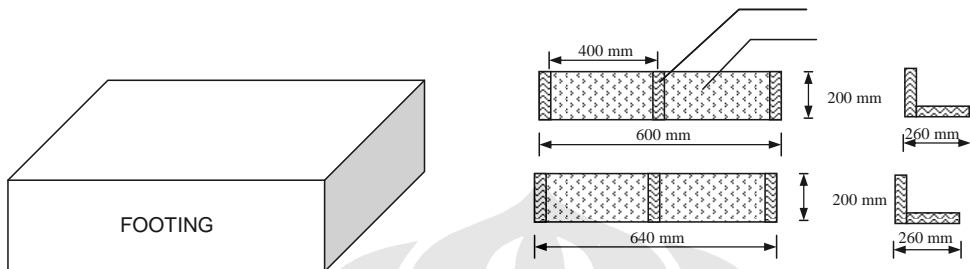


DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING FOOTING PONDASI

A. Data Dimensi Pondasi

- a. Tinggi Pondasi : 0.2 m
b. Lebar Pondasi : 0.6 m
c. Panjang Pondasi : 0.6 m

B. Data Rencana Material



Gambar Bekisting Footing Pondasi

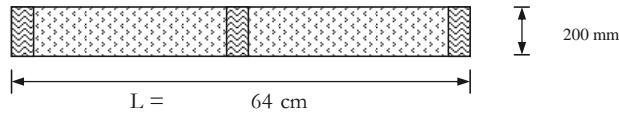
Keterangan Gambar :

- A : Bekisting kontak pipi
B : Rangka pipi horisontal
C : Rangka pipi vertikal

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Type
a.	Bekisting kontak pipi	Plat Baja	BJ 37
b.	Rangka pipi Vertikal	Plat Baja	BJ 37

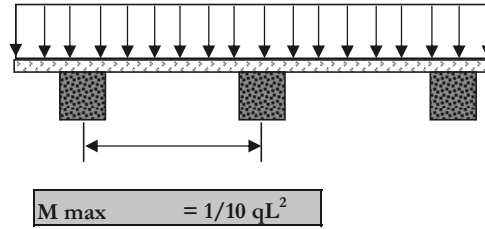
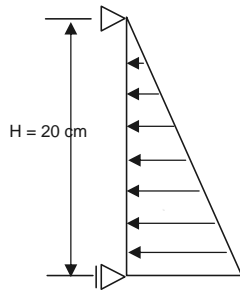
C.DESAIN SIDE BEAM
Tinjauan Plat Baja



1. Data teknis

A. - Kelas Kuat		=	III		
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	75	kg/cm ²	
- Tegangan geser ijin	$\bar{\tau}$	=	8	kg/cm ²	
- Berat jenis maksimum	γ_{max}	=	0.6	gr/cm ³	= 600 kg/m ³
- Berat jenis minimum	γ_{min}	=	0.4	gr/cm ³	= 400 kg/m ³
- Lendutan Maksimum	δ	=	L / 300	cm	= 0.2133333 cm
- Momen Inersia	I	=	1/12 b h ³	cm ⁴	= 13.333 cm ⁴
- Momen Lawan	W	=	1/6 b h ²	cm ³	= 13.333 cm ³
- Modulus elastisitas	E	=	80000	kg/cm ²	
B. Dimensi Tinjauan :					
- Tebal Papan	h	=	2	cm	= 0.02 m
- Lebar tinjauan	b	=	20	cm	= 0.2 m
C. Spec. Beton					
- Berat jenis beton basah	γ_{bt}	=	2500	kg/m ³	
- Tinggi pondasi	H	=	20	cm	= 0.2 m
- Lebar pondasi	B	=	60	cm	= 0.6 m
D. Asumsi Beban Kerja					
- Komposisi beban kerja		=	150	kg/m ²	
F. Faktor Koreksi material kayu					
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat		=	5/6		
		=	0.833		
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap		=	5/4		
		=	1.25		
E. Beban yang bekerja					
- Beban beton	q beton	=	(2500 x 0,2 x 0,6)	=	300 kg/m
- Beban kerja	q kerja	=	(150 x 0,2)	=	30 kg/m
- Beban Plat kontak pipi	q plat pipi	=	(600 x 0,02 x 0,2)	=	2.4 kg/m
	q total	=		=	332.4 kg/m
		=		=	3.324 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M_{\max}/W &< \sigma_{\text{lt ijin}} \\
 1/8 qL^2 &< \sigma_{\text{lt ijin}} \times W \\
 1/10 \times 3,324 \times L^2 &< 1041.640625 \text{ kg/cm} \\
 L^2 &< 3133.70 \text{ cm}^2 \\
 L &< 55.979 \text{ cm}
 \end{aligned}$$

b. Lendutan

$$\begin{aligned}
 \frac{5 q \text{ tot } L^4}{384 \times E \times I} &< \frac{L}{300} \text{ cm} \\
 \frac{1 \times 3,324 \times L^3}{145 \times 80000 \times 13,333} &< \frac{1}{300} \text{ cm} \\
 L^3 &< \frac{154662800}{997.2} \text{ cm}^4 \\
 L &< 53.728 \text{ cm}
 \end{aligned}$$

jarak maksimal = 54 cm

4. Kesimpulan

kurang dari 54 cm

Pada perencanaan lapangan akan dipakai rangka vertikal dengan jarak 30 cm

DESAIN SIDE BEAM

Tinjauan rangka kaso vertikal 4/6 cm

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	=	
- Berat jenis maksimum γ_{max}	=	0.6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0.4 gr/cm ³	=	400 kg/m ³
- Tebal Papan	=	2 cm	=	0.02 m

B. Mutu balok 5/7 :

- Kelas Kuat	=	III	=	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	75 kg/cm ²	=	
- Tegangan geser ijin $\bar{\tau}$	=	8 kg/cm ²	=	
- Berat jenis maksimum γ_{max}	=	0.6 gr/cm ³	=	600 kg/m ³
- Berat jenis minimum γ_{min}	=	0.4 gr/cm ³	=	400 kg/m ³
- Lendutan Maksimum δ	=	L / 300 cm	=	cm
- Momen Inersia I	=	1/12 b h ³ cm ⁴	=	72.000 cm ⁴
- Momen Lawan W	=	1/6 b h ² cm ³	=	24.000 cm ³
- Modulus elastisitas E	=	80000 kg/cm ²	=	

D. Dimensi Tinjauan :

- Tinggi kayu h	=	6 cm	=	0.06 m
- Lebar kayu b	=	4 cm	=	0.04 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	=	
- Tinggi pondasi H	=	20 cm	=	0.2 m
- Lebar Pondasi d	=	60 cm	=	0.6 m
- Jarak rangka vertikal L	=	30 cm	=	0.3 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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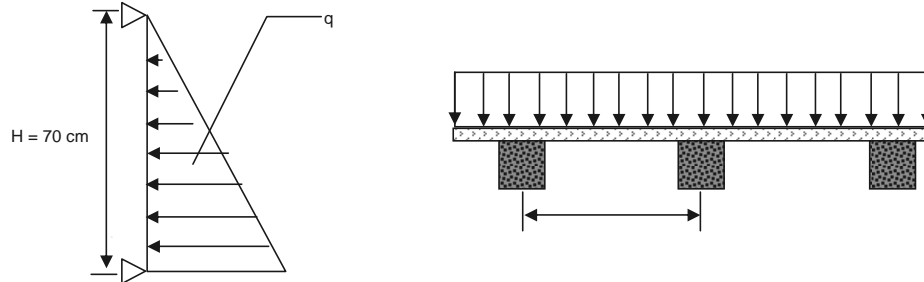
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0.833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1.25

F. Beban yang bekerja

- Beban beton q beton	=	(2500 x 0,2 x 0,6)	=	300 kg/m
- Beban kerja q kerja	=	(150 x 0,6)	=	90 kg/m
- Beban plywood q plywood	=	(600 x 0,2 x 0,02)	=	2.4 kg/m
- Beban sendiri 5/7 q 5/7	=	(600 x 0,06 x 0,04)	=	1.44 kg/m
		q total	=	393.84 kg/m
			=	3.938 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M \text{ max} &= 1/10 qL^2 \\
 &= 1/10 \times 393,84 \times (0,3)^2 \\
 &= \mathbf{4.431 \text{ kg.m}} = \mathbf{443.07 \text{ kg.cm}}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D \text{ max} &= 1/2 q \times L \\
 &= 1/2 \times 393,84 \times 0,3 \\
 &= \mathbf{59.076 \text{ kg}}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f \text{ max} &= \frac{1 q \text{ tot } L^4}{145 \times E \times I} \\
 &= \frac{1 \times 3,9384 \times 60^4}{145 \times 80000 \times 72} = \frac{51041664}{835200000} \\
 &= \mathbf{0.06111 \text{ cm}}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma \text{ ijin} \\
 443,07 / 24 &< 75 \text{ kg/cm}^2 \\
 \mathbf{18.4613} &< \mathbf{75 \text{ kg/cm}^2} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

b. Tegangan Geser

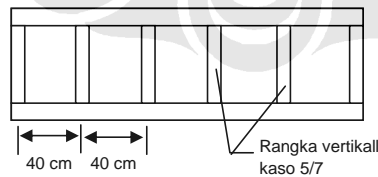
$$\begin{aligned}
 1,5 \times D \text{ max} / A &< \tau \text{ ijin} \\
 1,5 \times 59,076 / 24 &< 8 \text{ kg/cm}^2 \\
 \mathbf{3.69225} &< \mathbf{8 \text{ kg/cm}^2} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

c. Lendutan

$$\begin{aligned}
 f \text{ max} &< L/300 \text{ cm} \\
 \mathbf{0.06111} &< \mathbf{0.200 \text{ cm}} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

4. Kesimpulan

Jadi rangka pipi vertikal kaso 5/7 kelas III dengan jarak pasangan 40 cm **AMAN !!!**

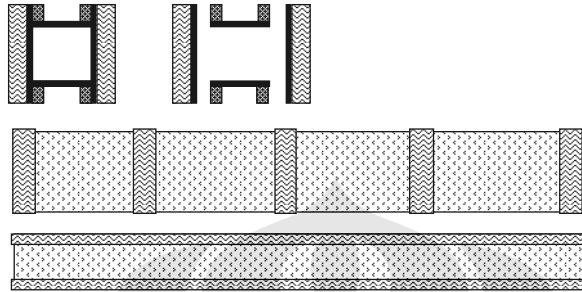


PERHITUNGAN PENGECEKAN KOMPOSISI BEKISTING KOLOM

Bekisting baja untuk kolom

1. DATA UMUM

Tinggi Kolom	=	300	cm
Lebar Kolom	=	20	cm
Panjang Kolom	=	20	cm
Berat Jenis Beton Basah	=	2500	kg/m ³
Beban Kerja	=	150	kg/m ²
Beban Bekisting	=	45	kg/m ²



Potongan Rencana Penampang Bekisting Kolom

Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas kayu
A	Bekisting kontak	Papan 2/20	III
B	Balok tiang	Balok 4/6	III
C	Balok perangkai	Balok 4/6	III

2. Tinjauan Bekisting Kontak

a. Data Properti Material

Jenis Material	Kelas Kuat	Properti Material			Dimensi Tinjauan		Properti Penampang	
		Teg. Lentur Ijin $\overline{\sigma_{II}}$ (kg/cm ²)	Berat Jenis γ (kg/cm ³)	Modulus E E (kg/cm ²)	Lebar L (cm)	Tebal t (cm)	Momen Inersia I (cm ⁴)	Momen Lawan W (cm ³)
Papan 2/20	III	75	600	80000	100	2	66.6666667	66.6666667

b. Data Teknis Pendukung

a. Spesi beton			
- Berat jenis beton	=	2500	kg/m ³
- Tebal beton	=	0.2	m
b. Faktor koreksi material			
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6	
	=	0.833	
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4	
	=	1.250	

c. Beban kerja dan Beban bekisting			
- Beban kerja	=	150	kg/m ²
- Beban bekisting	=	45	kg/m ²
- Faktor pengali beban	=	1/0,7	= 1.429

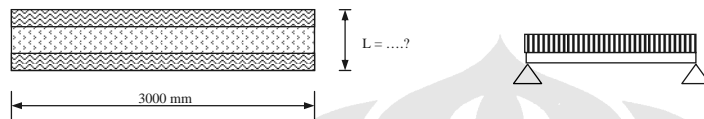
c. Data Pembebanan

- Beban Beton	=	(0,5*2500*0,2*3)	=	750	kg/m
- Beban Kerja	=	(0,5*150*3)	=	225	kg/m
- Beban Bekisting	=	(0,5*45*3*1/0,7)	=	96.42857143	kg/m
Pembebanan Total	q total		=	1071.429	kg/m
			=	10.714	kg/cm

d. Rumus-rumus Pendukung

a. Momen maksimum	Mmax =	$1/8 \cdot q \cdot L^2$
b. Lendutan	f max =	$\frac{5 \cdot q \cdot L^4}{384 \cdot E \cdot I}$

e. Menentukan Jarak Balok tiang



Dari segi kekuatan

M_{max}/W_x	<	$\frac{\sigma_{lt}}{\sigma_{lt} \cdot W_x}$	x faktor koreksi
M_{max}	<		
$1/8 \cdot q \cdot L^2$	<	5208.333333	kg.cm
L^2	<	3888.89	
L	<	62.4	cm

Lendutan Yang Terjadi

$(5 \cdot q \cdot L^4)/(384 \cdot E \cdot I)$	<	$L/300$	
L^3	<	$(384 \cdot EI)/300 \cdot 5 \cdot q$	
L^3	<	127431.11	cm ³
L	<	50.32	cm

f. Menentukan Jarak Balok tiang

Jarak balok tiang yang diperkenankan kurang dari **50.3** cm

Di lapangan digunakan jarak = **20** cm

g. Pengecekan terhadap jarak yang diambil

Dari lendutan yang terjadi

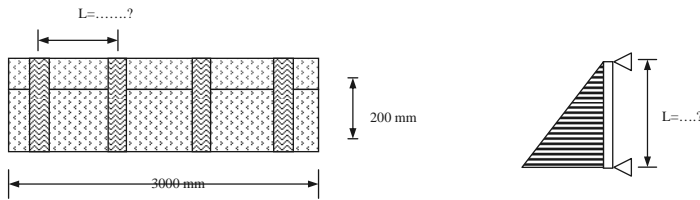
Lendutan Ijin	=	0.067	cm
Lendutan yang terjadi	=	0.00222	cm
Lendutan yang terjadi	<	Lendutan ijin	0.00222 < 0.067 Memenuhi syarat

Dari tegangan yang terjadi

Tegangan Ijin	=	78.125	kg/cm ²
Tegangan yang terjadi	=	6.428571429ok
Tegangan yang terjadi	<	Tegangan lentur ijin	6.428571429 < 78.125 Memenuhi syarat

Maka jarak balok tiang = 20 cm aman dipakai

3. Menentukan jarak balok perangkai



a. Data Properti Material

Jenis Material	Kelas Kuat	Properti Material			Dimensi Tinjauan		Properti Penampang	
		Teg. Lentur Ijin $\frac{\sigma}{t}$ (kg/cm ²)	Berat Jenis γ (kg/cm ³)	Modulus E E (kg/cm ²)	Lebar L (cm)	Tinggi t (cm)	Momen Inersia I (cm ⁴)	Momen Lawan W (cm ³)
Balok 4/6	III	75	600	80000	20	2	13.33333333	13.33333333

b. Data Teknis Pendukung

- a. Spesi beton
- Berat jenis beton = 2500 kg/m³
 - Tebal beton = 0.2 m
- b. Faktor koreksi material
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat = 5/6 = 0.833
 - Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap = 5/4 = 1.250
- c. Beban kerja dan Beban bekisting
- Beban kerja = 150 kg/m²
 - Beban bekisting = 45 kg/m²
 - Faktor pengali beban = 1/0.7 = 1.429

c. Data Pembebanan

- Beban yang terjadi = 1071.429 kg/m²
- = 0.107 kg/cm²
- Lebar kolom = 20 cm

Sehingga muatan yang terjadi pada balok perangkai = 2.143 kg/cm

e. Menentukan Jarak Balok tiang

Dari segi kekuatan

$$\begin{aligned} M_{max}/W_x &< \frac{\sigma}{t} \times \text{faktor koreksi} \\ M_{max} &< \frac{\sigma}{t} \times W_x \\ 1/10q.L^2 &< 1041.666667 \text{ kg.cm} \\ L^2 &< 4861.11 \\ L &< 69.7 \text{ cm} \end{aligned}$$

Lendutan Yang Terjadi

$$\begin{aligned} 1/145.(q.L^4)/EI &< L/300 \\ L^3 &< (145 \cdot EI)/300q \\ L^3 &< 240592.59 \text{ cm}^3 \\ L &< 62.20 \text{ cm} \end{aligned}$$

f. Menentukan Jarak Balok tiang

Jarak balok tiang yang diperkenankan kurang dari 62.2 cm

Di lapangan digunakan jarak = 40 cm

g. Pengecekan terhadap jarak yang diambil

Dari lendutan yang terjadi

Lendutan Ijin = 0.133 cm
Lendutan yang terjadi = 0.03547 cm

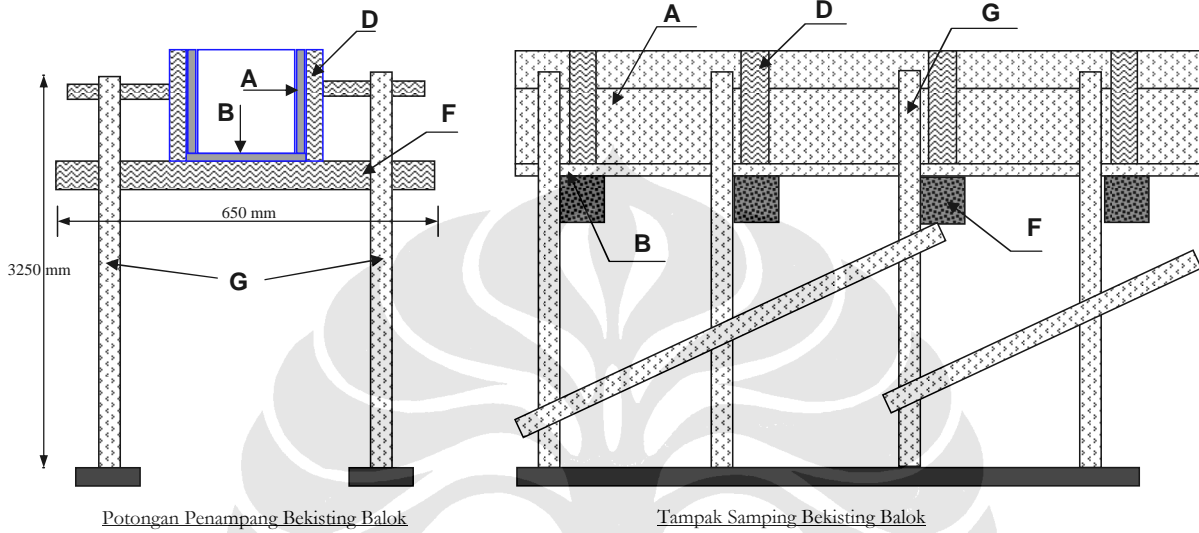
Lendutan yang terjadi < Lendutan ijin
0.03547 < 0.133

Memenuhi syarat

A. Data Dimensi Balok

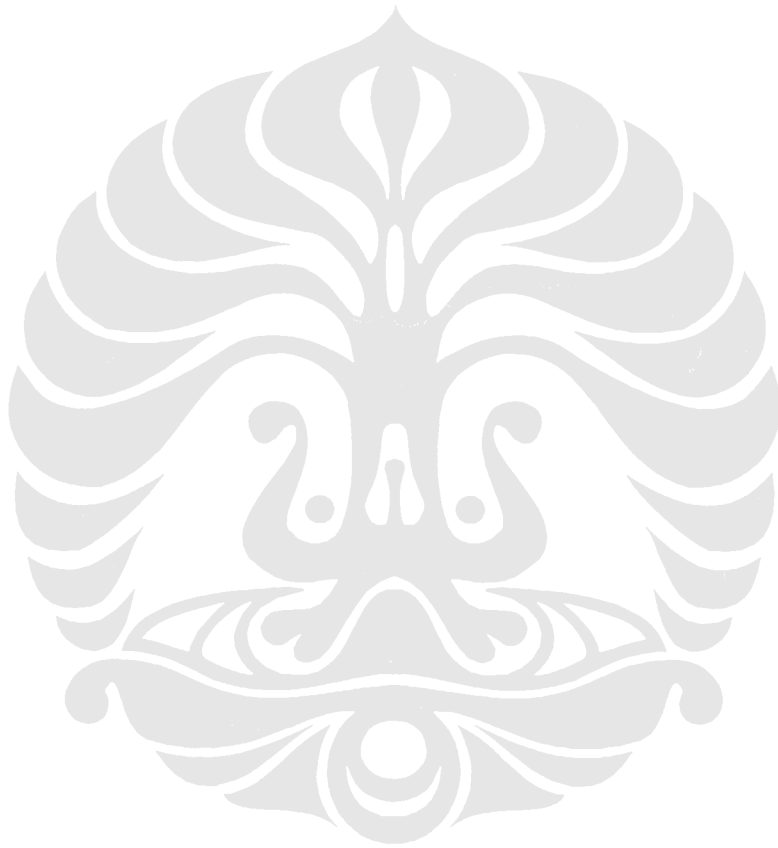
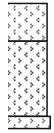
- a. Tinggi Balok : 0.2 m
- b. Lebar balok : 0.15 m
- c. Panjang bentang balok : 1 m
- d. Tinggi lantai ke lantai : 3 m

B. Data Rencana Material



Perencanaan Material

No	Bagian Bekisting	Material Rencana	Kelas Kuat Kayu
a.	Bekisting kontak pipi	Papan 2/20	III
b.	Bekisting kontak alas (bodeman)	Papan 2/20	III
c.	Rangka pipi Vertikal	Kaso 4/6	III
e.	Rangka alas (bodeman)	Kaso 4/6	III
f.	Balok Suri	Balok 6/15	III
g.	Stempel (Perancah)	Kaso 5/7	III



DESAIN DAN PENGECEKAN KOMPOSISI BEKISTING BALOK

DIMENSI BALOK 400 X 700

METODE KONVENSIONAL

A. DESAIN BEKISTING ALAS (BOTTOM OF BEAM)

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	
- Tegangan lentur ijin $\bar{\sigma}_t$	=	75	kg/cm ²
- Tegangan geser ijin $\bar{\tau}$	=	8	kg/cm ²
- Berat jenis maksimum γ_{max}	=	0.6	gr/cm ³ = 600 kg/m ³
- Berat jenis minimum γ_{min}	=	0.4	gr/cm ³ = 400 kg/m ³
- Lendutan Maksimum δ	=	L / 300	cm
- Momen Inersia I	=	1/12 b h ³	cm ⁴ = 10 cm ⁴
- Momen Lawan W	=	1/6 b h ²	cm ³ = 10 cm ³
- Modulus elastisitas E	=	80000	kg/cm ²

C. Dimensi Tinjauan :

- Tebal papan h	=	2	cm = 0.02 m
- Lebar Tinjauan b	=	15	cm = 0.15 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500	kg/m ³
- Tinggi balok H	=	20	cm = 0.2 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150	kg/m ² (F. Wigbout)
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F. Faktor Koreksi material kayu

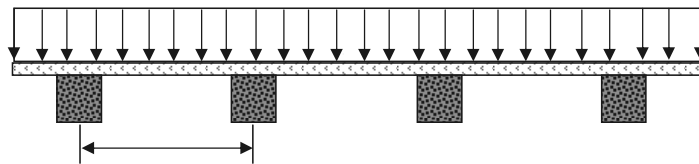
- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0.833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1.25

F. Beban yang bekerja

- Beban beton q beton	=	(2500 x 0,2 x 0,15)	=	75	kg/m
- Beban kerja q kerja	=	(150 x 0,15)	=	22.5	kg/m
- Beban Plywood q plywood	=	(600 x 0,15 x 0,02)	=	1.8	kg/m
q total				=	99.3 kg/m
				=	0.993 kg/cm

2. Analisa Beban

Jarak antara kaso-kaso= L ?



$M_{maks} = 1/10 \times q_{total} \times L^2$

3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned} M/W &< \sigma_{ijin} \times \text{faktor koreksi} \\ M_{max} &< \sigma_{ijin} \times \text{faktor koreksi} \times W \\ 1/10 \times q_{total} \times L^2 &< 75 \times 5/6 \times 5/4 \times 10 \\ L^2 &< (10 \times 781,25) / 0,993 \\ L^2 &< 7867,57 \text{ cm}^2 \\ L &< 88,70 \text{ cm} \end{aligned}$$

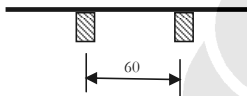
b. Lendutan

$$\begin{aligned} \frac{q_{tot} L^4}{145 \times E \times I} &< \frac{L}{300} \text{ cm} \\ L^3 &< \frac{145 \times E \times I}{300 \times q} \\ L^3 &< \frac{145 \times 80000 \times 10}{300 \times 0,993} \\ L^3 &< 389392,41 \\ L &< 73,02 \text{ cm} \end{aligned}$$

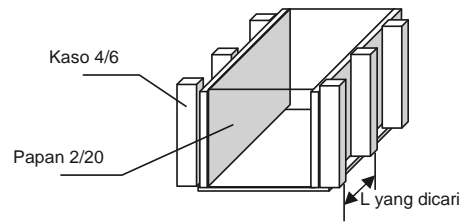
\rightarrow Jarak maksimal = $73,02 \text{ cm}$

4. Kesimpulan

Bekisting kontak alas (papan 2/20) di beri tumpuan berupa balok suri dengan jarak kurang dari **73,02 cm**
Di lapangan menggunakan jarak 60 cm



C.DESAIN SIDE BEAM
Tinjauan papan 2/20



1. Data teknis

A. Mutu plywood :

- Kelas Kuat	=	III	
- Tegangan lentur ijin	$\bar{\sigma}_{lt}$	=	75 kg/cm ²
- Tegangan geser ijin	$\bar{\tau}$	=	8 kg/cm ²
- Berat jenis maksimum	γ_{max}	=	0.6 gr/cm ³ = 600 kg/m ³
- Berat jenis minimum	γ_{min}	=	0.4 gr/cm ³ = 400 kg/m ³
- Lendutan Maksimum	δ	=	L / 300 cm = cm
- Momen Inersia	I	=	1/12 b h ³ cm ⁴ = 16.667 cm ⁴
- Momen Lawan	W	=	1/6 b h ² cm ³ = 16.667 cm ³
- Modulus elastisitas	E	=	80000 kg/cm ²

B. Dimensi Tinjauan :

- Tebal Plywood	h	=	2 cm = 0.02 m
- Lebar tinjauan	b	=	25 cm = 0.25 m

C. Spec. Beton

- Berat jenis beton basah	γ_{bt}	=	2500 kg/m ³
- Tinggi balok	H	=	20 cm = 0.2 m
- Lebar balok	B	=	15 cm = 0.15 m

D. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²
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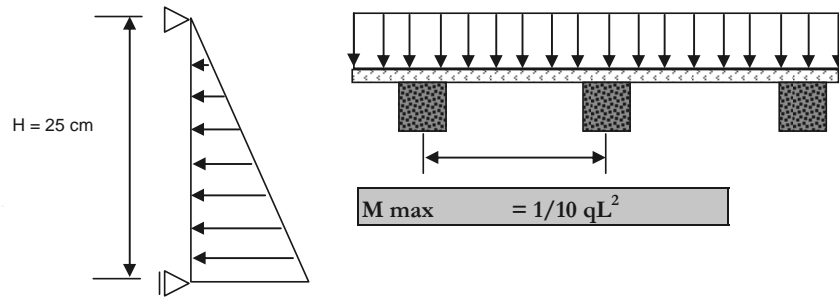
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6
	=	0.833
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4
	=	1.25

E. Beban yang bekerja

- Beban beton	q beton	=	(2500 x 0,2 x 0,15)	=	75 kg/m
- Beban kerja	q kerja	=	(150 x 0,2)	=	30 kg/m
- Beban Plywood	q plywood	=	(600 x 0,02 x 0,25)	=	3 kg/m
<hr/>					
	q total	=		=	108 kg/m
		=		=	1.08 kg/cm

2. Analisa Beban



3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned} M_{\max}/W &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \\ \frac{1}{10} qL^2 &< \sigma_{\text{lt ijin}} \times \text{faktor koreksi} \times W \\ \frac{1}{10} \times 1,08 \times L^2 &< 1302,109375 \text{ kg/cm}^2 \\ L^2 &< 1302,109375 / (\frac{1}{10} \times 1,08) \\ L^2 &< 12056,57 \text{ cm}^2 \\ L &< \mathbf{109.802 \text{ cm}} \end{aligned}$$

b. Lendutan

$$\begin{aligned} \frac{1 q_{\text{tot}} L^4}{145 \times E \times I} &< \frac{L}{300} \text{ cm} \\ \frac{1 \times 1,08 \times L^3}{145 \times 80000 \times 16,667} &< \frac{1}{300} \text{ cm} \\ L^3 &< \frac{193337200}{324} \text{ cm}^4 \\ L &< \mathbf{84.189 \text{ cm}} \end{aligned}$$

jarak maksimal = **84 cm**

4. Kesimpulan

Digunakan Rangka Vertikal Kaso 4/6 dengan jarak kurang dari **84 cm**

Pada perencanaan lapangan akan dipakai rangka vertikal kaso 4/6 dengan jarak 60 cm

D.DESAIN SIDE BEAM

Tinjauan rangka kaso vertikal 4/6 cm

1. Data teknis

A. Mutu Plywood :

- Kelas Kuat	=	III	
- Berat jenis maksimum γ_{max}	=	0.6 gr/cm ³	= 600 kg/m ³
- Berat jenis minimum γ_{min}	=	0.4 gr/cm ³	= 400 kg/m ³
- Tebal Papan	=	2 cm	= 0.02 m

B. Mutu balok 5/7 :

- Kelas Kuat	=	III	
- Tegangan lentur ijin $\bar{\sigma}_{lt}$	=	75 kg/cm ²	
- Tegangan geser ijin $\bar{\tau}$	=	8 kg/cm ²	
- Berat jenis maksimum γ_{max}	=	0.6 gr/cm ³	= 600 kg/m ³
- Berat jenis minimum γ_{min}	=	0.4 gr/cm ³	= 400 kg/m ³
- Lendutan Maksimum δ	=	L / 300	= cm
- Momen Inersia I	=	1/12 b h ³	= 72.000 cm ⁴
- Momen Lawan W	=	1/6 b h ²	= 24.000 cm ³
- Modulus elastisitas E	=	80000 kg/cm ²	

D. Dimensi Tinjauan :

- Tinggi kayu h	=	6 cm	= 0.06 m
- Lebar kayu b	=	4 cm	= 0.04 m

D. Spec. Beton

- Berat jenis beton basah γ_{bt}	=	2500 kg/m ³	
- Tinggi balok H	=	20 cm	= 0.2 m
- Lebar Balok d	=	15 cm	= 0.15 m
- Jarak rangka vertikal L	=	80 cm	= 0.8 m

E. Asumsi Beban Kerja

- Komposisi beban kerja	=	150 kg/m ²	
-------------------------	---	-----------------------	--

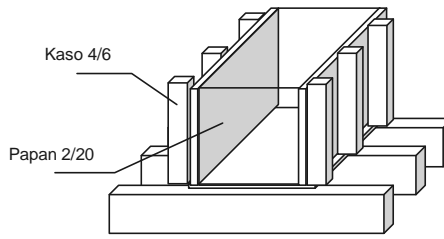
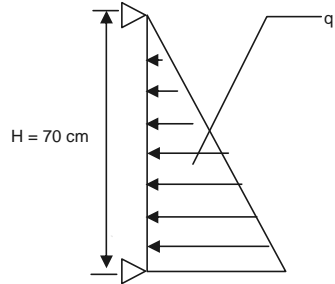
F. Faktor Koreksi material kayu

- Kondisi konstruksi yang tidak terlindung tetapi kayu dapat mengering dengan cepat	=	5/6	
	=	0.833	
- Kondisi konstruksi yang tegangannya diakibatkan muatan tetap dan tidak tetap	=	5/4	
	=	1.25	

F. Beban yang bekerja

- Beban beton q beton	=	0.5 x (2500 x 0,2 x 0,15)	= 37.5 kg/m
- Beban kerja q kerja	=	0.5 x (150 x 0,15)	= 11.25 kg/m
- Beban plywood q plywood	=	0.5 x (600 x 0,2 x 0,02)	= 1.2 kg/m
- Beban sendiri 5/7 q 5/7	=	0.5 x (600 x 0,06 x 0,04)	= 0.72 kg/m
		q total	= 50.67 kg/m
			= 0.507 kg/cm

2. Analisa Statika



Reaksi Momen Maksimum

$$\begin{aligned}
 M_{\max} &= \frac{1}{8} qL^2 \\
 &= \frac{1}{8} \times 50,67 \times (0,8)^2 \\
 &= \mathbf{4.054 \text{ kg.m}} = \mathbf{405.36 \text{ kg.cm}}
 \end{aligned}$$

Reaksi Gaya Geser Maksimum

$$\begin{aligned}
 D_{\max} &= \frac{1}{2} q \times L \\
 &= \frac{1}{2} \times 50,67 \times 0,8 \\
 &= \mathbf{20.268 \text{ kg}}
 \end{aligned}$$

Reaksi Lendutan maksimum :

$$\begin{aligned}
 f_{\max} &= \frac{5 q \text{ tot } L^4}{384 \times E \times I} \\
 &= \frac{5 \times 0,5067 \times 15^4}{384 \times 80000 \times 72} = \frac{128258.4375}{2211840000} \\
 &= \mathbf{0.00006 \text{ cm}}
 \end{aligned}$$

3. Kontrol Terhadap Tegangan

a. Tegangan Lentur

$$\begin{aligned}
 M/W &< \sigma_{\text{ijin}} \\
 405,36 / 24 &< 75 \text{ kg/cm}^2 \\
 \mathbf{16.8900} &< \mathbf{75 \text{ kg/cm}^2} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

b. Tegangan Geser

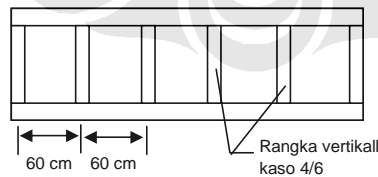
$$\begin{aligned}
 1,5 \times D_{\max} / A &< \tau_{\text{ijin}} \\
 1,5 \times 20,268 / 24 &< 8 \text{ kg/cm}^2 \\
 \mathbf{1.26675} &< \mathbf{8 \text{ kg/cm}^2} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

c. Lendutan

$$\begin{aligned}
 f_{\max} &< L/300 \text{ cm} \\
 \mathbf{0.00006} &< \mathbf{0.050 \text{ cm}} \dots\dots\dots \text{memenuhi syarat !!!!!!!!}
 \end{aligned}$$

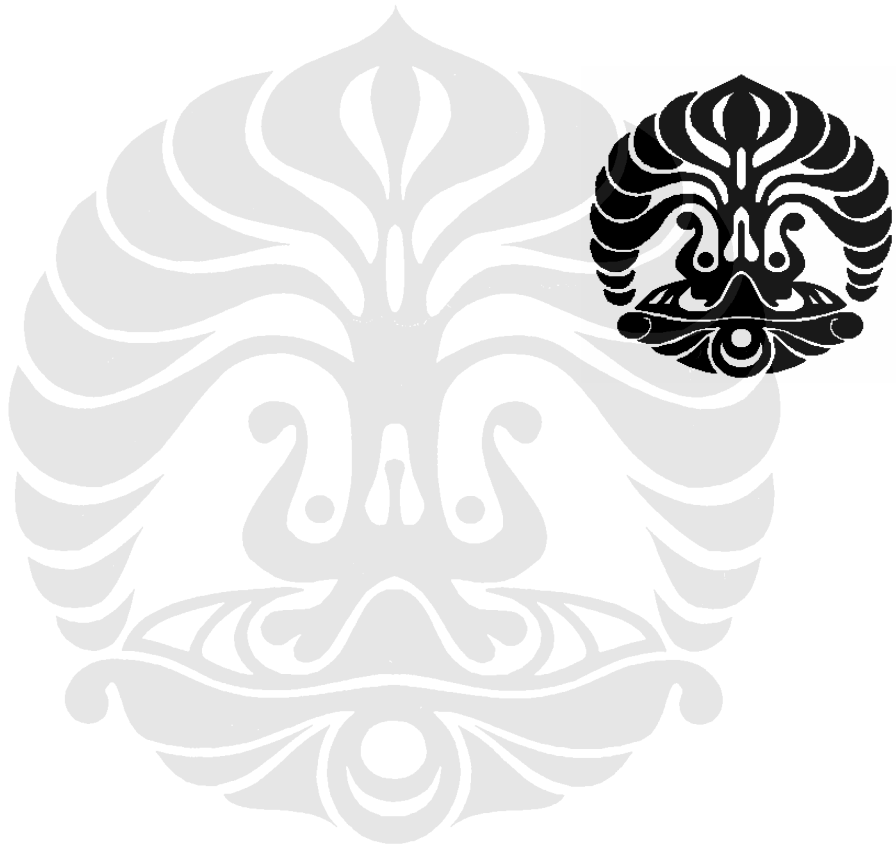
4. Kesimpulan

Jadi rangka pipi vertikal kaso 5/7 kelas III dengan jarak pasangan 60 cm **AMAN !!!**



LAMPIRAN D1

Analisa Biaya Bekisting Konvensional (Pondasi, Sloof, Kolom, Balok dan Ring Balok)



BILL OF QUANTITY
Bekisting Cara Tradisional Rumah Tinggal 1 Lantai

No.	Uraian Pekerjaan	Volume	Satuan
	Bangunan 2 lantai		
	Pembetonan		
1	<u>Pondasi</u>		
	Footing	0,864	m3
	Pedestal	0,384	m3
2	<u>Sloof</u>	1,0775	m3
3	<u>Kolom lt.1</u>	0,72	m3
6	<u>Ring balk</u>	0,431	m3
	Bekisting		
a.	<u>Bekisting pondasi</u>		
	Footing	0,48	m2
	Pedestal	0,64	m2
b.	<u>Bekisting sloof</u>	21,55	m2
c.	<u>Bekisting kolom lt.1</u>	1,8	m2
f.	<u>Bekisting ring balk</u>	12,93	m2

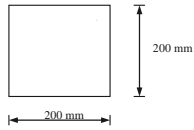
BACK UP PERHITUNGAN MATERIAL DAN ALAT

Metode Cara Tradisional

Pondasi Setempat

n = 12

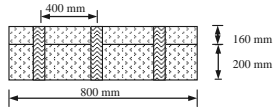
Pedestal



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
200	200	160	800

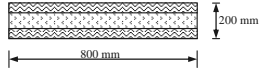
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	2000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

Sisi 1 dan 3



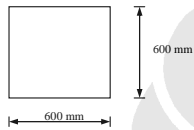
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	3
1	100	800	360

Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	2
			800

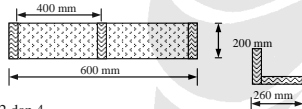
Footing



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
600	600	100	200

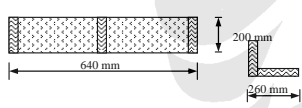
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

Sisi 1 dan 3



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	600	3
			200
			3
			200

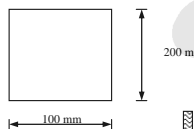
Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	640	3
			200
			3
			200

Sloof

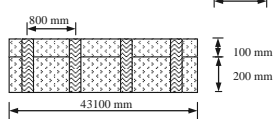
n = 1



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	200	0	43100

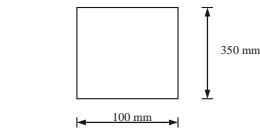
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

Sisi 1 dan 3

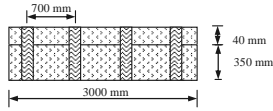


Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	43100	55
			200 m'
			55
			200 m'

Kolom It 1 n = 12



Sisi 1 dan 3

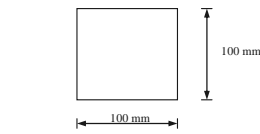


Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	350	40	3000

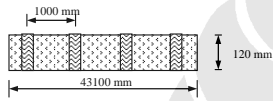
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso	
1	350	3000	6	450
1	40	3000		

Ring balok = 3 m n = 1



Sisi 1 dan 3



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	100	20	43100

Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso	
1	120	43100	45	120

Daftar Kebutuhan Material

Ukuran Papan 2/20 (mm2)=	0.02	x	0.2	x	2 mm
Ukuran Kaso 4/6 (mm') =	0.04	x	0.06	x	4 mm
Ukuran Kaso 5/7 (mm') =	0.05	x	0.07	x	4 mm
Ukuran Balok 8/12 (mm') =	0.08	x	0.12	x	4 mm

No.	Uraian	n	Jml papan	Ukuran Papan		Luas Total	Jml Papan (lbr)	Jml Kaso	Ukuran Kaso P (m)	Panjang Total P (m)	Volume Kaso (m3)
				L (m)	P (m)						
1	Pondasi Setempat										
	<u>Pedestal</u>										
	Sisi 1 dan 3	12	1	0.2	0.8	1.92	2.4	3	0.36	12.96	0.031104
	Sisi 2 dan 4	12	1	0.1	0.8	0.96	1.2				
	Sisi 2 dan 4	12	1	0.2	0.8	1.92	2.4	2	0.8	19.2	0.04608
	<u>Footing</u>										
	Sisi 1 dan 3	12	1	0.2	0.6	1.44	1.8	3	0.2	7.2	0.01728
	Sisi 2 dan 4	12	1	0.2	0.64	1.536	1.92	3	0.2	7.2	0.01728
	Sisi 2 dan 4	12	1	0.2	0.64	1.536	1.92	3	0.2	7.2	0.01728
	TOTAL					7,776	9,72			60,96	0,146304
2	Sloof 3 m										
	Sisi 1 dan 3	1	1	0.2	43.1	8.62	10.775	55	0.2	11	0.0264
	Sisi 2 dan 4							55	0.2	0	0
	TOTAL					8,62	10,775			11	0,0264
3	Kolom lt.1										
	Sisi 1 dan 3	12	1	0.35	3	12.6	15.75	6	0.45	32.4	0.07776
	Sisi 2 dan 4	12	1	0.04	3	1.44	1.8				
	TOTAL					14,04	17,55			32,4	0,07776
6	Ring balok = 3 m										
	Sisi 1 dan 3	1	1	0.12	43.1	5.172	6.465	45	0.12	5.4	0.01296
	TOTAL					5,172	6,465			5,4	0,01296
TOTAL						Papan 2/20 =	71,216		Kaso 4/6 =	219,52	0,526848

DAFTAR HARGA MATERIAL

NO	URAIAN	SATUAN	HARGA SATUAN
	Papan Randu 2/20	lbr	Rp 48.000,00
	Kaso 4/6	m3	Rp 2.100.000,00
	Kaso 5/7	m3	Rp 2.100.000,00
	Balok 8/12	m3	Rp 2.100.000,00
	Paku	kg	Rp 8.000,00
	Minyak Bekisting	ltr	Rp 2.500,00

Biaya Kebutuhan Material Untuk Bekisting

No.	Uraian	Luas Pembetonan	Volume	Satuan	Harga Satuan	Total
1	Pondasi Setempat	1,12				
	Papan Randu 2/20		9,72	lbr	Rp 48.000,00	Rp 466.560,00
	Kaso 4/6		0,146304	m3	Rp 2.100.000,00	Rp 307.238,40
	Paku		0,336	kg	Rp 8.000,00	Rp 2.688,00
	Minyak Bekisting		0,224	ltr	Rp 2.500,00	Rp 560,00
2	Sloof	21,55				
	Papan Randu 2/20		10,775	lbr	Rp 48.000,00	Rp 517.200,00
	Kaso 4/6		0,0264	m3	Rp 2.100.000,00	Rp 55.440,00
	Paku		6,465	kg	Rp 8.000,00	Rp 51.720,00
	Minyak Bekisting		4,31	ltr	Rp 2.500,00	Rp 10.775,00
3	Kolom I.I	1,8				
	Papan Randu 2/20		17,55	lbr	Rp 48.000,00	Rp 842.400,00
	Kaso 4/6		0,07776	m3	Rp 2.100.000,00	Rp 163.296,00
	Paku		0,54	kg	Rp 8.000,00	Rp 4.320,00
	Minyak Bekisting		0,36	ltr	Rp 2.500,00	Rp 900,00
6	Ring balok	12,93				
	Papan Randu 2/20		6,465	lbr	Rp 48.000,00	Rp 310.320,00
	Kaso 4/6		0,01296	m3	Rp 2.100.000,00	Rp 27.216,00
	Paku		3,879	kg	Rp 8.000,00	Rp 31.032,00
	Minyak Bekisting		2,586	ltr	Rp 2.500,00	Rp 6.465,00
	TOTAL					Rp 2.798.130,40

DAFTAR HARGA UPAH

NO	URAIAN	KOEFISIEN	SATUAN	HARGA SATUAN
	Pekerja	0,3300	hari	40000
	Mandor	0,0330	hari	55000
	Tukang Kayu	0,3200	hari	50000
	Kepala Tukang Kayu	0,0060	hari	55000

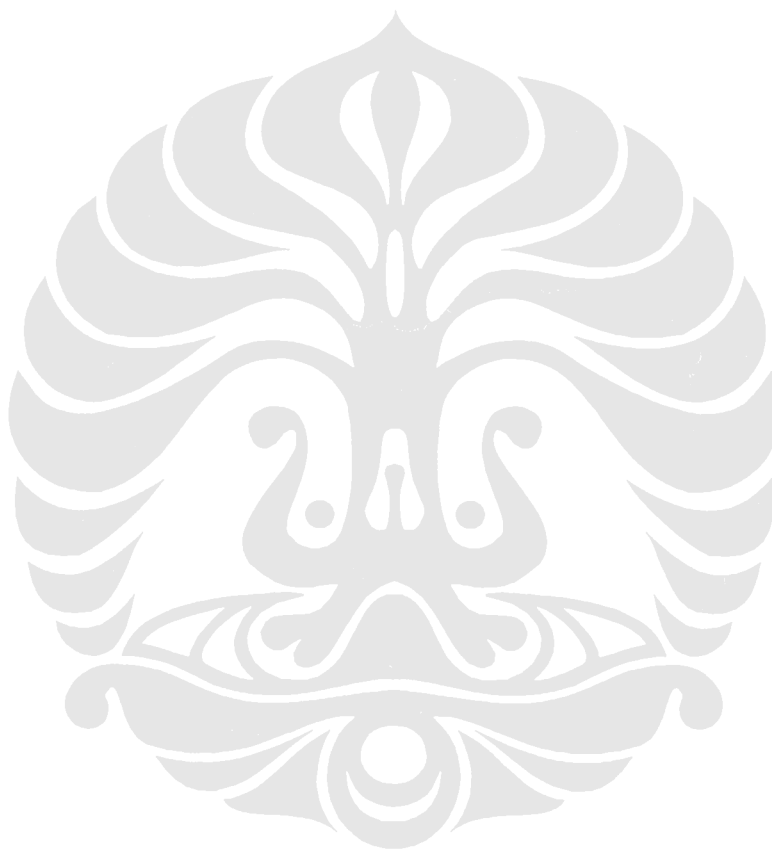
Biaya Kebutuhan Upah Untuk Bekisting

No.	Uraian	Volume pembedonan	Satuan	Koefisien	Volume total	Satuan	Harga Satuan/m2	Total
1	Pondasi Setempat	1,12	m2					
	Pekerja			0,33	0,3696	hari	40000	Rp 14.784,00
	Mandor			0,033	0,03696	hari	55000	Rp 2.032,80
	Tukang Kayu			0,32	0,3584	hari	50000	Rp 17.920,00
	Kepala Tukang Kayu			0,006	0,00672	hari	55000	Rp 369,60
2	Sloof	21,55	m2					
	Pekerja			0,33	7,1115	hari	40000	Rp 284.460,00
	Mandor			0,033	0,71115	hari	55000	Rp 39.113,25
	Tukang Kayu			0,32	6,896	hari	50000	Rp 344.800,00
	Kepala Tukang Kayu			0,006	0,1293	hari	55000	Rp 7.111,50
3	Kolom lt. 1	1,8	m2					
	Pekerja			0,33	0,594	hari	40000	Rp 23.760,00
	Mandor			0,033	0,0594	hari	55000	Rp 3.267,00
	Tukang Kayu			0,32	0,576	hari	50000	Rp 28.800,00
	Kepala Tukang Kayu			0,006	0,0108	hari	55000	Rp 594,00
6	Ring balok	12,93	m2					
	Pekerja			0,33	4,2669	hari	40000	Rp 170.676,00
	Mandor			0,033	0,42669	hari	55000	Rp 23.467,95
	Tukang Kayu			0,32	4,1376	hari	50000	Rp 206.880,00
	Kepala Tukang Kayu			0,006	0,07758	hari	55000	Rp 4.266,90
	TOTAL							Rp 1.172.303,00

Biaya Pekerjaan Bekisting

1 rumah tinggal 1 kali pakai

No.	Uraian	Volume pembedonan	Satuan	Harga Material	Harga Upah	Total
1	Pondasi	1,248	m3	Rp 776.486,4	Rp 35.106,40	Rp 811.592,80
2	Sloof	1,0775	m3	Rp 624.360,0	Rp 675.484,75	Rp 1.299.844,75
3	Kolom lt.1	0,72	m3	Rp 1.010.016,0	Rp 56.421,00	Rp 1.066.437,00
4	Ring balk	0,431	m3	Rp 368.568,0	Rp 405.290,85	Rp 773.858,85
	TOTAL			Rp 2.779.430,40	Rp 1.172.303,00	Rp 3.951.733,40



BILL OF QUANTITY
Bekisting Cara Tradisional Rumah Tinggal 2 Lantai

No.	Uraian Pekerjaan	Volume	Satuan
	Bangunan 2 lantai		
	Pembetonan		
1	<u>Pondasi</u>		
	Footing	0,864	m3
	Pedestal	0,384	m3
2	<u>Sloof</u>	1,0775	m3
3	<u>Kolom lt.1</u>	1,44	m3
4	<u>Balok</u>	1,293	m3
5	<u>Kolom lt.2</u>	0,72	m3
6	<u>Ring balk</u>	0,431	m3
	Bekisting		
a.	<u>Bekisting pondasi</u>		
	Footing	0,48	m2
	Pedestal	0,64	m2
b.	<u>Bekisting sloof</u>	21,55	m2
c.	<u>Bekisting kolom lt.1</u>	2,4	m2
d.	<u>Bekisting balok</u>	25,86	m2
e.	<u>Bekisting kolom lt.2</u>	1,2	m2
f.	<u>Bekisting ring balk</u>	8,62	m2

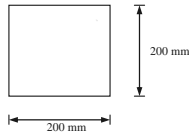
BACK UP PERHITUNGAN MATERIAL DAN ALAT

Metode Cara Tradisional

Pondasi Setempat

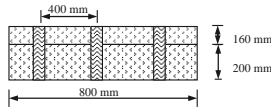
n = 12

Pedestal



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
200	200	160	800

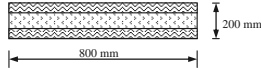
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	2000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

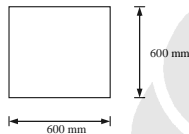
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	360
1	100	800	

Sisi 2 dan 4



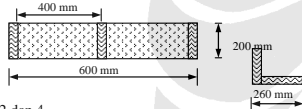
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	2
			800

Footing



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
600	600	100	200

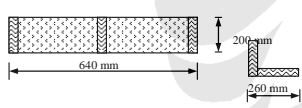
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	600	3
			200
			3
			200

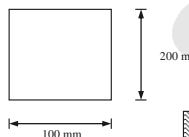
Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	640	3
			200
			3
			200

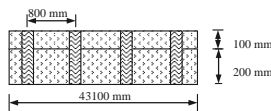
Sloof

n = 1



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	200	0	43100

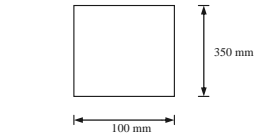
Sisi 1 dan 3



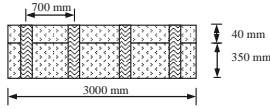
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	43100	55
			200 m'
			55
			200 m'

Kolom lt 1 n = 12



Sisi 1 dan 3

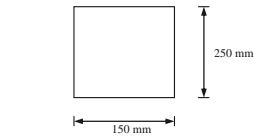


Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	400	40	3000

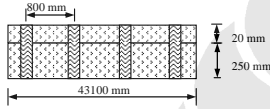
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	350	3000	6
1	40	3000	450

Balak = 3 m n = 1



Sisi 1 dan 3

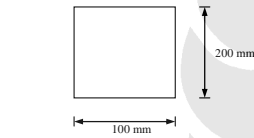


Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	300	20	43100

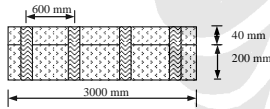
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	250	43100	55
1	100	43100	320

Kolom lt2 n = 12



Sisi 1 dan 3

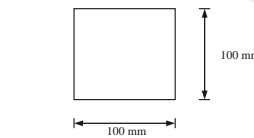


Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	200	40	3000

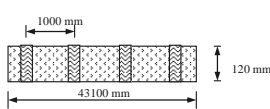
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	3000	6
1	40	3000	450

Ring balok = 3 m n = 1



Sisi 1 dan 3



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
100	100	20	43100

Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	120	43100	45
			120

Daftar Kebutuhan Material

Ukuran Papan 2/20 (mm ²)=	0.02	x	0.2	x	2 mm
Ukuran Kaso 4/6 (mm ²) =	0.04	x	0.06	x	4 mm
Ukuran Kaso 5/7 (mm ²) =	0.05	x	0.07	x	4 mm
Ukuran Balok 8/12 (mm ²) =	0.08	x	0.12	x	4 mm

No.	Uraian	n	Jml papan	Ukuran Papan		Luas Total	Jml Papan (lbr)	Jml Kaso	Ukuran Kaso P (m)	Panjang Total P (m)	Volume Kaso (m ³)
				L (m)	P (m)						
1	Pondasi Setempat										
	<u>Pedestal</u>										
	Sisi 1 dan 3	12	1	0.2	0.8	1.92	2.4	3	0.36	12.96	0.031104
	Sisi 2 dan 4	12	1	0.1	0.8	0.96	1.2				
	Sisi 2 dan 4	12	1	0.2	0.8	1.92	2.4	2	0.8	19.2	0.04608
	<u>Footing</u>										
	Sisi 1 dan 3	12	1	0.2	0.6	1.44	1.8	3	0.2	7.2	0.01728
	Sisi 2 dan 4	12	1	0.2	0.64	1.536	1.92	3	0.2	7.2	0.01728
	Sisi 2 dan 4	12	1	0.2	0.64	1.536	1.92	3	0.2	7.2	0.01728
	Sisi 2 dan 4	12	1	0.2	0.64	1.536	1.92	3	0.2	7.2	0.01728
	TOTAL					7,776	9,72			60,96	0,146304
2	Sloof 3 m										
	Sisi 1 dan 3	1	1	0.2	43.1	8.62	10.775	55	0.2	11	0.0264
	Sisi 1 dan 3	1	1	0.2	43.1	8.62	10.775	55	0.2	0	0
	TOTAL					8,62	10,775			11	0,0264
3	Kolom lt.1										
	Sisi 1 dan 3	12	1	0.35	3	12.6	15.75	6	0.45	32.4	0.07776
	Sisi 1 dan 3	12	1	0.04	3	1.44	1.8				
	TOTAL					14,04	17,55			32,4	0,07776
4	Balok = 3 m										
	Sisi 1 dan 3	1	1	0.25	43.1	10.775	13.46875	55	0.32	17.6	0.04224
	Sisi 1 dan 3	1	1	0.1	43.1	4.31	5.3875				
	TOTAL					15,085	18,85625			17,6	0,04224
5	Kolom lt.2										
	Sisi 1 dan 3	12	1	0.2	3	7.2	9	6	0.45	32.4	0.07776
	Sisi 1 dan 3	12	1	0.04	3	1.44	1.8				
	TOTAL					8,64	10,8			32,4	0,07776
6	Ring balok = 3 m										
	Sisi 1 dan 3	1	1	0.12	43.1	5.172	6.465	45	0.12	5.4	0.01296
	TOTAL					5,172	6,465			5,4	0,01296
	TOTAL					118,666		Kaso 4/6 =		319,52	0,766848

DAFTAR HARGA MATERIAL

NO	URAIAN	SATUAN	HARGA SATUAN
	Papan Randu 2/20	lbr	Rp 48.000,00
	Kaso 4/6	m3	Rp 2.100.000,00
	Kaso 5/7	m3	Rp 2.100.000,00
	Balok 8/12	m3	Rp 2.100.000,00
	Paku	kg	Rp 8.000,00
	Minyak Bekisting	ltr	Rp 2.500,00

Biaya Kebutuhan Material Untuk Bekisting

No.	Uraian	Luas Pembetonan	Volume	Satuan	Harga Satuan	Total
1	Pondasi Setempat	1,12				
	Papan Randu 2/20		9,72	lbr	Rp 48.000,00	Rp 466.560,00
	Kaso 4/6		0,146304	m3	Rp 2.100.000,00	Rp 307.238,40
	Paku		0,336	kg	Rp 8.000,00	Rp 2.688,00
	Minyak Bekisting		0,224	ltr	Rp 2.500,00	Rp 560,00
2	Sloof	21,55				
	Papan Randu 2/20		10,775	lbr	Rp 48.000,00	Rp 517.200,00
	Kaso 4/6		0,0264	m3	Rp 2.100.000,00	Rp 55.440,00
	Paku		6,465	kg	Rp 8.000,00	Rp 51.720,00
	Minyak Bekisting		4,31	ltr	Rp 2.500,00	Rp 10.775,00
3	Kolom H.1	2,4				
	Papan Randu 2/20		17,55	lbr	Rp 48.000,00	Rp 842.400,00
	Kaso 4/6		0,07776	m3	Rp 2.100.000,00	Rp 163.296,00
	Paku		0,72	kg	Rp 8.000,00	Rp 5.760,00
	Minyak Bekisting		0,48	ltr	Rp 2.500,00	Rp 1.200,00
4	Balok	25,86				
	Papan Randu 2/20		18,85625	lbr	Rp 48.000,00	Rp 905.100,00
	Kaso 4/6		0,04224	m3	Rp 2.100.000,00	Rp 88.704,00
	Paku		7,758	kg	Rp 8.000,00	Rp 62.064,00
	Minyak Bekisting		5,172	ltr	Rp 2.500,00	Rp 12.930,00
5	Kolom H.2	1,2				
	Papan Randu 2/20		10,8	lbr	Rp 48.000,00	Rp 518.400,00
	Kaso 4/6		0,07776	m3	Rp 2.100.000,00	Rp 163.296,00
	Paku		0,36	kg	Rp 8.000,00	Rp 2.880,00
	Minyak Bekisting		0,24	ltr	Rp 2.500,00	Rp 600,00
6	Ring balok	8,62				
	Papan Randu 2/20		6,465	lbr	Rp 48.000,00	Rp 310.320,00
	Kaso 4/6		0,01296	m3	Rp 2.100.000,00	Rp 27.216,00
	Paku		2,586	kg	Rp 8.000,00	Rp 20.688,00
	Minyak Bekisting		1,724	ltr	Rp 2.500,00	Rp 4.310,00
	TOTAL					Rp 4.541.345,40

DAFTAR HARGA UPAH

NO	URAIAN	KOEFISIEN	SATUAN	HARGA SATUAN
	Pekerja	0,3300	hari	40000
	Mandor	0,0330	hari	55000
	Tukang Kayu	0,3200	hari	50000
	Kepala Tukang Kayu	0,0060	hari	55000

Biaya Kebutuhan Upah Untuk Bekisting

No.	Uraian	Volume pembedonan	Satuan	Koefisien	Volume total	Satuan	Harga Satuan/m2	Total
1	Pondasi Setempat	1,12	m2					
	Pekerja			0,33	0,3696	hari	40000	Rp 14.784,00
	Mandor			0,033	0,03696	hari	55000	Rp 2.032,80
	Tukang Kayu			0,32	0,3584	hari	50000	Rp 17.920,00
	Kepala Tukang Kayu			0,006	0,00672	hari	55000	Rp 369,60
2	Sloof	21,55	m2					
	Pekerja			0,33	7,1115	hari	40000	Rp 284.460,00
	Mandor			0,033	0,71115	hari	55000	Rp 39.113,25
	Tukang Kayu			0,32	6,896	hari	50000	Rp 344.800,00
	Kepala Tukang Kayu			0,006	0,1293	hari	55000	Rp 7.111,50
3	Kolom lt. 1	2,4	m2					
	Pekerja			0,33	0,792	hari	40000	Rp 31.680,00
	Mandor			0,033	0,0792	hari	55000	Rp 4.356,00
	Tukang Kayu			0,32	0,768	hari	50000	Rp 38.400,00
	Kepala Tukang Kayu			0,006	0,0144	hari	55000	Rp 792,00
4	Balok	25,86	m2					
	Pekerja			0,33	8,5338	hari	40000	Rp 341.352,00
	Mandor			0,033	0,85338	hari	55000	Rp 46.935,90
	Tukang Kayu			0,32	8,2752	hari	50000	Rp 413.760,00
	Kepala Tukang Kayu			0,006	0,15516	hari	55000	Rp 8.533,80
5	Kolom lt. 2	1,2	m2					
	Pekerja			0,33	0,396	hari	40000	Rp 15.840,00
	Mandor			0,033	0,0396	hari	55000	Rp 2.178,00
	Tukang Kayu			0,32	0,384	hari	50000	Rp 19.200,00
	Kepala Tukang Kayu			0,006	0,0072	hari	55000	Rp 396,00
6	Ring balok	8,62	m2					
	Pekerja			0,33	2,8446	hari	40000	Rp 113.784,00
	Mandor			0,033	0,28446	hari	55000	Rp 15.645,30
	Tukang Kayu			0,32	2,7584	hari	50000	Rp 137.920,00
	Kepala Tukang Kayu			0,006	0,05172	hari	55000	Rp 2.844,60
	TOTAL							Rp 1.904.208,75

Biaya Pekerjaan Bekisting

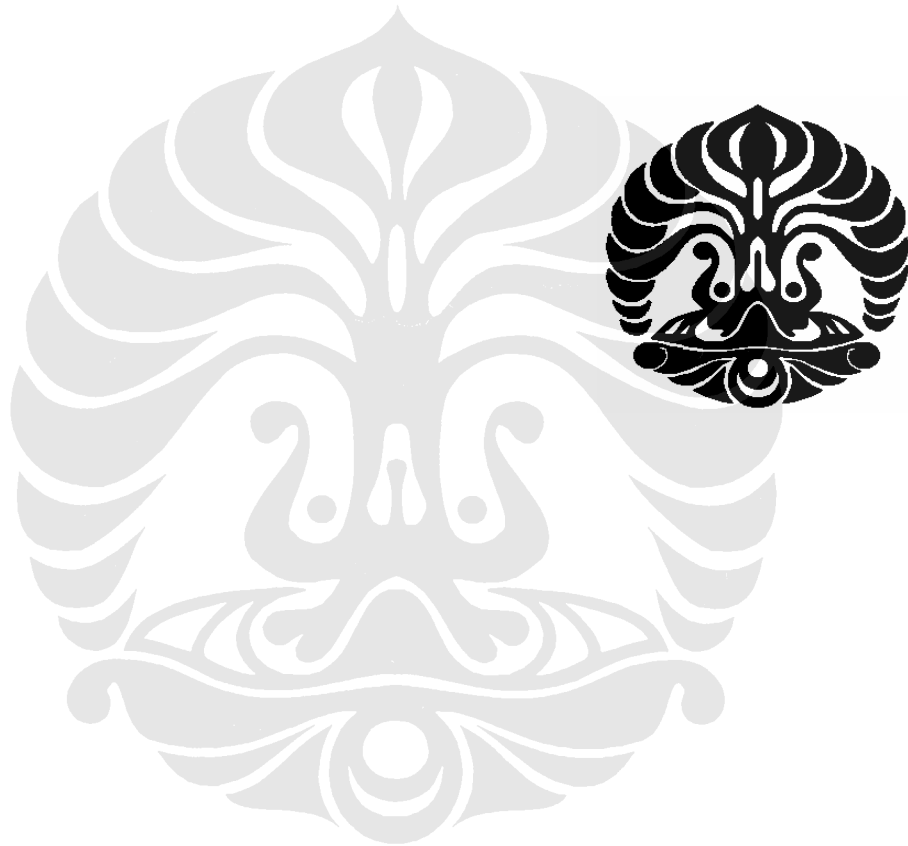
1 rumah tinggal 1 kali pakai

No.	Uraian	Volume pembedonan	Satuan	Harga Material	Harga Upah	Total
1	Pondasi	1,248	m3	Rp 776.486,4	Rp 35.106,40	Rp 811.592,80
2	Sloof	1,0775	m3	Rp 624.360,0	Rp 675.484,75	Rp 1.299.844,75
3	Kolom lt.1	1,44	m3	Rp 1.011.456,0	Rp 75.228,00	Rp 1.086.684,00
4	Balok	1,293	m3	Rp 1.055.868,0	Rp 810.581,70	Rp 1.866.449,70
5	Kolom lt.2	0,72	m3	Rp 684.576,0	Rp 37.614,00	Rp 722.190,00
6	Ring balk	0,431	m3	Rp 358.224,0	Rp 270.193,90	Rp 628.417,90
	TOTAL			Rp 4.510.970,40	Rp 1.904.208,75	Rp 6.415.179,15



LAMPIRAN D2

Analisa Biaya Bekisting Baja (Pondasi, Sloof, Kolom, Balok dan Ring Balok)

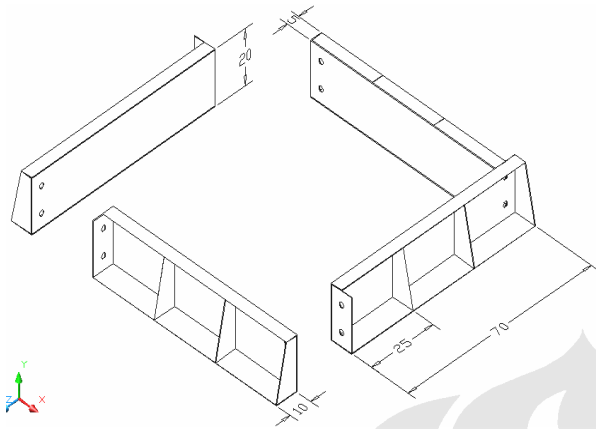


BILL OF QUANTITY
Bekisting Rumah Tinggal 1 Lantai dengan Material Baja

No.	Uraian Pekerjaan	Volume	Satuan
	Pembetonan		
1	<u>Pondasi</u>		
	Footing	0,864	m3
	Pedestal	0,384	m3
2	<u>Sloof</u>	1,293	m3
3	<u>Kolom lt.1</u>	1,44	m3
6	<u>Ring balk</u>	0,96975	m3
	Bekisting		
a.	<u>Bekisting pondasi</u>		
	Footing	0,48	m2
	Pedestal	0,64	m2
b.	<u>Bekisting sloof</u>	17,24	m2
c.	<u>Bekisting kolom lt.1</u>	2,4	m2
f.	<u>Bekisting ring balk</u>	19,395	m2

Pondasi Setempat

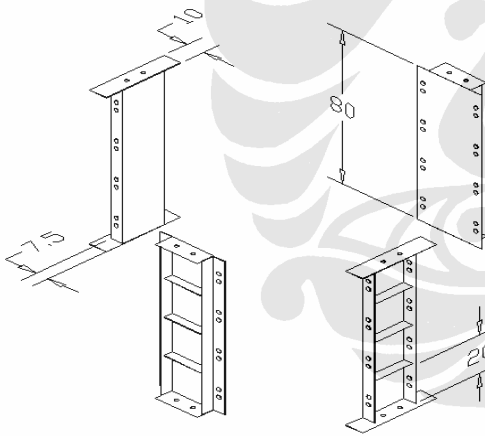
Footing



Plat Baja

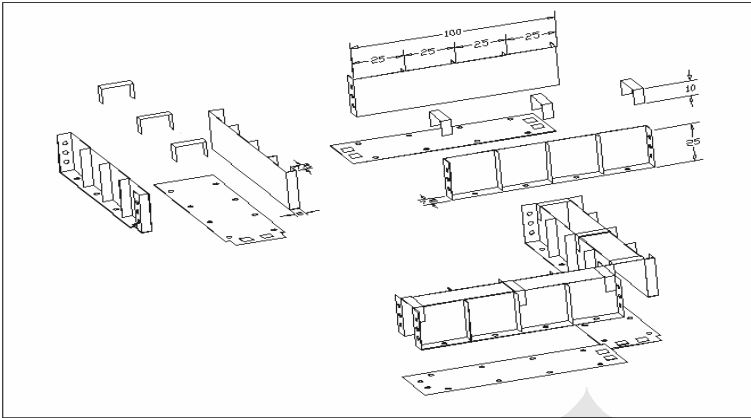
	n	tebal	panjang	lebar	volume	berat
kontak pipi	4	0,003	0,7	0,2	0,00168	13,188 kg
rangka pipi vert.1	12	0,002	0,2	0,075	0,00036	2,826 kg
rangka pipi vert.2	4	0,002	0,2	0,1	0,00016	1,256 kg
rangka pipi horz.1	4	0,002	0,7	0,1	0,00056	4,396 kg
rangka pipi horz.2	4	0,002	0,7	0,05	0,00028	2,198 kg
Jumlah Baut	8	bh				23,864 kg

Pedestal



	n	tebal	panjang	lebar	volume	berat
kontak pipi	4	0,003	0,8	0,35	0,00336	26,376 kg
rangka pipi vert.1	8	0,002	0,8	0,075	0,00096	7,536 kg
rangka pipi horz.1	16	0,002	0,2	0,05	0,00032	2,512 kg
rangka pipi horz.2	8	0,002	0,4	0,1	0,00064	5,024 kg
Jumlah Baut	40	bh				41,448 kg

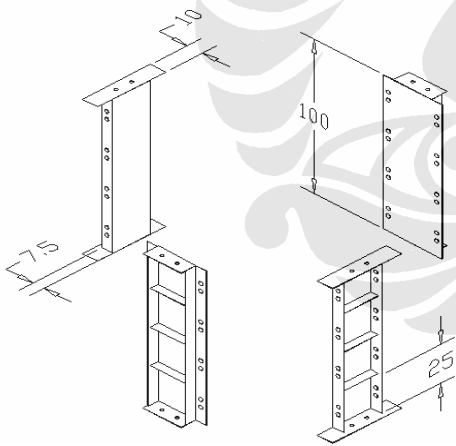
Sloof



Balok/m2

Plat Baja						
	n	tebal	png	lebar	volume	berat
kontak pipi	2	0,003	1	0,25	0,0015	11,775 kg
kontak alas	1	0,003	1	0,4	0,0012	9,42 kg
rangka pipi vert.1	6	0,002	0,25	0,05	0,00015	1,1775 kg
rangka pipi vert.2	4	0,002	0,25	0,1	0,0002	1,57 kg
rangka pipi horz.1	2	0,002	1	0,1	0,0004	3,14 kg
Pengikat pipi	3	0,002	0,35	0,05	0,000105	0,82425 kg
						27,90675 kg
Jumlah Baut	14	bh				
Panjang Sloof	43,1	m'				

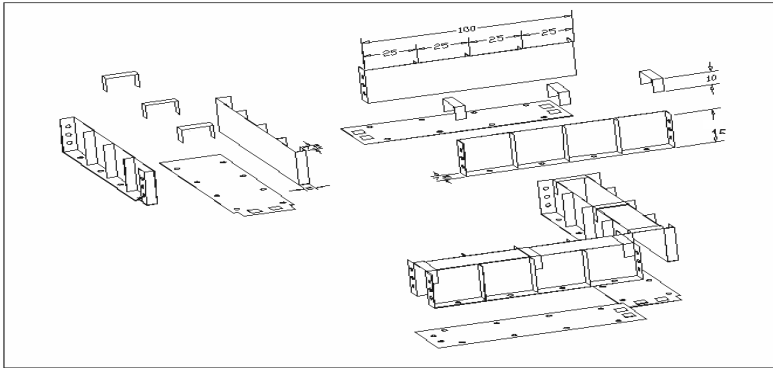
Kolom



Kolom / m2

Plat Baja						
	n	tebal	png	lebar	volume	berat
kontak pipi	4	0,003	1	0,35	0,0042	32,97 kg
rangka pipi vert.1	8	0,002	1	0,075	0,0012	9,42 kg
rangka pipi horz.1	16	0,002	0,2	0,05	0,00032	2,512 kg
rangka pipi horz.2	8	0,002	0,4	0,1	0,00064	5,024 kg
						49,926 kg
Jumlah Baut	40	bh				
Tinggi Kolom	3	m'				

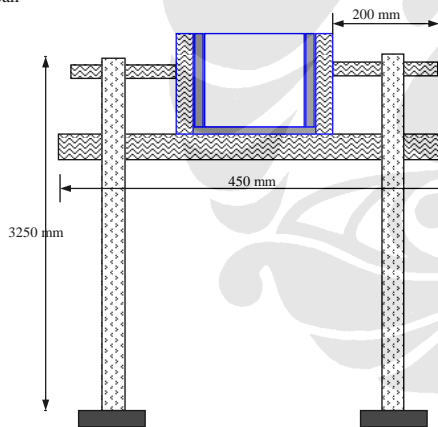
Ring balok



Ring Balok/m2

Plat Baja		n	tebal	pjpg	lebar	volume	berat
kontak pipi		2	0,003	1	0,15	0,0009	7,065 kg
kontak alas		1	0,003	1	0,4	0,0012	9,42 kg
rangka pipi vert.1		6	0,002	0,15	0,05	0,00009	0,7065 kg
rangka pipi vert.2		4	0,002	0,15	0,1	0,00012	0,942 kg
rangka pipi horz.1		2	0,002	1	0,1	0,0004	3,14 kg
Pengikat pipi		3	0,002	0,35	0,05	0,000105	0,82425 kg
Jumlah Baut		14	bh				22,09775 kg
Kaso Alas 4/6		2	0,04	0,06	1	0,0048 m3	
Panjang Ring Balok		43,1	m'				

Perancah



n	=	72
	Jumlah	Panjang
Kaso 5/7	144	3,25 m
	72	0,45 m
Balok 8/12	2	43,1 m

Rekap kebutuhan Material

No.	Uraian	Plat Baja	Satuan	Mur Baut	Satuan
1	Pondasi Setempat				
	<u>Pedestal</u>	286,368	kg	8	bh
	<u>Footing</u>	497,376	kg	40	bh
2	Sloof 3 m	1202,781	kg	603,4	bh
3	Kolom lt.1	1797,336	kg	480	bh
6	Ring balok = 3 m	952,413	kg	603,4	bh
	TOTAL	4736,274	kg	1734,800	bh

No.	Uraian	Jml Kaso 5/7	Panjang Kaso	Panjang Total	Volume Kaso
	Perancah Ring Balk	144	3,25	468	1,638
		72	0,45	32,4	0,1134
	TOTAL	Kaso 5/7 =		500,4	1,7514

Uraian	Jml Balok 8/12	Panjang Balok	Panjang Total	Volume balok
Perancah Ring balok	2	43,1	86,2	0,82752
TOTAL	Balok 8/12 =		86,2	0,82752

DAFTAR HARGA MATERIAL

NO	URAIAN	SATUAN	HARGA SATUAN
	Baja BJ 37	kg	Rp 9.000,00
	Baut 12 mm	bh	Rp 5.000,00
	Minyak Bekisting	litr	Rp 2.500,00

Biaya Kebutuhan Material Untuk Bekisting

No.	Uraian	Luas Pembetonan	Satuan	Volume	Satuan	Harga Satuan	Total
1	Pondasi Setempat	1,12	m2				
	Baja BJ 37			783,744	kg	Rp 9.000,00	Rp 7.053.696,00
	Baut 12 mm			48	bh	Rp 5.000,00	Rp 240.000,00
	Minyak Bekisting			0,224	litr	Rp 2.500,00	Rp 560,00
2	Sloof	17,24	m2				
	Baja BJ 37			1202,780925	kg	Rp 9.000,00	Rp 10.825.028,33
	Baut 12 mm			603,4	bh	Rp 5.000,00	Rp 3.017.000,00
	Minyak Bekisting			3,448	litr	Rp 2.500,00	Rp 8.620,00
3	Kolom lt.1	2,4	m2				
	Baja BJ 37			1797,336	kg	Rp 9.000,00	Rp 16.176.024,00
	Baut 12 mm			480	bh	Rp 5.000,00	Rp 2.400.000,00
	Minyak Bekisting			0,48	litr	Rp 2.500,00	Rp 1.200,00
6	Ring balok	19,395	m2				
	Baja BJ 37			952,413025	kg	Rp 9.000,00	Rp 8.571.717,23
	Baut 12 mm			603,4	bh	Rp 5.000,00	Rp 3.017.000,00
	Minyak Bekisting			3,879	litr	Rp 2.500,00	Rp 9.697,50
	TOTAL						Rp 51.320.543,05

Biaya Kebutuhan Material Untuk Perancah

No.	Uraian	Volume	Satuan	Volume / n	Satuan	Harga Satuan	Total
	Ring balok						
	Kaso 5/7	1,7514	m2	0,35028	m3	Rp 2.100.000,00	Rp 735.588,00
	Balok 8/12	0,82752	m2	0,082752	m3	Rp 2.100.000,00	Rp 173.779,20
	TOTAL						Rp 909.367,20

DAFTAR HARGA MATERIAL

NO	URAIAN	KOEFISIEN	SATUAN	HARGA SATUAN
	Pekerja	1,2000	hari	40000
	Tukang Kayu	1,2000	hari	50000
	Kepala Tukang Kayu	0,1200	hari	55000

Biaya Kebutuhan Upah Untuk Bekisting

No.	Uraian	Volume pembedonan	Satuan	Koefisien	Volume total	Satuan	Harga Satuan/m2	Total
1	Pondasi Setempat	1,12	m2					
	Pekerja			1,2	1,344	hari	40000	Rp 53.760,00
	Tukang Kayu			1,2	1,344	hari	50000	Rp 67.200,00
	Kepala Tukang Kayu			0,12	0,1344	hari	55000	Rp 7.392,00
2	Sloof	17,24	m2					
	Pekerja			1,2	20,688	hari	40000	Rp 827.520,00
	Tukang Kayu			1,2	20,688	hari	50000	Rp 1.034.400,00
	Kepala Tukang Kayu			0,12	2,0688	hari	55000	Rp 113.784,00
3	Kolom lt. 1	2,4	m2					
	Pekerja			1,2	2,88	hari	40000	Rp 115.200,00
	Tukang Kayu			1,2	2,88	hari	50000	Rp 144.000,00
	Kepala Tukang Kayu			0,12	0,288	hari	55000	Rp 15.840,00
6	Ring balok	19,395	m2					
	Pekerja			1,2	23,274	hari	40000	Rp 930.960,00
	Tukang Kayu			1,2	23,274	hari	50000	Rp 1.163.700,00
	Kepala Tukang Kayu			0,12	2,3274	hari	55000	Rp 128.007,00
	TOTAL							Rp 4.601.763,00

Biaya Pekerjaan Bekisting Baja untuk RT 1 lantai
1 rumah tinggal 1 kali pakai

No.	Uraian	Volume pembetonan	Satuan	Harga Material	Harga Upah	Total
1	Pondasi	1,248	m3	Rp 7.294.256,0	Rp 128.352,00	Rp 7.422.608,00
2	Sloof	1,293	m3	Rp 13.850.648,3	Rp 1.975.704,00	Rp 15.826.352,33
3	Kolom lt.1	1,44	m3	Rp 18.577.224,0	Rp 275.040,00	Rp 18.852.264,00
6	Ring balk	0,96975	m3	Rp 11.598.414,7	Rp 2.222.667,00	Rp 13.821.081,73
	Perancah			Rp 735.588,0		
7	Pabrikasi	4736,27	kg	Rp 7.104.410,9		Rp 7.104.410,93
	TOTAL			Rp 59.160.541,98	Rp 4.601.763,00	Rp 63.026.716,98

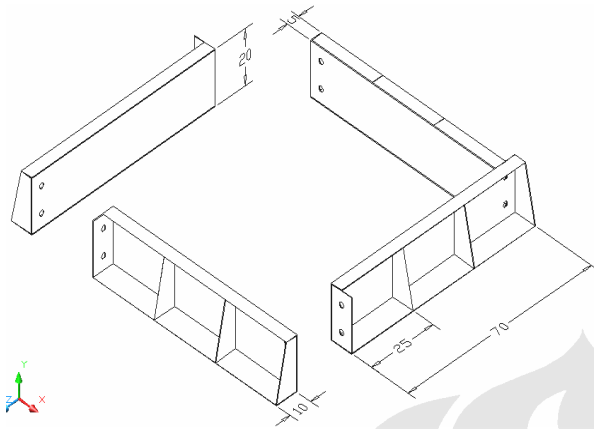


BILL OF QUANTITY
Bekisting Rumah Tinggal 2 Lantai dengan Material Baja

No.	Uraian Pekerjaan	lume pembeton	Volume	Satuan
	Pembetonan	n		
1	<u>Pondasi</u>			
	Footing	12	0,864	m3
	Pedestal	12	0,384	m3
2	<u>Sloof</u>	1	1,293	m3
3	<u>Kolom lt.1</u>	12	1,44	m3
4	<u>Balok</u>	1	1,293	m3
5	<u>Kolom lantai 2</u>	12	1,44	m3
6	<u>Ring balk</u>	1	0,96975	m3
	Bekisting	n		
a.	<u>Bekisting pondasi</u>			
	Footing	12	0,48	m2
	Pedestal	12	0,64	m2
b.	<u>Bekisting sloof</u>	1	17,24	m2
c.	<u>Bekisting kolom lt.1</u>	12	2,4	m2
d.	<u>Bekisting balok</u>	1	23,705	m2
e.	<u>Bekisting kolom lantai 2</u>	12	2,4	m2
f.	<u>Bekisting ring balk</u>	1	19,395	m2

Pondasi Setempat

Footin

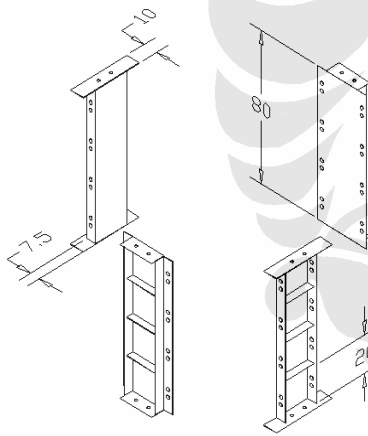


Plat Baja

	n	tebal	pjng	lebar	volume	berat
lantak pi	4	0,003	0,7	0,2	0,00168	13,188 kg
ka pipi v	12	0,002	0,2	0,075	0,00036	2,826 kg
ka pipi v	4	0,002	0,2	0,1	0,00016	1,256 kg
sa pipi t	4	0,002	0,7	0,1	0,00056	4,396 kg
sa pipi t	4	0,002	0,7	0,05	0,00028	2,198 kg
						23,864 kg

mlah B: 8 bh

Pedestal

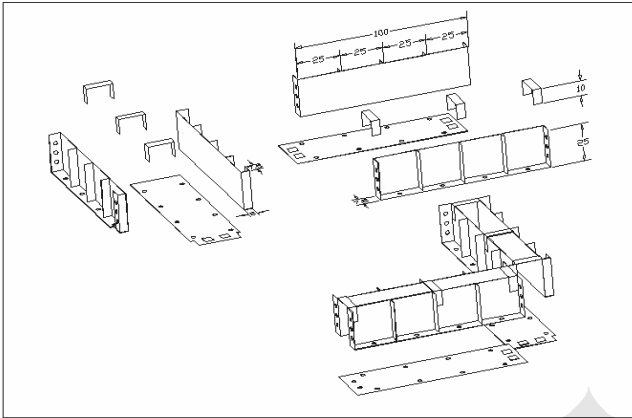


Plat Baja

	n	tebal	pjng	lebar	volume	berat
lantak pi	4	0,003	0,8	0,35	0,00336	26,376 kg
ka pipi v	8	0,002	0,8	0,075	0,00096	7,536 kg
sa pipi t	16	0,002	0,2	0,05	0,00032	2,512 kg
sa pipi t	8	0,002	0,4	0,1	0,00064	5,024 kg
						41,448 kg

mlah B: 40 bh

Sloof & Balok

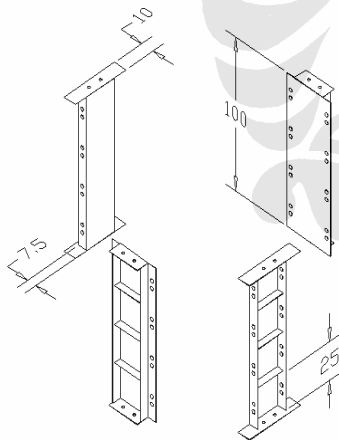


balok/m

Plat Baja

	n	tebal	panjang	lebar	volume	berat
rantai pi	2	0,003	1	0,25	0,0015	11,775 kg
rantai al	1	0,003	1	0,4	0,0012	9,42 kg
ka pipi v	6	0,002	0,25	0,05	0,00015	1,1775 kg
ka pipi v	4	0,002	0,25	0,1	0,0002	1,57 kg
sa pipi t	2	0,002	1	0,1	0,0004	3,14 kg
ngikat t	3	0,002	0,35	0,05	0,000105	0,82425 kg
						27,90675 kg
mlah Bc	14	bh				
panjang Sl	43,1	m'				
panjang Ba	43,1	m'				

Kolom

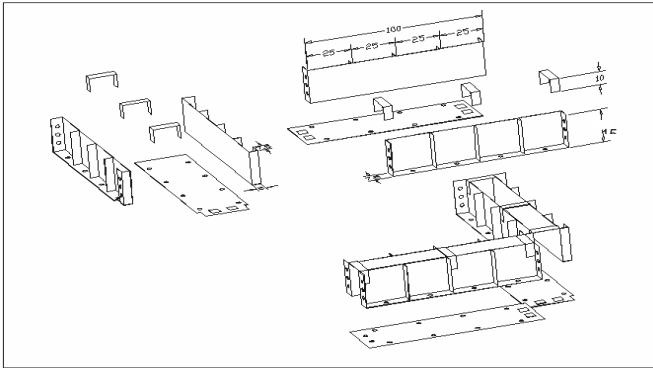


kolom / t

Plat Baja

	n	tebal	panjang	lebar	volume	berat
rantai pi	4	0,003	1	0,35	0,0042	32,97 kg
ka pipi v	8	0,002	1	0,075	0,0012	9,42 kg
sa pipi t	16	0,002	0,2	0,05	0,00032	2,512 kg
sa pipi t	8	0,002	0,4	0,1	0,00064	5,024 kg
						49,926 kg
mlah Bc	40	bh				
inggi Kol	3	m'				

Ring balok = 3 m



g Balok

Plat Baja

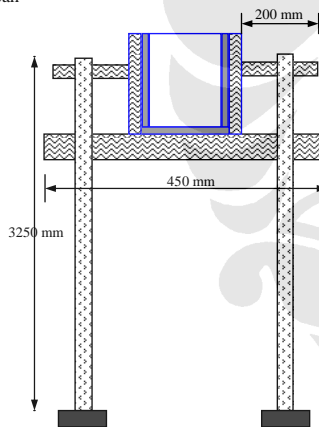
	n	tebal	pnjng	lebar	volume	berat
ontak pi	2	0,003	1	0,15	0,0009	7,065 kg
ontak al	1	0,003	1	0,4	0,0012	9,42 kg
ka pipi v	6	0,002	0,15	0,05	0,00009	0,7065 kg
ka pipi v	4	0,002	0,15	0,1	0,00012	0,942 kg
ca pipi f	2	0,002	1	0,1	0,0004	3,14 kg
ngikat f	3	0,002	0,35	0,05	0,000105	0,82425 kg
						22,09775 kg

mlah B:

so Alas :

ng Ring

Perancah



n	Jumlah	Panjang
Kaso 5/7	144	3,25 m
	72	0,45 m
alok 8/1	2	43,1 m

Rekap kebutuhan Material

No.	Uraian	Plat Baja	Satuan	Mur Baut	Satuan
1	Pondasi Setempat				
	<u>Pedestal</u>	286,368	kg	8	bh
	<u>Footing</u>	497,376	kg	40	bh
2	Sloof 3 m	1202,781	kg	603,4	bh
3	Kolom lt.1	1797,336	kg	480	bh
4	Balok = 3 m	1202,781	kg	603,4	bh
5	Kolom lt.2	1797,336	kg	480	bh
6	Ring balok = 3 m	952,413	kg	603,4	bh
	TOTAL	7736,391	kg	2818,200	bh

No.	Uraian	Jml Kaso 5/7	Panjang Kaso	Panjang Total	Volume Kaso
	Perancah Balok	144	3,25	468	1,638
		72	0,45	32,4	0,1134
	Perancah Ring Balk	144	3,25	468	1,638
		72	0,45	32,4	0,1134
	TOTAL	Kaso 5/7 =		500,4	3,5028

Uraian	Jml Balok 8/12	Panjang Balok	Panjang Total	Volume balok
Perancah Balok	2	43,1	86,2	0,82752
TOTAL	Balok 8/12 =		86,2	0,82752

DAFTAR HARGA MATERIAL

NO	URAIAN	SATUAN	HARGA SATUAN
Volume pembeconan			
	Baja BJ 37	kg	Rp 9.000,00
	Baut 12 mm	bh	Rp 5.000,00
	Minyak Bekisting	lir	Rp 2.500,00

Biaya Kebutuhan Material Untuk Bekisting

No.	Uraian	Luas Pembetonan	Satuan	Volume	Satuan	Harga Satuan	Total
1	Pondasi Setempat	1,12	m2				
	Baja BJ 37			783,744	kg	Rp 9.000,00	Rp 7.053.696,00
	Baut 12 mm			48	bh	Rp 5.000,00	Rp 240.000,00
	Minyak Bekisting			0,224	lir	Rp 2.500,00	Rp 560,00
2	Sloof	17,24	m2				
	Baja BJ 37			1202,780925	kg	Rp 9.000,00	Rp 10.825.028,33
	Baut 12 mm			603,4	bh	Rp 5.000,00	Rp 3.017.000,00
	Minyak Bekisting			3,448	lir	Rp 2.500,00	Rp 8.620,00
3	Kolom lt.1	2,4	m2				
	Baja BJ 37			1797,336	kg	Rp 9.000,00	Rp 16.176.024,00
	Baut 12 mm			480	bh	Rp 5.000,00	Rp 2.400.000,00
	Minyak Bekisting			0,48	lir	Rp 2.500,00	Rp 1.200,00
4	Balok	23,705	m2				
	Baja BJ 37			1202,780925	kg	Rp 9.000,00	Rp 10.825.028,33
	Baut 12 mm			603,4	bh	Rp 5.000,00	Rp 3.017.000,00
	Minyak Bekisting			4,741	lir	Rp 2.500,00	Rp 11.852,50
5	Kolom lt.2	2,4	m2				
	Baja BJ 37			1797,336	kg	Rp 9.000,00	Rp 16.176.024,00
	Baut 12 mm			480	bh	Rp 5.000,00	Rp 2.400.000,00
	Minyak Bekisting			0,48	lir	Rp 2.500,00	Rp 1.200,00
6	Ring balok	19,395	m2				
	Baja BJ 37			952,413025	kg	Rp 9.000,00	Rp 8.571.717,23
	Baut 12 mm			603,4	bh	Rp 5.000,00	Rp 3.017.000,00
	Minyak Bekisting			3,879	lir	Rp 2.500,00	Rp 9.697,50
	TOTAL						Rp 83.751.647,88

Biaya Kebutuhan Material Untuk Perancah

No.	Uraian	Volume	Satuan	Volume / n	Satuan	Harga Satuan	Total
	Balok						
	Kaso 5/7	3,5028	m2	0,70056	m3	Rp 2.100.000,00	Rp 1.471.176,00
	Balok 8/12	0,82752	m2	0,082752	m3	Rp 2.100.000,00	Rp 173.779,20
	Ring balok						
	Kaso 5/7	1,7514	m2	0,35028	m3	Rp 2.100.000,00	Rp 735.588,00
	TOTAL						Rp 2.380.543,20

DAFTAR HARGA MATERIAL

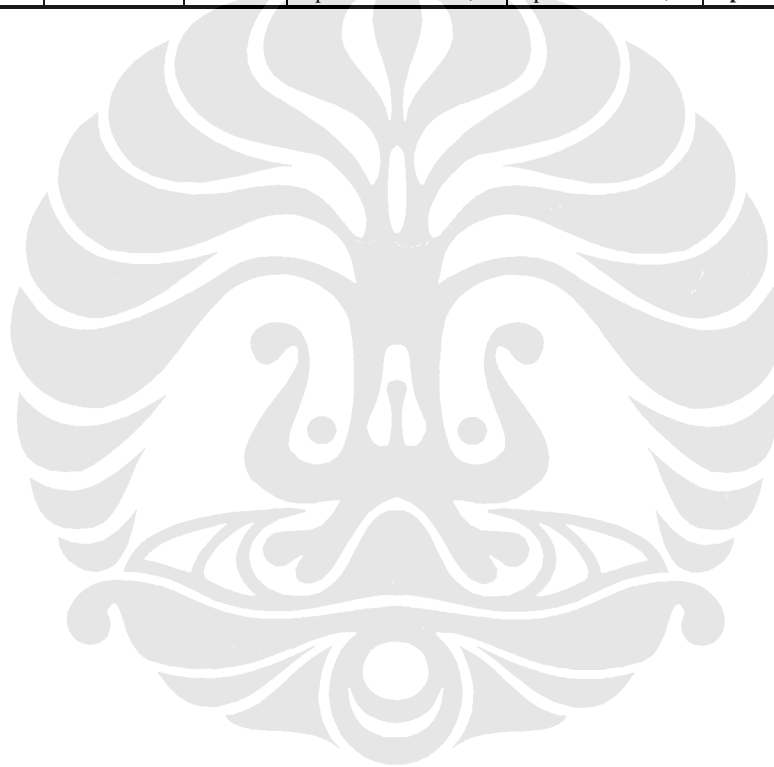
NO	URAIAN	KOEFISIEN	SATUAN	HARGA SATUAN
Volume pembetonan				
	Pekerja	1,2000	hari	40000
	Tukang Kayu	1,2000	hari	50000
	Kepala Tukang Kayu	0,1200	hari	55000

Biaya Kebutuhan Upah Untuk Bekisting

No.	Uraian	Volume pembetonan	Satuan	Koefisien	Volume total	Satuan	Harga Satuan/m2	Total
1	Pondasi Setempat	1,12	m2					
	Pekerja			1,2	1,344	hari	40000	Rp 53.760,00
	Tukang Kayu			1,2	1,344	hari	50000	Rp 67.200,00
	Kepala Tukang Kayu			0,12	0,1344	hari	55000	Rp 7.392,00
2	Sloof	17,24	m2					
	Pekerja			1,2	20,688	hari	40000	Rp 827.520,00
	Tukang Kayu			1,2	20,688	hari	50000	Rp 1.034.400,00
	Kepala Tukang Kayu			0,12	2,0688	hari	55000	Rp 113.784,00
3	Kolom lt. 1	2,4	m2					
	Pekerja			1,2	2,88	hari	40000	Rp 115.200,00
	Tukang Kayu			1,2	2,88	hari	50000	Rp 144.000,00
	Kepala Tukang Kayu			0,12	0,288	hari	55000	Rp 15.840,00
4	Balok	23,705	m2					
	Pekerja			1,2	28,446	hari	40000	Rp 1.137.840,00
	Tukang Kayu			1,2	28,446	hari	50000	Rp 1.422.300,00
	Kepala Tukang Kayu			0,12	2,8446	hari	55000	Rp 156.453,00
5	Kolom lt. 2	2,4	m2					
	Pekerja			1,2	2,88	hari	40000	Rp 115.200,00
	Tukang Kayu			1,2	2,88	hari	50000	Rp 144.000,00
	Kepala Tukang Kayu			0,12	0,288	hari	55000	Rp 15.840,00
6	Ring balok	19,395	m2					
	Pekerja			1,2	23,274	hari	40000	Rp 930.960,00
	Tukang Kayu			1,2	23,274	hari	50000	Rp 1.163.700,00
	Kepala Tukang Kayu			0,12	2,3274	hari	55000	Rp 128.007,00
	TOTAL							Rp 7.593.396,00

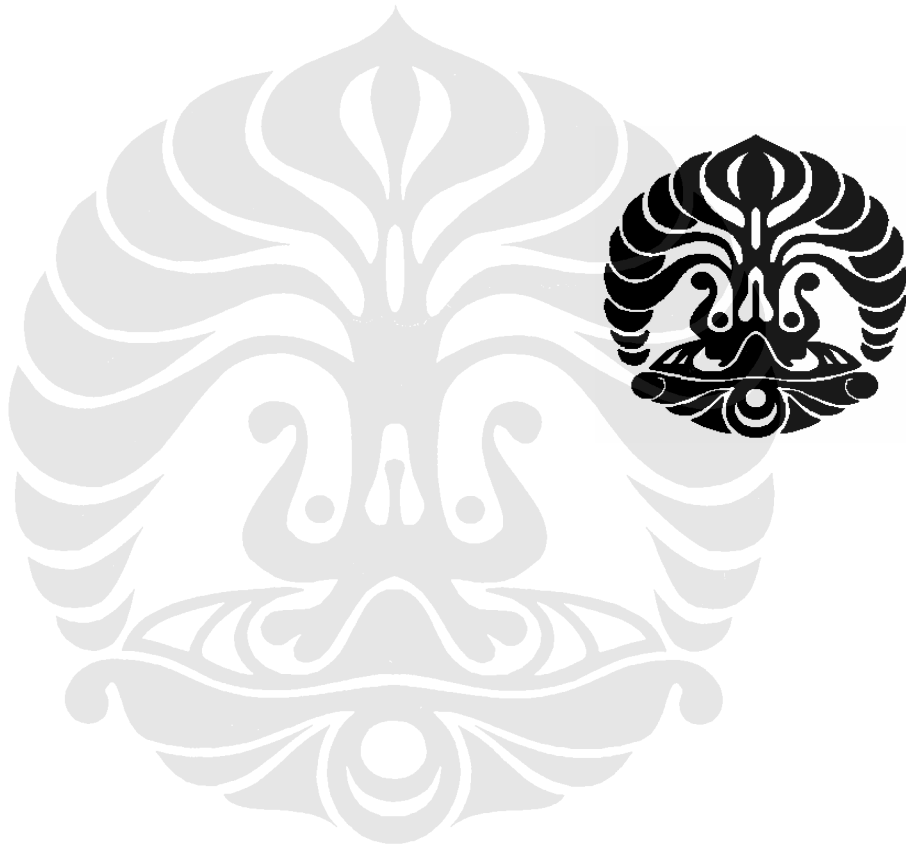
Biaya Pekerjaan Bekisting Baja untuk RT 2 Lantai
1 rumah tinggal 1 kali pakai

No.	Uraian	Volume pembetonan	Satuan	Harga Material	Harga Upah	Total
1	Pondasi	1,248	m3	Rp 7.294.256,0	Rp 128.352,00	Rp 7.422.608,00
2	Sloof	1,293	m3	Rp 13.850.648,3	Rp 1.975.704,00	Rp 15.826.352,33
3	Kolom lt.1	1,44	m3	Rp 18.577.224,0	Rp 275.040,00	Rp 18.852.264,00
4	Balok	1,293	m3	Rp 13.853.880,8	Rp 2.716.593,00	Rp 16.570.473,83
	Perancah			Rp 1.644.955,2		
5	Kolom lantai 2	1,44	m3	Rp 18.577.224,0	Rp 275.040,00	Rp 18.852.264,00
6	Ring balk	0,96975	m3	Rp 11.598.414,7	Rp 2.222.667,00	Rp 13.821.081,73
	Perancah			Rp 735.588,0		
7	Pabrikasi	7736,39	kg	Rp 11.604.586,3		Rp 11.604.586,31
	TOTAL			Rp 97.736.777,39	Rp 7.593.396,00	Rp 102.949.630,19



LAMPIRAN D3

Analisa Biaya Bekisting Kayu (Pondasi, Sloof, Kolom, Balok dan Ring Balok)



BILL OF QUANTITY
Bekisting Rumah Tinggal 1 Lantai dengan Material Kayu

No.	Uraian Pekerjaan	Volume	Satuan
	Pembetonan		
1	<u>Pondasi</u>		
	Footing	0,864	m3
	Pedestal	0,384	m3
2	<u>Sloof</u>	1,293	m3
3	<u>Kolom lt.1</u>	1,44	m3
4	<u>Ring balk</u>	0,96975	m3
	Bekisting		
a.	<u>Bekisting pondasi</u>		
	Footing	0,48	m2
	Pedestal	0,64	m2
b.	<u>Bekisting sloof</u>	17,24	m2
c.	<u>Bekisting kolom lt.1</u>	2,4	m2
d.	<u>Bekisting ring balk</u>	19,395	m2

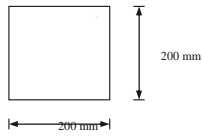
BACK UP PERHITUNGAN MATERIAL DAN ALAT

Metode Konvensional

Pondasi Setempat

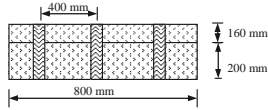
n = 12

Pedestal



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
200	200	160	800

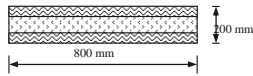
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	2000	mm
Ukuran Kaso 4/6 (mm ³) =	40	x	60	x	4000	mm

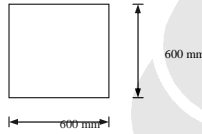
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	3
1	100	800	360

Sisi 2 dan 4



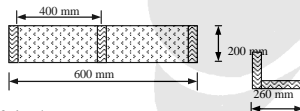
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	2
			800

Footing



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
600	600	100	200

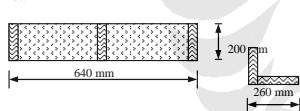
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm ³) =	40	x	60	x	4000	mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	600	3
			200
			200

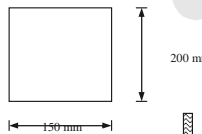
Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	640	3
			200
			200

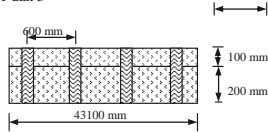
Sloof

n = 1



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
150	200	100	43100

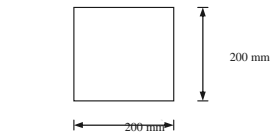
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm ³) =	40	x	60	x	4000	mm

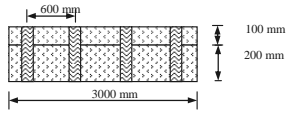
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	43100	73
1	100	43100	73
			300 m'
			200 m'

Kolom It 1 n = 12



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
200	200	100	3000

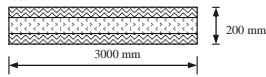
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

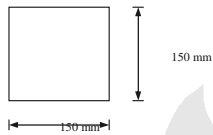
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso	
1	200	3000	6	300
1	100	3000		

Sisi 2 dan 4



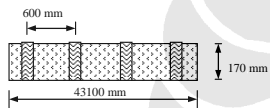
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso	
1	200	3000	2	3000

Ring balok = 3 m n = 1



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
150	150	20	43100

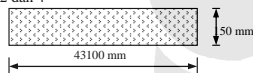
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

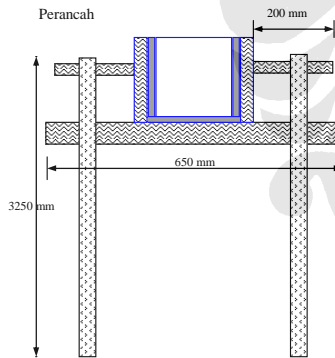
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso	
1	170	43100	73	170

Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso	
1	150	43100		

Perancah



n	=	73	
Jml Kaso 5/7	Ukuran Kaso	Jml Balok 8/12	Ukuran Balok
146	3250	73	650

Daftar Kebutuhan Material

Ukuran Papan 2/20 (mm ²)=	0.02	x	0.2	x	2 mm
Ukuran Kaso 4/6 (mm ²) =	0.04	x	0.06	x	4 mm
Ukuran Kaso 5/7 (mm ²) =	0.05	x	0.07	x	4 mm
Ukuran Balok 8/12 (mm ²) =	0.08	x	0.12	x	4 mm

No.	Uraian	n	Jml papan	Ukuran Papan		Luas Total	Jml Papan (lbr)	Jml Kaso	Ukuran Kaso		Panjang Total	Volume Kaso (m ³)
				L (m)	P (m)				P (m)	P (m)		
1	Pondasi Setempat											
	<i>Pedestal</i>											
	Sisi 1 dan 3	12	1	0.2	0.8	1,92	2,4	3	0.36		12,96	0,031104
		12	1	0.1	0.8	0,96	1,2					
	Sisi 2 dan 4	12	1	0.2	0.8	1,92	2,4	2	0.8		19,2	0,04608
	<i>Footing</i>											
	Sisi 1 dan 3	12	1	0.2	0.6	1,44	1,8	3	0.2		7,2	0,01728
		12						3	0.2		7,2	0,01728
	Sisi 2 dan 4	12	1	0.2	0.64	1,536	1,92	3	0.2		7,2	0,01728
		12						3	0.2		7,2	0,01728
	TOTAL					7,776	9,72				60,96	0,146304
2	Sloof 3 m											
	Sisi 1 dan 3	1	1	0.2	43.1	8.62	10,775	73	0.3		21,9	0,05256
		1	1	0.1	43.1	4.31	5,3875	73	0.2		14,6	0,03504
	TOTAL					12,93	16,1625				36,5	0,0876
3	Kolom lt.1											
	Sisi 1 dan 3	12	1	0.2	3	7.2	9	6	0.3		21,6	0,05184
		12	1	0.1	3	3.6	4,5					
	Sisi 2 dan 4	12	1	0.2	3	7.2	9	2	3		7,2	0,1728
	TOTAL					18	22,5				93,6	0,22464
4	Ring balok = 3 m											
	Sisi 1 dan 3	1	1	0.17	43.1	7.327	9.15875	73	0.17		12,41	0,029784
	Sisi 2 dan 4	1	1	0.15	43.1	6.465	8.08125					
	TOTAL					13,792	17,24				12,41	0,029784
	TOTAL					Papan 2/20 = 104,996				Kaso 4/6 = 406,94	0,976656	

No.	Uraian	Jumlah	Jml Kaso 5/7	Panjang Kaso	Panjang Total	Volume Kaso	Jml Balok 8/12	Panjang Balok	Panjang Total	Volume balok
	Perancah Ring Balok	1	146	3,25	474,5	1,66075	73	0,65	47,45	0,45552
	TOTAL				474,5	1,66075			47,45	0,45552
	TOTAL			Kaso 5/7 = 949		3,3215		Balok 8/12 = 94,9		0,91104

DAFTAR HARGA MATERIAL

NO	URAIAN	SATUAN	HARGA SATUAN
	Papan Randu 2/20	lbr	Rp 48.000,00
	Kaso 4/6	m3	Rp 2.100.000,00
	Kaso 5/7	m3	Rp 2.100.000,00
	Balok 8/12	m3	Rp 2.100.000,00
	Paku	kg	Rp 8.000,00
	Minyak Bekisting	ltr	Rp 2.500,00

Biaya Kebutuhan Material Untuk Bekisting

No.	Uraian	Luas Pembetonan	Volume	Satuan	Harga Satuan	Total
1	Pondasi Setempat	1,12				
	Papan Randu 2/20		9,72	lbr	Rp 48.000,00	Rp 466.560,00
	Kaso 4/6		0,146304	m3	Rp 2.100.000,00	Rp 307.238,40
	Paku		0,336	kg	Rp 8.000,00	Rp 2.688,00
	Minyak Bekisting		0,224	ltr	Rp 2.500,00	Rp 560,00
2	Sloof	17,24				
	Papan Randu 2/20		16,1625	lbr	Rp 48.000,00	Rp 775.800,00
	Kaso 4/6		0,0876	m3	Rp 2.100.000,00	Rp 183.960,00
	Paku		5,172	kg	Rp 8.000,00	Rp 41.376,00
	Minyak Bekisting		3,448	ltr	Rp 2.500,00	Rp 8.620,00
3	Kolom t.1	2,4				
	Papan Randu 2/20		22,5	lbr	Rp 48.000,00	Rp 1.080.000,00
	Kaso 4/6		0,22464	m3	Rp 2.100.000,00	Rp 471.744,00
	Paku		0,72	kg	Rp 8.000,00	Rp 5.760,00
	Minyak Bekisting		0,48	ltr	Rp 2.500,00	Rp 1.200,00
4	Ring balok	19,395				
	Papan Randu 2/20		17,24	lbr	Rp 48.000,00	Rp 827.520,00
	Kaso 4/6		0,029784	m3	Rp 2.100.000,00	Rp 62.546,40
	Paku		5,8185	kg	Rp 8.000,00	Rp 46.548,00
	Minyak Bekisting		3,879	ltr	Rp 2.500,00	Rp 9.697,50
	TOTAL					Rp 4.291.818,30

Biaya Kebutuhan Material Untuk Perancah

No.	Uraian	Volume	Volume / n	Satuan	Harga Satuan	Total
	Ring Balok 3 m					
	Kaso 5/7	1,66075	0,33215	m3	Rp 2.100.000,00	Rp 697.515,00
	Balok 8/12	0,45552	0,045552	m3	Rp 2.100.000,00	Rp 95.659,20
	TOTAL					Rp 793.174,20

DAFTAR HARGA UPAH

NO	URAIAN	KOEFISIEN	SATUAN	HARGA SATUAN
	Pekerja	0,3300	hari	40000
	Mandor	0,0330	hari	55000
	Tukang Kayu	0,3200	hari	50000
	Kepala Tukang Kayu	0,0060	hari	55000

Biaya Kebutuhan Upah Untuk Bekisting

No.	Uraian	Volume pembedonan	Satuan	Koefisien	Volume total	Satuan	Harga Satuan/m2	Total
1	Pondasi Setempat	1,12	m2					
	Pekerja			0,33	0,3696	hari	40000	Rp 14.784,00
	Mandor			0,033	0,03696	hari	55000	Rp 2.032,80
	Tukang Kayu			0,32	0,3584	hari	50000	Rp 17.920,00
	Kepala Tukang Kayu			0,006	0,00672	hari	55000	Rp 369,60
2	Sloof	17,24	m2					
	Pekerja			0,33	5,6892	hari	40000	Rp 227.568,00
	Mandor			0,033	0,56892	hari	55000	Rp 31.290,60
	Tukang Kayu			0,32	5,5168	hari	50000	Rp 275.840,00
	Kepala Tukang Kayu			0,006	0,10344	hari	55000	Rp 5.689,20
3	Kolom lt. 1	2,4	m2					
	Pekerja			0,33	0,792	hari	40000	Rp 31.680,00
	Mandor			0,033	0,0792	hari	55000	Rp 4.356,00
	Tukang Kayu			0,32	0,768	hari	50000	Rp 38.400,00
	Kepala Tukang Kayu			0,006	0,0144	hari	55000	Rp 792,00
4	Ring balok	19,395	m2					
	Pekerja			0,33	6,40035	hari	40000	Rp 256.014,00
	Mandor			0,033	0,640035	hari	55000	Rp 35.201,93
	Tukang Kayu			0,32	6,2064	hari	50000	Rp 310.320,00
	Kepala Tukang Kayu			0,006	0,11637	hari	55000	Rp 6.400,35
	TOTAL							Rp 1.258.658,48

Biaya Pekerjaan Bekisting Kayu untuk RT 1 Lantai

1 rumah tinggal 1 kali pakai

No.	Uraian	Volume pembedonan	Satuan	Harga Material	Harga Upah	Total
1	Pondasi	1,248	m3	Rp 776.486,4	Rp 35.106,40	Rp 811.592,80
2	Sloof	1,293	m3	Rp 1.001.136,0	Rp 540.387,80	Rp 1.541.523,80
3	Kolom lt.1	1,44	m3	Rp 1.557.504,0	Rp 75.228,00	Rp 1.632.732,00
4	Ring balk	0,96975	m3	Rp 1.729.788,6	Rp 607.936,28	Rp 2.337.724,88
	TOTAL			Rp 5.064.915,00	Rp 1.258.658,48	Rp 6.323.573,48



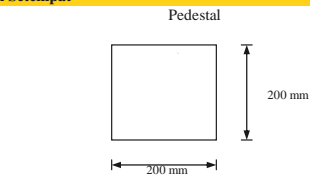
BILL OF QUANTITY
Bekisting Rumah Tinggal 2 Lantai dengan Material Kayu

No.	Uraian Pekerjaan	Volume	Satuan
	Bangunan 2 lantai		
	Pembetonan		
1	<u>Pondasi</u>		
	Footing	0,864	m3
	Pedestal	0,384	m3
2	<u>Sloof</u>	1,293	m3
3	<u>Kolom lt.1</u>	1,44	m3
4	<u>Balok</u>	1,61625	m3
5	<u>Kolom lt.2</u>	1,44	m3
6	<u>Ring balk</u>	0,96975	m3
	Bekisting		
a.	<u>Bekisting pondasi</u>		
	Footing	0,48	m2
	Pedestal	0,64	m2
b.	<u>Bekisting sloof</u>	17,24	m2
c.	<u>Bekisting kolom lt.1</u>	2,4	m2
d.	<u>Bekisting balok</u>	28,015	m2
e.	<u>Bekisting kolom lt.2</u>	2,4	m2
f.	<u>Bekisting ring balk</u>	19,395	m2

BACK UP PERHITUNGAN MATERIAL DAN ALAT

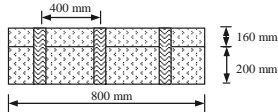
Metode Konvensional

lasi Setempat **n = 12**



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
200	200	160	800

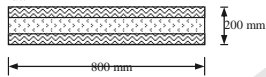
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	2000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

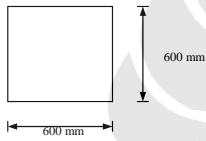
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	3
1	100	800	360

Sisi 2 dan 4



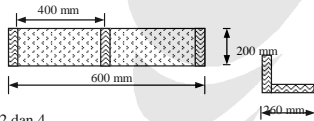
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	800	2
			800

Footing



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
600	600	100	200

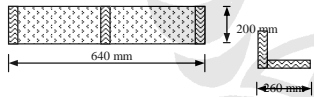
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm') =	40	x	60	x	4000	mm

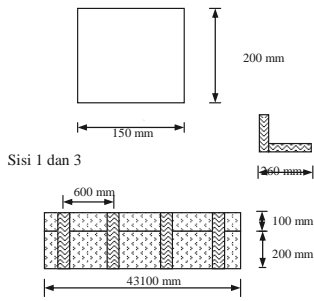
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	600	3
			200
			3
			200

Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	640	3
			200
			3
			200

Sloof n = 1

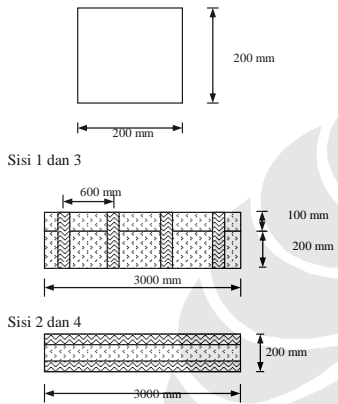


Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
150	200	100	43100

Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200 43100	73	300 m'
1	100 43100	73	200 m'

Kolom It 1 n = 24



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
200	200	100	3000

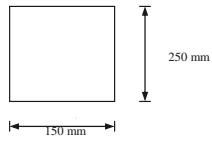
Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000 mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000 mm

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200 3000	6	300
1	100 3000		

Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200 3000	2	3000

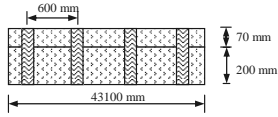
Balok = 3 m

n = 1



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
150	250	20	43100

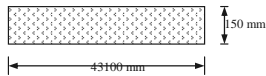
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000	mm

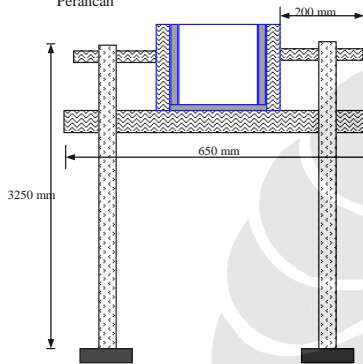
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	200	73	270
1	100	43100	

Sisi 2



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	150	43100	

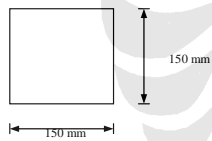
Perancah



Jml Kaso 5/7	Ukuran Kaso	Jml Balok 8/12	Ukuran Balok
146	3250	73	650
		2	43100

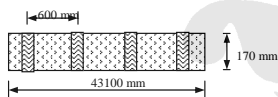
Ring balok = 3 m

n = 1



Panjang (mm)	Lebar (mm)	Lebihan (mm)	Tinggi (mm)
150	150	20	43100

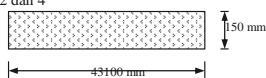
Sisi 1 dan 3



Ukuran Papan 2/20 (mm ²)=	20	x	200	x	4000	mm
Ukuran Kaso 4/6 (mm ²) =	40	x	60	x	4000	mm

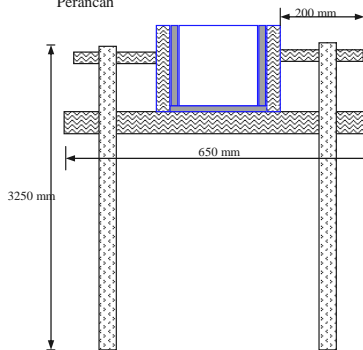
Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	170	73	170

Sisi 2 dan 4



Jml papan	Ukuran Papan	Jml Kaso	Ukuran Kaso
1	150	43100	

Perancah



Jml Kaso 5/7	Ukuran Kaso	Jml Balok 8/12	Ukuran Balok
146	3250	73	650

Daftar Kebutuhan Material

Ukuran Papan 2/20 (mm2)=	0,02	x	0,2	x	2 mm
Ukuran Kaso 4/6 (mm') =	0,04	x	0,06	x	4 mm
Ukuran Kaso 5/7 (mm') =	0,05	x	0,07	x	4 mm
Ukuran Balok 8/12 (mm) =	0,08	x	0,12	x	4 mm

No.	Uraian	n	Jml papan	Ukuran Papan		Luas Total	Jml Papan (lbr)	Jml Kaso	Ukuran Kaso		Volume Kaso (m3)
				L (m)	P (m)				P (m)	P (m)	
1	Pondasi Setempat										
	Pedestal										
	Sisi 1 dan 3	12	1	0,2	0,8	1,92	2,4	3	0,36	12,96	0,031104
	Sisi 2 dan 4	12	1	0,1	0,8	0,96	1,2				
	Sisi 2 dan 4	12	1	0,2	0,8	1,92	2,4	2	0,8	19,2	0,04608
	Footing										
	Sisi 1 dan 3	12	1	0,2	0,6	1,44	1,8	3	0,2	7,2	0,01728
	Sisi 2 dan 4	12	1	0,2	0,64	1,536	1,92	3	0,2	7,2	0,01728
	Sisi 2 dan 4	12	1	0,2	0,64	1,536	1,92	3	0,2	7,2	0,01728
	TOTAL	12				7,776	9,72	3	0,2	60,96	0,146304
2	Sloof 3 m										
	Sisi 1 dan 3	1	1	0,2	43,1	8,62	10,775	73	0,3	21,9	0,05256
	Sisi 2 dan 4	1	1	0,1	43,1	4,31	5,3875	73	0,2	14,6	0,03504
	TOTAL					12,93	16,1625			36,5	0,0876
3	Kolom lt.1										
	Sisi 1 dan 3	12	1	0,2	3	7,2	9	6	0,3	21,6	0,05184
	Sisi 2 dan 4	12	1	0,1	3	3,6	4,5				
	Sisi 2 dan 4	12	1	0,2	3	7,2	9	2	3	7,2	0,1728
	TOTAL					18	22,5			93,6	0,22464
4	Balok = 3 m										
	Sisi 1 dan 3	1	1	0,2	43,1	8,62	10,775	73	0,27	19,71	0,047304
	Sisi 2 dan 4	1	1	0,1	43,1	4,31	5,3875				
	Sisi 2 dan 4	1	1	0,15	43,1	6,465	8,08125				
	TOTAL					19,395	24,24375			19,71	0,047304
5	Kolom lt.2										
	Sisi 1 dan 3	12	1	0,2	3	7,2	9	6	0,3	21,6	0,05184
	Sisi 2 dan 4	12	1	0,1	3	3,6	4,5				
	Sisi 2 dan 4	12	1	0,2	3	7,2	9	2	3	7,2	0,1728
	TOTAL					18	22,5			93,6	0,22464
6	Ring balok = 3 m										
	Sisi 1 dan 3	1	1	0,17	43,1	7,327	9,15875	73	0,17	12,41	0,029784
	Sisi 2 dan 4	1	1	0,15	43,1	6,465	8,08125				
	TOTAL					13,792	17,24			12,41	0,029784
	TOTAL					Papan 2/20 =	179,786		Kaso 4/6 =	633,56	1,520544

No.	Uraian	Jumlah	Jml Kaso 5/7	Panjang Kaso	Panjang Total	Volume Kaso	Jml Balok 8/12	Panjang Balok	Panjang Total	Volume balok
	Perancah Balok	1	146	3,25	474,5	1,66075	2	43,1	86,2	0,82752
			73	0,65	47,45	0,166075				
	TOTAL				521,95	1,826825			86,2	0,82752
	Perancah Ring Balok	1	146	3,25	474,5	1,66075				
			73	0,65	47,45	0,166075				
	TOTAL				521,95	1,826825			0	0
	TOTAL			Kaso 5/7 =	2087,8	7,3073		Balok 8/12 =	172,4	1,65504

DAFTAR HARGA MATERIAL

NO	URAIAN	SATUAN	HARGA SATUAN
	Papan Randu 2/20	lbr	Rp 48.000,00
	Kaso 4/6	m ³	Rp 2.100.000,00
	Kaso 5/7	m ³	Rp 2.100.000,00
	Balok 8/12	m ³	Rp 2.100.000,00
	Paku	kg	Rp 8.000,00
	Minyak Bekisting	ltr	Rp 2.500,00

Biaya Kebutuhan Material Untuk Bekisting

No.	Uraian	Luas Pembetonan	Volume	Satuan	Harga Satuan	Total
1	Pondasi Setempat	1,12				
	Papan Randu 2/20		9,72	lbr	Rp 48.000,00	Rp 466.560,00
	Kaso 4/6		0,146304	m ³	Rp 2.100.000,00	Rp 307.238,40
	Paku		0,336	kg	Rp 8.000,00	Rp 2.688,00
	Minyak Bekisting		0,224	ltr	Rp 2.500,00	Rp 560,00
2	Sloof	17,24				
	Papan Randu 2/20		16,1625	lbr	Rp 48.000,00	Rp 775.800,00
	Kaso 4/6		0,0876	m ³	Rp 2.100.000,00	Rp 183.960,00
	Paku		5,172	kg	Rp 8.000,00	Rp 41.376,00
	Minyak Bekisting		3,448	ltr	Rp 2.500,00	Rp 8.620,00
3	Kolom It.1	2,4				
	Papan Randu 2/20		22,5	lbr	Rp 48.000,00	Rp 1.080.000,00
	Kaso 4/6		0,22464	m ³	Rp 2.100.000,00	Rp 471.744,00
	Paku		0,72	kg	Rp 8.000,00	Rp 5.760,00
	Minyak Bekisting		0,48	ltr	Rp 2.500,00	Rp 1.200,00
4	Balok	28,015				
	Papan Randu 2/20		24,24375	lbr	Rp 48.000,00	Rp 1.163.700,00
	Kaso 4/6		0,047304	m ³	Rp 2.100.000,00	Rp 99.338,40
	Paku		8,4045	kg	Rp 8.000,00	Rp 67.236,00
	Minyak Bekisting		5,603	ltr	Rp 2.500,00	Rp 14.007,50
5	Kolom It.2	2,4				
	Papan Randu 2/20		22,5	lbr	Rp 48.000,00	Rp 1.080.000,00
	Kaso 4/6		0,22464	m ³	Rp 2.100.000,00	Rp 471.744,00
	Paku		0,72	kg	Rp 8.000,00	Rp 5.760,00
	Minyak Bekisting		0,48	ltr	Rp 2.500,00	Rp 1.200,00
6	Ring balok	19,395				
	Papan Randu 2/20		17,24	lbr	Rp 48.000,00	Rp 827.520,00
	Kaso 4/6		0,029784	m ³	Rp 2.100.000,00	Rp 62.546,40
	Paku		5,8185	kg	Rp 8.000,00	Rp 46.548,00
	Minyak Bekisting		3,879	ltr	Rp 2.500,00	Rp 9.697,50
	TOTAL					Rp 7.194.804,20

Biaya Kebutuhan Material Untuk Perancah

No.	Uraian	Volume	Volume / n	Satuan	Harga Satuan	Total
	Balok 3 m					
	Kaso 5/7	1,826825	0,365365	m ³	Rp 2.100.000,00	Rp 767.266,50
	Balok 8/12	0,82752	0,082752	m ³	Rp 2.100.000,00	Rp 173.779,20
	Ring Balok 3 m					
	Kaso 5/7	1,826825	0,365365	m ³	Rp 2.100.000,00	Rp 767.266,50
	Balok 8/12	0	0	m ³	Rp 2.100.000,00	Rp -
	TOTAL					Rp 1.708.312,20

DAFTAR HARGA MATERIAL

NO	URAIAN	KOEFISIEN	SATUAN	HARGA SATUAN
	Pekerja	0,3300	hari	40000
	Mandor	0,0330	hari	55000
	Tukang Kayu	0,3200	hari	50000
	Kepala Tukang Kayu	0,0060	hari	55000

Biaya Kebutuhan Upah Untuk Bekisting

No.	Uraian	Volume pembetonan	Satuan	Koefisien	Volume total	Satuan	Harga Satuan/m2	Total
1	Pondasi Setempat	1,12	m2					
	Pekerja			0,33	0,3696	hari	40000	Rp 14.784,00
	Mandor			0,033	0,03696	hari	55000	Rp 2.032,80
	Tukang Kayu			0,32	0,3584	hari	50000	Rp 17.920,00
	Kepala Tukang Kayu			0,006	0,00672	hari	55000	Rp 369,60
2	Sloof	17,24	m2					
	Pekerja			0,33	5,6892	hari	40000	Rp 227.568,00
	Mandor			0,033	0,56892	hari	55000	Rp 31.290,60
	Tukang Kayu			0,32	5,5168	hari	50000	Rp 275.840,00
	Kepala Tukang Kayu			0,006	0,10344	hari	55000	Rp 5.689,20
3	Kolom It. 1	2,4	m2					
	Pekerja			0,33	0,792	hari	40000	Rp 31.680,00
	Mandor			0,033	0,0792	hari	55000	Rp 4.356,00
	Tukang Kayu			0,32	0,768	hari	50000	Rp 38.400,00
	Kepala Tukang Kayu			0,006	0,0144	hari	55000	Rp 792,00
4	Balok	28,015	m2					
	Pekerja			0,33	9,24495	hari	40000	Rp 369.798,00
	Mandor			0,033	0,924495	hari	55000	Rp 50.847,23
	Tukang Kayu			0,32	8,9648	hari	50000	Rp 448.240,00
	Kepala Tukang Kayu			0,006	0,16809	hari	55000	Rp 9.244,95
5	Kolom It. 2	2,4	m2					
	Pekerja			0,33	0,792	hari	40000	Rp 31.680,00
	Mandor			0,033	0,0792	hari	55000	Rp 4.356,00
	Tukang Kayu			0,32	0,768	hari	50000	Rp 38.400,00
	Kepala Tukang Kayu			0,006	0,0144	hari	55000	Rp 792,00
6	Ring balok	19,395	m2					
	Pekerja			0,33	6,40035	hari	40000	Rp 256.014,00
	Mandor			0,033	0,640035	hari	55000	Rp 35.201,93
	Tukang Kayu			0,32	6,2064	hari	50000	Rp 310.320,00
	Kepala Tukang Kayu			0,006	0,11637	hari	55000	Rp 6.400,35
	TOTAL							Rp 2.212.016,65

Biaya Pekerjaan Bekisting Kayu untuk RT 2 Lantai

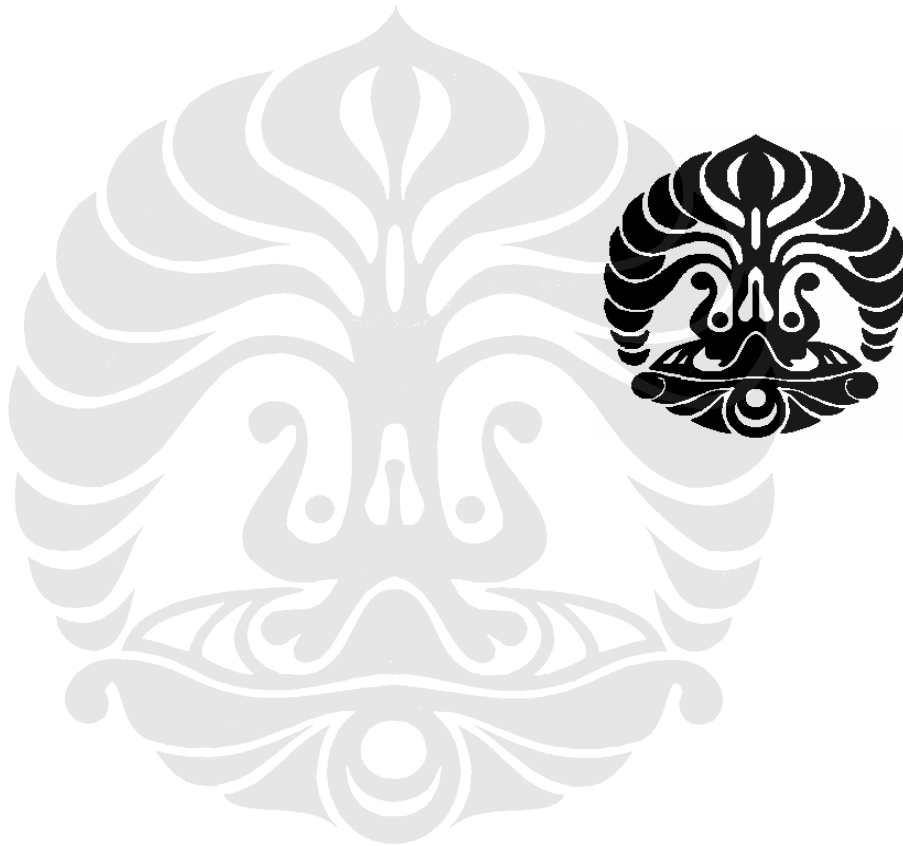
1 rumah tinggal 1 kali pakai

No.	Uraian	Volume pembetonan	Satuan	Harga Material	Harga Upah	Total
1	Pondasi	1,248	m3	Rp 776.486,4	Rp 35.106,40	Rp 811.592,80
2	Sloof	1,293	m3	Rp 1.001.136,0	Rp 540.387,80	Rp 1.541.523,80
3	Kolom lt.1	1,44	m3	Rp 1.557.504,0	Rp 75.228,00	Rp 1.632.732,00
4	Balok	1,61625	m3	Rp 2.271.320,1	Rp 878.130,18	Rp 3.149.450,28
5	Kolom lt.2	1,44	m3	Rp 1.557.504,0	Rp 75.228,00	Rp 1.632.732,00
6	Ring balk	0,96975	m3	Rp 1.703.880,9	Rp 607.936,28	Rp 2.311.817,18
	TOTAL			Rp 8.867.831,40	Rp 2.212.016,65	Rp 11.079.848,05



LAMPIRAN E

Perbandingan Analisa Biaya Bekisting (Rumah tinggal 1 lantai dan 2 lantai)



Dari Segi Biaya

1 set bekisting = 1 x pakai 1 rumah tinggal

Rumah Tinggal 1 Lantai

Biaya material bekisting untuk 1 x pakai dan 1 rumah tinggal

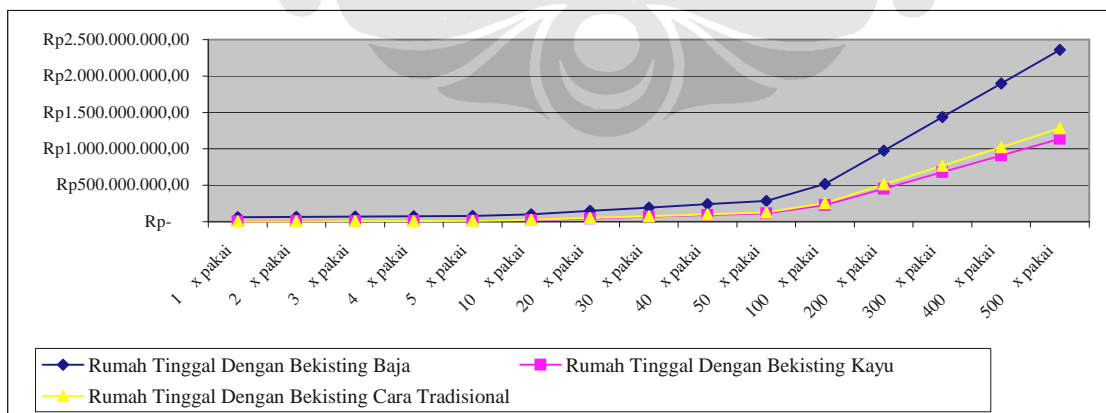
Bekisting Baja	Rp	57.204.876,48
Bekisting Kayu	Rp	5.064.915,00
Bekisting Cara Tradisional	Rp	2.779.430,40

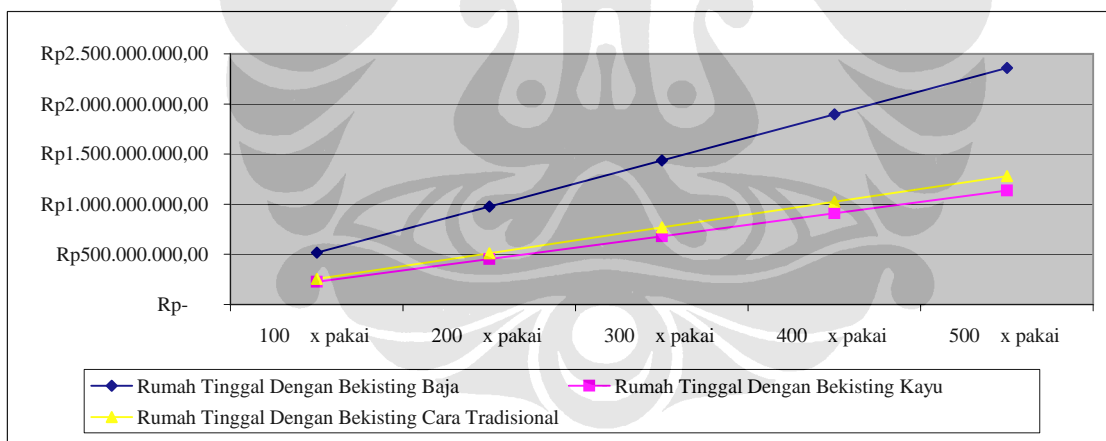
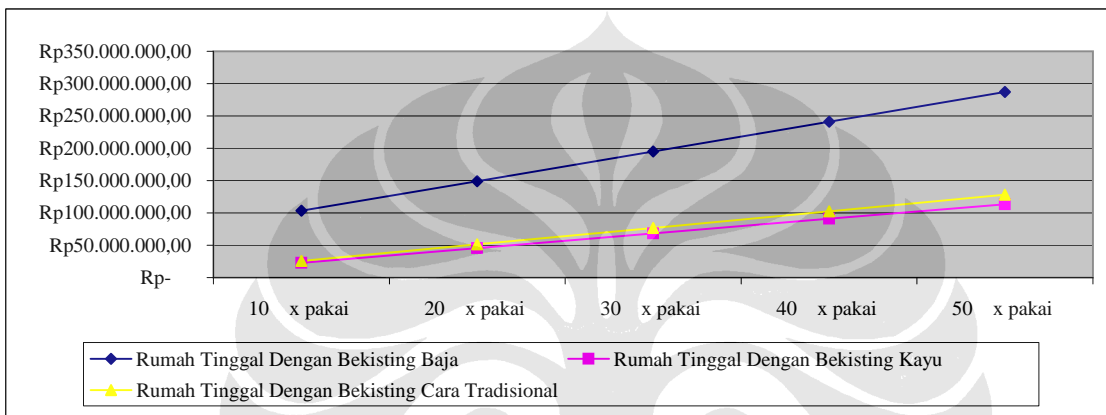
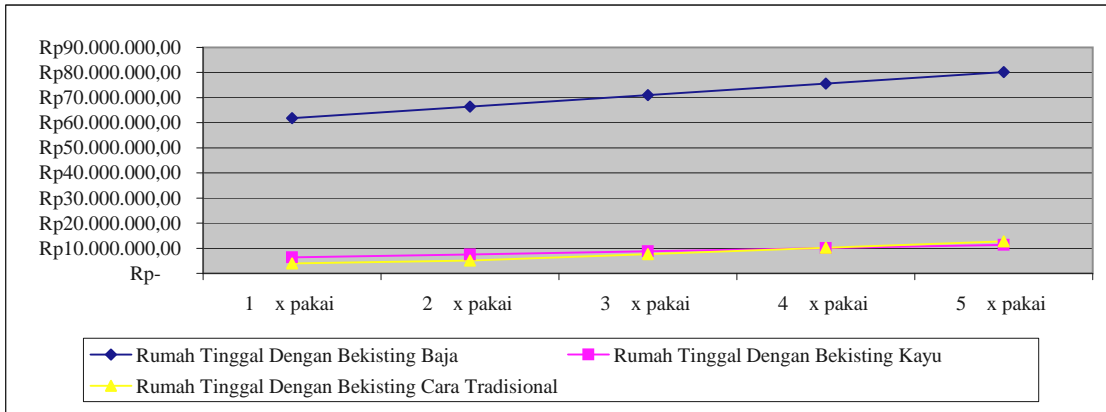
Biaya Upah bekisting untuk 1 rumah tinggal

Bekisting Baja	Rp	4.601.763,00
Bekisting Kayu	Rp	1.258.658,48
Bekisting Cara Tradisional	Rp	1.172.303,00

Perbandingan biaya bekisting dengan variabel n x pakai

	Bekisting Baja	Bekisting Kayu	Bekisting Cara Tradisional
	Pemakaian berulang-ulang	Pemakaian max 5 x pakai	Pemakaian maximum 2 x pakai
	n	5	2
1 x pakai	Rp 61.806.639,48	Rp 6.323.573,48	Rp 3.951.733,40
2 x pakai	Rp 66.408.402,48	Rp 7.582.231,95	Rp 5.124.036,40
3 x pakai	Rp 71.010.165,48	Rp 8.840.890,43	Rp 7.686.054,60
4 x pakai	Rp 75.611.928,48	Rp 10.099.548,90	Rp 10.248.072,80
5 x pakai	Rp 80.213.691,48	Rp 11.358.207,38	Rp 12.810.091,00
10 x pakai	Rp 103.222.506,48	Rp 22.716.414,75	Rp 25.620.182,00
20 x pakai	Rp 149.240.136,48	Rp 45.432.829,50	Rp 51.240.364,00
30 x pakai	Rp 195.257.766,48	Rp 68.149.244,25	Rp 76.860.546,00
40 x pakai	Rp 241.275.396,48	Rp 90.865.659,00	Rp 102.480.728,00
50 x pakai	Rp 287.293.026,48	Rp 113.582.073,75	Rp 128.100.910,00
100 x pakai	Rp 517.381.176,48	Rp 227.164.147,50	Rp 256.201.820,00
200 x pakai	Rp 977.557.476,48	Rp 454.328.295,00	Rp 512.403.640,00
300 x pakai	Rp 1.437.733.776,48	Rp 681.492.442,50	Rp 768.605.460,00
400 x pakai	Rp 1.897.910.076,48	Rp 908.656.590,00	Rp 1.024.807.280,00
500 x pakai	Rp 2.358.086.376,48	Rp 1.135.820.737,50	Rp 1.281.009.100,00





Rumah Tinggal 2 Lantai

Biaya material bekisting untuk 1 x pakai dan 1 rumah tinggal

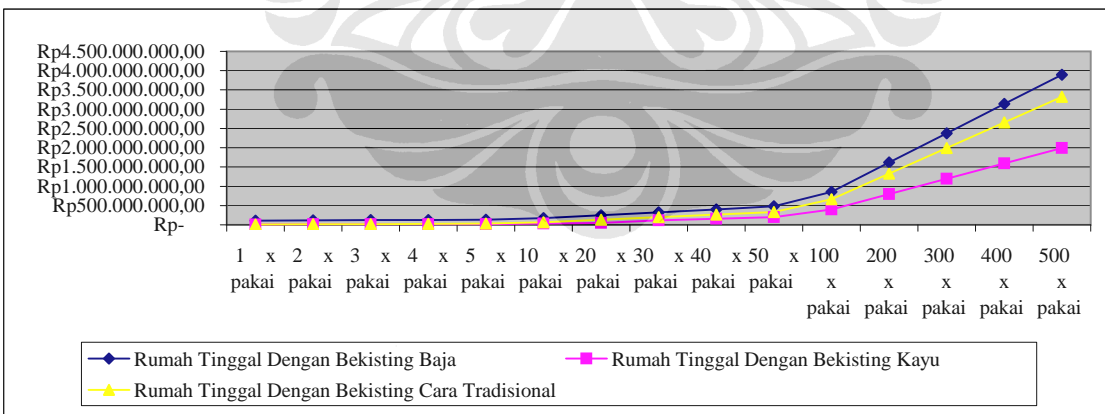
Bekisting Baja	Rp	97.736.777,39
Bekisting Kayu	Rp	8.867.831,40
Bekisting Cara Tradisional	Rp	4.510.970,40

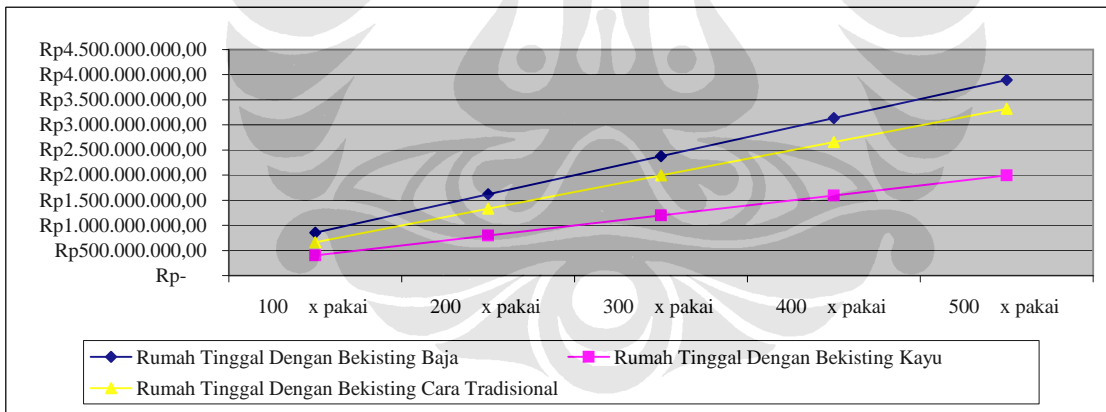
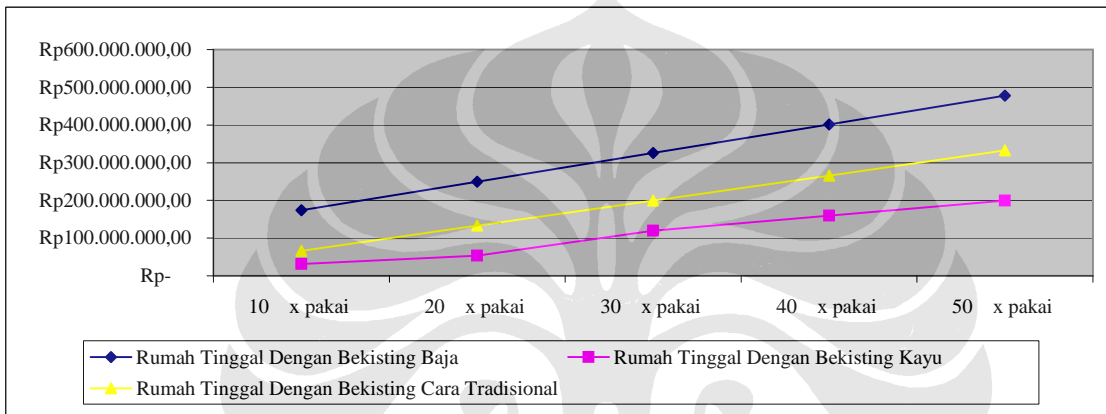
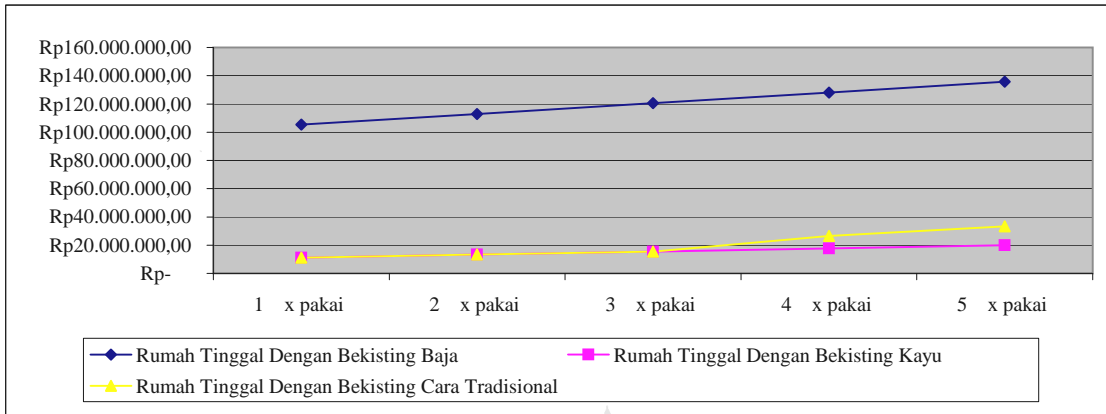
Biaya Upah bekisting untuk 1 rumah tinggal

Bekisting Baja	Rp	7.593.396,00
Bekisting Kayu	Rp	2.212.016,65
Bekisting Cara Tradisional	Rp	1.904.208,75

Perbandingan biaya bekisting dengan variabel n x pakai

	Bekisting Baja	Bekisting Kayu	Bekisting Cara Tradisional
	Pemakaian berulang-ulang n	Pemakaian max 5 x pakai 5	Pemakaian maximum 2 x pakai 2
1 x pakai	Rp 105.330.173,39	Rp 11.079.848,05	Rp 11.079.848,05
2 x pakai	Rp 112.923.569,39	Rp 13.291.864,70	Rp 13.291.864,70
3 x pakai	Rp 120.516.965,39	Rp 15.503.881,35	Rp 15.503.881,35
4 x pakai	Rp 128.110.361,39	Rp 17.715.898,00	Rp 26.583.729,40
5 x pakai	Rp 135.703.757,39	Rp 19.927.914,65	Rp 33.229.661,75
10 x pakai	Rp 173.670.737,39	Rp 30.987.997,90	Rp 66.459.323,50
20 x pakai	Rp 249.604.697,39	Rp 53.108.164,40	Rp 132.918.647,00
30 x pakai	Rp 325.538.657,39	Rp 119.567.487,90	Rp 199.377.970,50
40 x pakai	Rp 401.472.617,39	Rp 159.423.317,20	Rp 265.837.294,00
50 x pakai	Rp 477.406.577,39	Rp 199.279.146,50	Rp 332.296.617,50
100 x pakai	Rp 857.076.377,39	Rp 398.558.293,00	Rp 664.593.235,00
200 x pakai	Rp 1.616.415.977,39	Rp 797.116.586,00	Rp 1.329.186.470,00
300 x pakai	Rp 2.375.755.577,39	Rp 1.195.674.879,00	Rp 1.993.779.705,00
400 x pakai	Rp 3.135.095.177,39	Rp 1.594.233.172,00	Rp 2.658.372.940,00
500 x pakai	Rp 3.894.434.777,39	Rp 1.992.791.465,00	Rp 3.322.966.175,00





Dari Segi Biaya

1 set bekisting = 1 x pakai 1 rumah tinggal

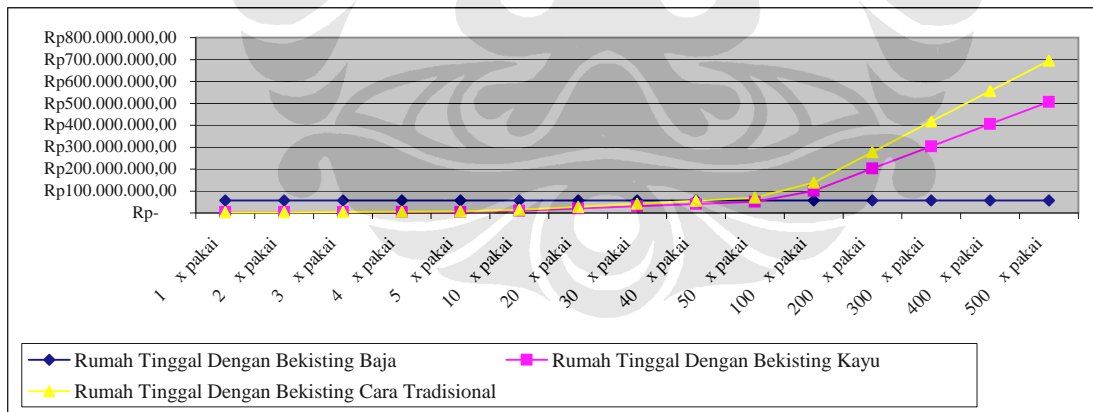
Rumah Tinggal 1 Lantai

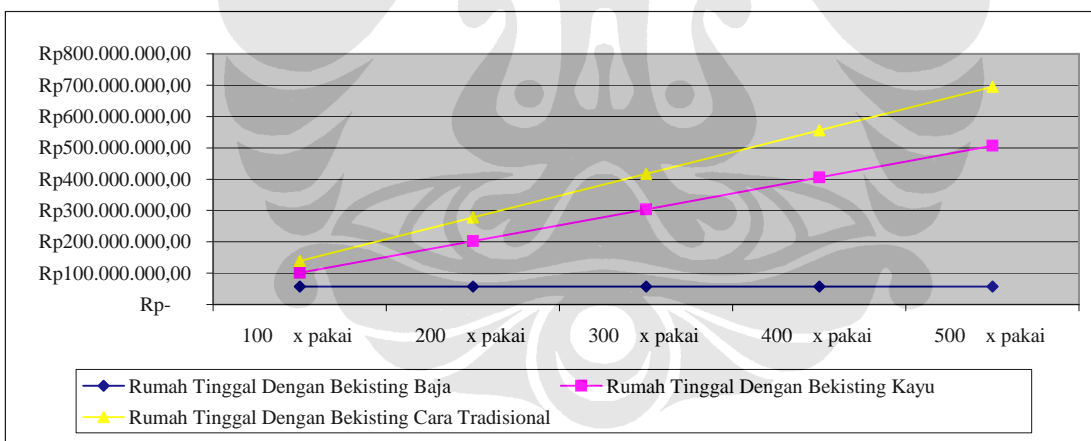
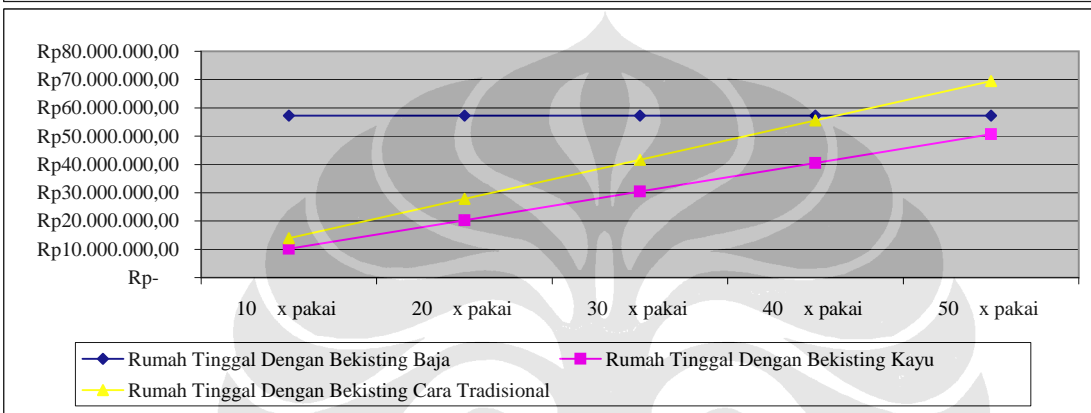
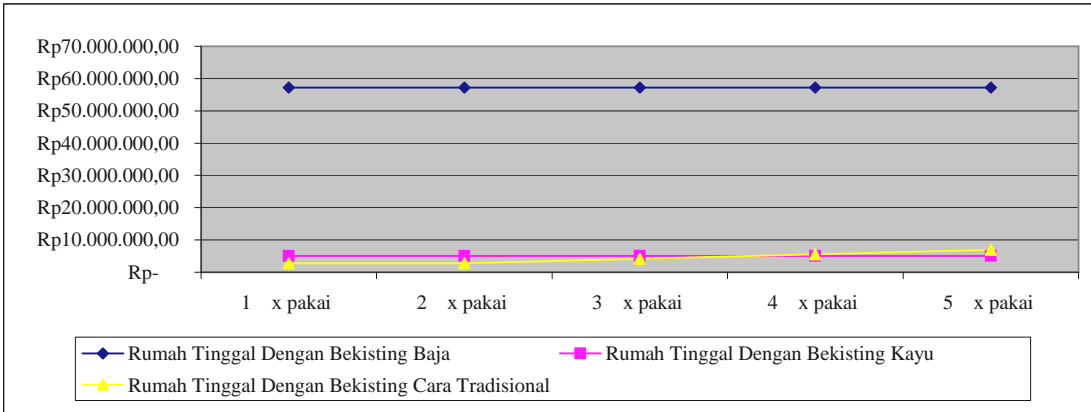
Biaya material bekisting untuk 1 x pakai dan 1 rumah tinggal

Bekisting Baja	Rp	57.204.876,48
Bekisting Kayu	Rp	5.064.915,00
Bekisting Cara Tradisional	Rp	2.779.430,40

Perbandingan biaya bekisting dengan variabel n x pakai

	Bekisting Baja	Bekisting Kayu	Bekisting Cara Tradisional
	Pemakaian berulang-ulang	Pemakaian max 5 x pakai	Pemakaian maximum 2 x pakai
	n	5	2
1 x pakai	Rp 57.204.876,48	Rp 5.064.915,00	Rp 2.779.430,40
2 x pakai	Rp 57.204.876,48	Rp 5.064.915,00	Rp 2.779.430,40
3 x pakai	Rp 57.204.876,48	Rp 5.064.915,00	Rp 4.169.145,60
4 x pakai	Rp 57.204.876,48	Rp 5.064.915,00	Rp 5.558.860,80
5 x pakai	Rp 57.204.876,48	Rp 5.064.915,00	Rp 6.948.576,00
10 x pakai	Rp 57.204.876,48	Rp 10.129.830,00	Rp 13.897.152,00
20 x pakai	Rp 57.204.876,48	Rp 20.259.660,00	Rp 27.794.304,00
30 x pakai	Rp 57.204.876,48	Rp 30.389.490,00	Rp 41.691.456,00
40 x pakai	Rp 57.204.876,48	Rp 40.519.320,00	Rp 55.588.608,00
50 x pakai	Rp 57.204.876,48	Rp 50.649.150,00	Rp 69.485.760,00
100 x pakai	Rp 57.204.876,48	Rp 101.298.300,00	Rp 138.971.520,00
200 x pakai	Rp 57.204.876,48	Rp 202.596.600,00	Rp 277.943.040,00
300 x pakai	Rp 57.204.876,48	Rp 303.894.900,00	Rp 416.914.560,00
400 x pakai	Rp 57.204.876,48	Rp 405.193.200,00	Rp 555.886.080,00
500 x pakai	Rp 57.204.876,48	Rp 506.491.500,00	Rp 694.857.600,00





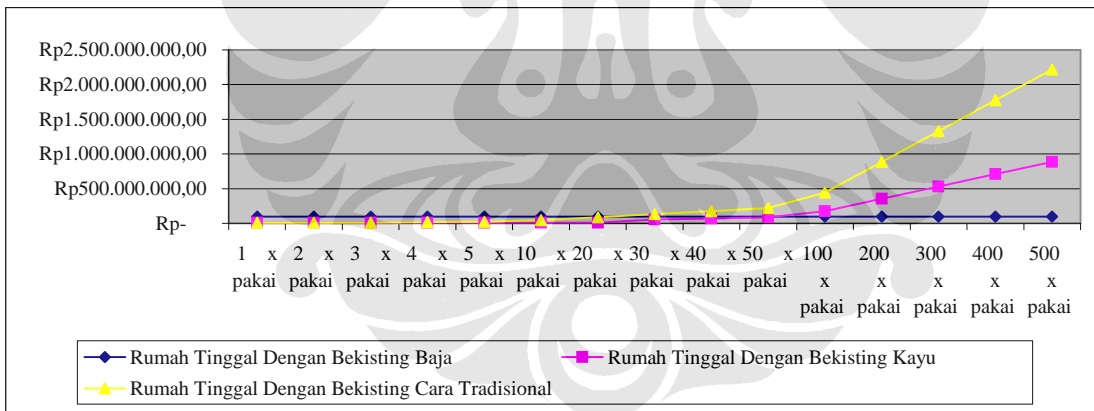
Rumah Tinggal 2 Lantai

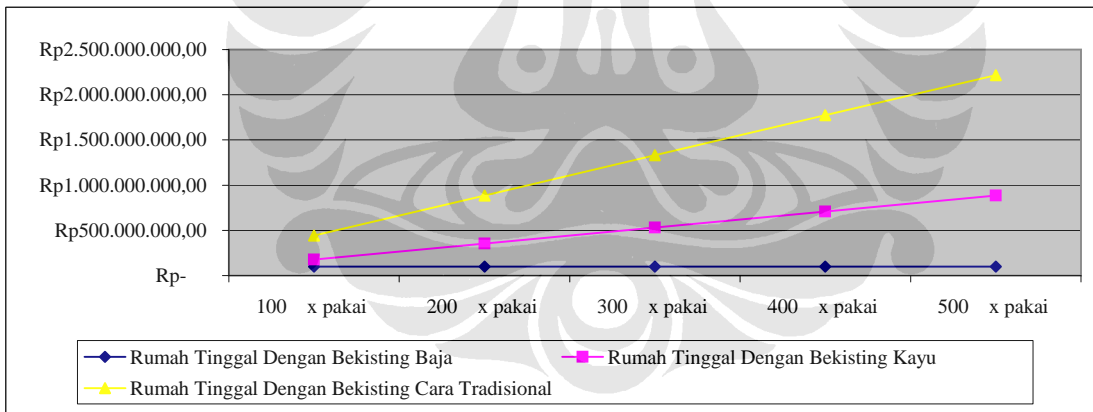
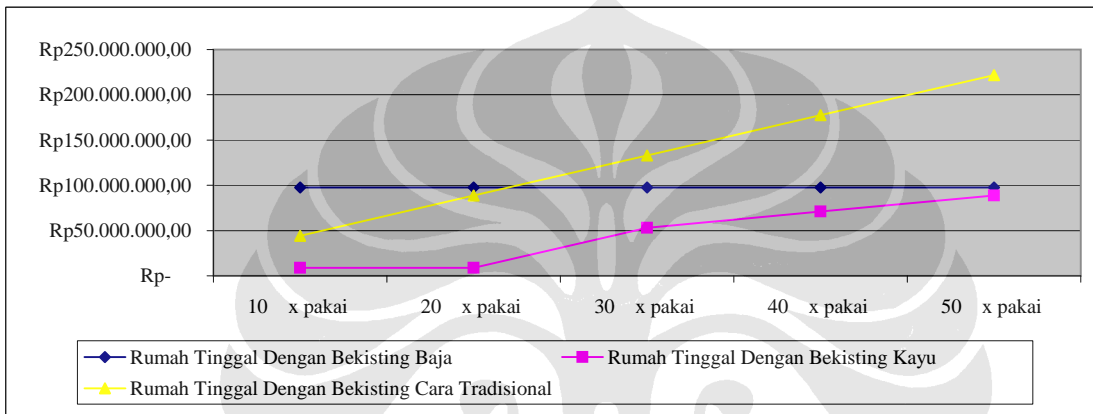
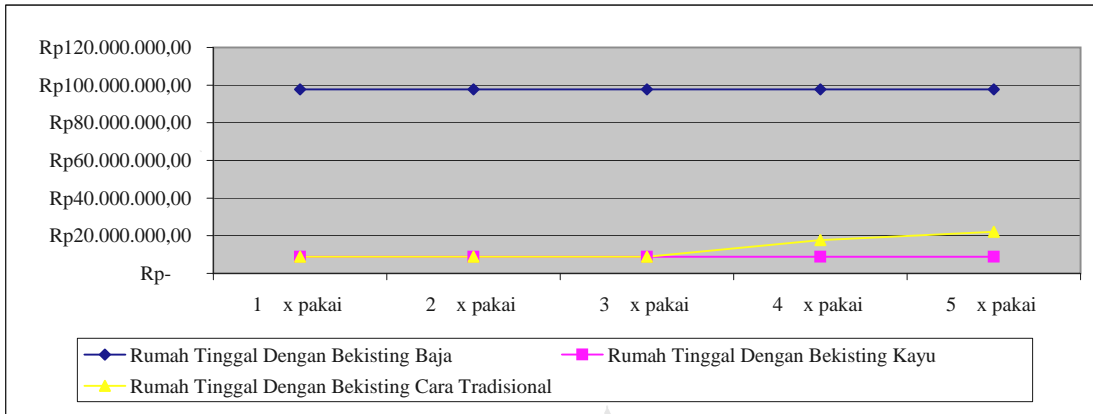
Biaya material bekisting untuk 1 x pakai dan 1 rumah tinggal

Bekisting Baja	Rp	97.736.777,39
Bekisting Kayu	Rp	8.867.831,40
Bekisting Cara Tradisional	Rp	4.510.970,40

Perbandingan biaya bekisting dengan variabel n x pakai

	Bekisting Baja	Bekisting Kayu	Bekisting Cara Tradisional
	Pemakaian berulang-ulang	Pemakaian max 5 x pakai	Pemakaian maximum 2 x pakai
	n	5	2
1 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 8.867.831,40
2 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 8.867.831,40
3 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 8.867.831,40
4 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 17.735.662,80
5 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 22.169.578,50
10 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 44.339.157,00
20 x pakai	Rp 97.736.777,39	Rp 8.867.831,40	Rp 88.678.314,00
30 x pakai	Rp 97.736.777,39	Rp 53.206.988,40	Rp 133.017.471,00
40 x pakai	Rp 97.736.777,39	Rp 70.942.651,20	Rp 177.356.628,00
50 x pakai	Rp 97.736.777,39	Rp 88.678.314,00	Rp 221.695.785,00
100 x pakai	Rp 97.736.777,39	Rp 177.356.628,00	Rp 443.391.570,00
200 x pakai	Rp 97.736.777,39	Rp 354.713.256,00	Rp 886.783.140,00
300 x pakai	Rp 97.736.777,39	Rp 532.069.884,00	Rp 1.330.174.710,00
400 x pakai	Rp 97.736.777,39	Rp 709.426.512,00	Rp 1.773.566.280,00
500 x pakai	Rp 97.736.777,39	Rp 886.783.140,00	Rp 2.216.957.850,00





Dari Segi Biaya

1 set bekisting = 1 x pakai 1 rumah tinggal

Rumah Tinggal 1 Lantai

Biaya material bekisting untuk 1 x pakai dan 1 rumah tinggal

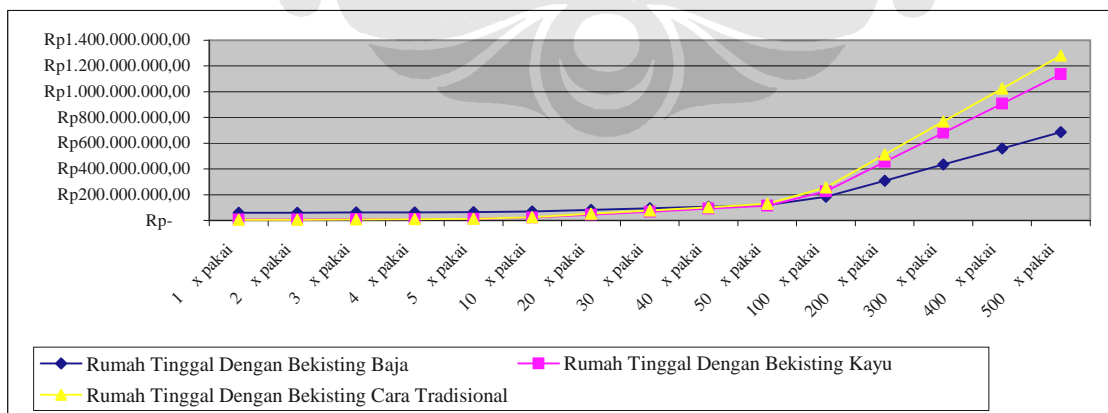
Bekisting Baja	Rp	57.204.876,48
Bekisting Kayu	Rp	5.064.915,00
Bekisting Cara Tradisional	Rp	2.779.430,40

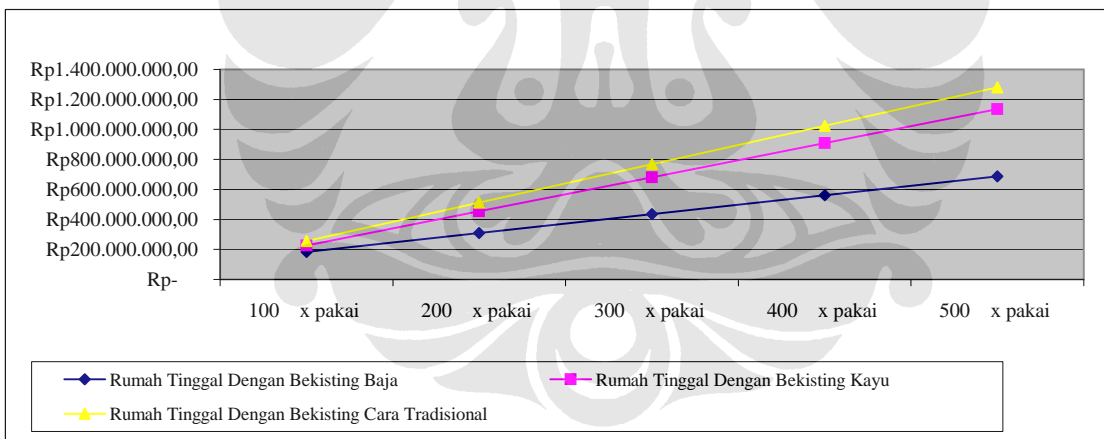
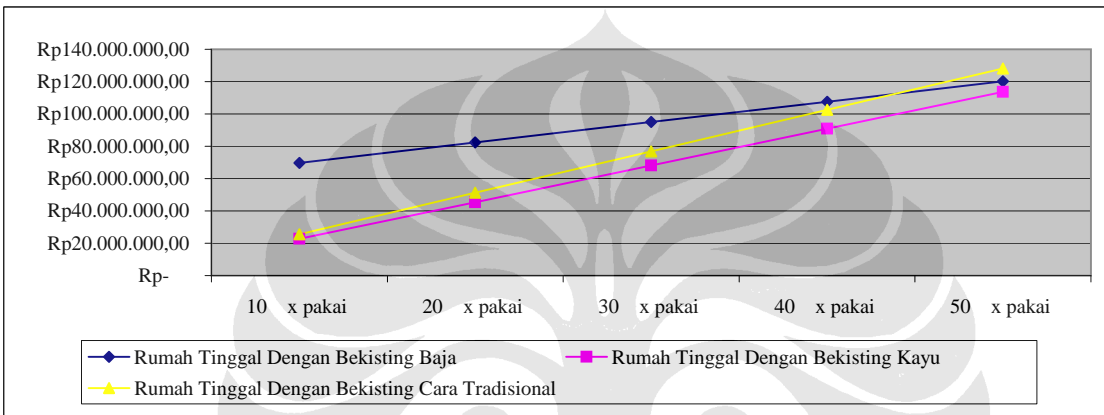
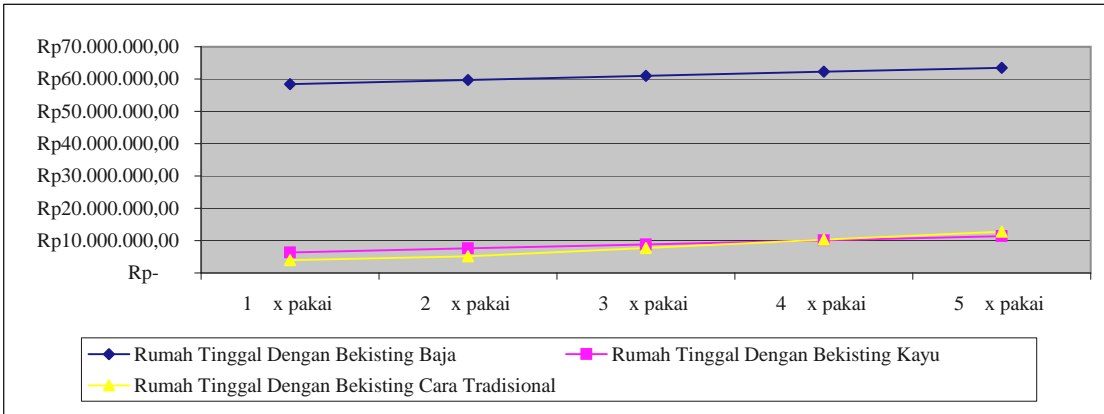
Biaya Upah bekisting untuk 1 rumah tinggal

Bekisting Baja	Rp	1.258.658,48
Bekisting Kayu	Rp	1.258.658,48
Bekisting Cara Tradisional	Rp	1.172.303,00

Perbandingan biaya bekisting dengan variabel n x pakai

	Bekisting Baja	Bekisting Kayu	Bekisting Cara Tradisional
	Pemakaian berulang-ulang	Pemakaian max 5 x pakai	Pemakaian maximum 2 x pakai
	n	5	2
1 x pakai	Rp 58.463.534,95	Rp 6.323.573,48	Rp 3.951.733,40
2 x pakai	Rp 59.722.193,43	Rp 7.582.231,95	Rp 5.124.036,40
3 x pakai	Rp 60.980.851,90	Rp 8.840.890,43	Rp 7.686.054,60
4 x pakai	Rp 62.239.510,38	Rp 10.099.548,90	Rp 10.248.072,80
5 x pakai	Rp 63.498.168,85	Rp 11.358.207,38	Rp 12.810.091,00
10 x pakai	Rp 69.791.461,23	Rp 22.716.414,75	Rp 25.620.182,00
20 x pakai	Rp 82.378.045,98	Rp 45.432.829,50	Rp 51.240.364,00
30 x pakai	Rp 94.964.630,73	Rp 68.149.244,25	Rp 76.860.546,00
40 x pakai	Rp 107.551.215,48	Rp 90.865.659,00	Rp 102.480.728,00
50 x pakai	Rp 120.137.800,23	Rp 113.582.073,75	Rp 128.100.910,00
100 x pakai	Rp 183.070.723,98	Rp 227.164.147,50	Rp 256.201.820,00
200 x pakai	Rp 308.936.571,48	Rp 454.328.295,00	Rp 512.403.640,00
300 x pakai	Rp 434.802.418,98	Rp 681.492.442,50	Rp 768.605.460,00
400 x pakai	Rp 560.668.266,48	Rp 908.656.590,00	Rp 1.024.807.280,00
500 x pakai	Rp 686.534.113,98	Rp 1.135.820.737,50	Rp 1.281.009.100,00





Rumah Tinggal 2 Lantai

Biaya material bekisting untuk 1 x pakai dan 1 rumah tinggal

Bekisting Baja	Rp	97.736.777,39
Bekisting Kayu	Rp	8.867.831,40
Bekisting Cara Tradisional	Rp	4.510.970,40

Biaya Upah bekisting untuk 1 rumah tinggal

Bekisting Baja	Rp	2.212.016,65
Bekisting Kayu	Rp	2.212.016,65
Bekisting Cara Tradisional	Rp	1.904.208,75

Perbandingan biaya bekisting dengan variabel n x pakai

	Dengan Bekisting Baja	Dengan Bekisting Kayu	Dengan Bekisting Konvensional
	Pemakaian berulang-ulang	Pemakaian max 5 x pakai	Pemakaian maximum 2 x pakai
	n	5	2
1 x pakai	Rp 99.948.794,04	Rp 11.079.848,05	Rp 11.079.848,05
2 x pakai	Rp 102.160.810,69	Rp 13.291.864,70	Rp 13.291.864,70
3 x pakai	Rp 104.372.827,34	Rp 15.503.881,35	Rp 15.503.881,35
4 x pakai	Rp 106.584.843,99	Rp 17.715.898,00	Rp 26.583.729,40
5 x pakai	Rp 108.796.860,64	Rp 19.927.914,65	Rp 33.229.661,75
10 x pakai	Rp 119.856.943,89	Rp 30.987.997,90	Rp 66.459.323,50
20 x pakai	Rp 141.977.110,39	Rp 53.108.164,40	Rp 132.918.647,00
30 x pakai	Rp 164.097.276,89	Rp 119.567.487,90	Rp 199.377.970,50
40 x pakai	Rp 186.217.443,39	Rp 159.423.317,20	Rp 265.837.294,00
50 x pakai	Rp 208.337.609,89	Rp 199.279.146,50	Rp 332.296.617,50
100 x pakai	Rp 318.938.442,39	Rp 398.558.293,00	Rp 664.593.235,00
200 x pakai	Rp 540.140.107,39	Rp 797.116.586,00	Rp 1.329.186.470,00
300 x pakai	Rp 761.341.772,39	Rp 1.195.674.879,00	Rp 1.993.779.705,00
400 x pakai	Rp 982.543.437,39	Rp 1.594.233.172,00	Rp 2.658.372.940,00
500 x pakai	Rp 1.203.745.102,39	Rp 1.992.791.465,00	Rp 3.322.966.175,00

