

LAMPIRAN



No	Parameter	Alat dan Bahan	Prosedur Penelitian
1	Amonium	<ul style="list-style-type: none"> • Spektrofotometer type DR-5000 HACH/ UV-Vis spektrofotometer type DR-5000 HACH • labu Kjeldahl 500 mL; • pipet mikro 100, 250, 500 dan 1000 μL; • labu ukur 500 dan 1000 mL; • gelas ukur 100 mL; • pipet ukur 10 mL; • labu erlenmeyer 100 dan 250 mL; • gelas piala 100 mL. 	<p>a. cara pengukuran kadar nitrogen-orgarnik dihitung sebagai ammonium-N yang terdapat dalam air antara 0,02- 5,00 mg/L NH₄-N;</p> <p>b. penggunaan metode makro Kjeldahl dengan alat spektrofotometer pada kisaran panjang gelombang 400-500 nm.</p>

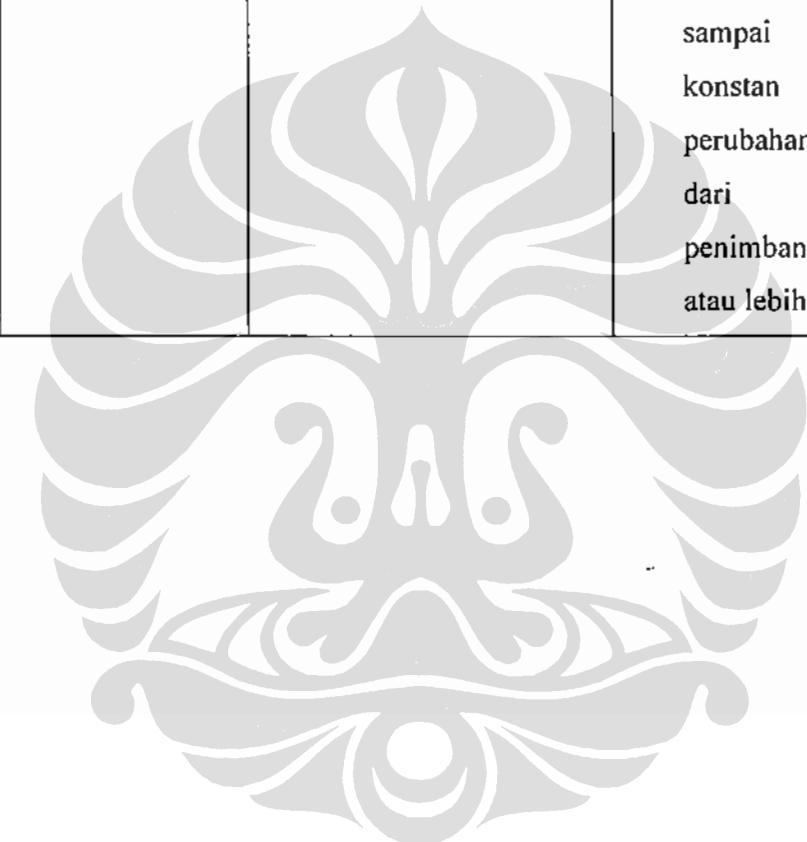
2	Indeks volume lumpur	a. Tabung Imhoff (<i>Imhoff cone</i>). b. <i>Stopwatch</i> c. Termometer	1. Masukan 1 liter contoh / sample ke dalam tabung Imhoff. 2. jalankan stopwacth. Catat perolehan volume lumpur yang terkumpul didasar tabung Imhoff setiap 5, 10, 15, 20, 30, 45 dan 60 menit.
3.	Phospat	<ul style="list-style-type: none"> ▪ Air suling. ▪ Culvet ▪ Amino Acid 1934-32 ▪ Molybdovanadate 20760 ▪ gelas ukur; ▪ Sampel air 100 ml ▪ Spektrofotometer type type DR-5000 HACH 	<ol style="list-style-type: none"> 1. Set program 501 (layer akan menunjukan Dial nm TO 890) 2. Putar panjang gelombang ke 890 nm 3. Tekan READ/ENTER (layer akan menunjukan mg/l PO₄³⁻) 4. Masukan contoh ke cuvet 5. Masukan fosfor 3 phosphate powder ke cuvet (sampel akan berwarna biru bening) 6. Tekan SHIFT Timer 7 (2 menit) 7. Ketika tanda peringatan berbunyi masukan cuvet blanko 8. Tekan ZERO hingga muncul 0,00 mg/l PO₄³⁻ FV 9. Segera masukan cuvet sampel, tidak boleh lebih dari 3 menit sejak tanda peringatan berbunyi 10. Tekan READ/ENTER, baca

			hasil yang tertera di Dial
4.	DO	<ul style="list-style-type: none"> • DO meter yang telah dikalibrasi, ▪ botol KOB, • pengaduk magnit yang dilengkapi pengatur kecepatan putar tetap dan waktu. 	<ol style="list-style-type: none"> 1. penyediaan contoh uji yang telah diambil sesuai dengan metode pengambilan contoh uji kualitas air, 2. isi botol KOB dengan contoh uji secara duplo sampai penuh biarkan terjadi turbulensi, 3. benda uji siap diuji. 4. hidupkan alat DO meter atur alat DO meter untuk mengukur suhu udara 5. baca dan catat suhu udara 6. atur alat DO meter untuk mengukur oksigen terlarut atur DO meter sehingga menunjukkan kadar oksigen diudara. 7. masukkan magnit kedalam botol KOB, 8. aduk benda uji dengan pengaduk magnit, 9. catat skala yang ditunjuk pada skala alat sebagai kadar DO dalam mg/L.
5.	TSS	<ul style="list-style-type: none"> ▪ Kertas saring (glass-fiber filter) dengan beberapa jenis: ▪ Air suling, ▪ desikator yang berisi silika gel; 	<ol style="list-style-type: none"> 1. Gunakan wadah gelas atau botol plastik polietilen atau yang setara. 2. Awetkan contoh uji pada suhu 4°C, untuk meminimalkan dekomposisi mikrobiologikal

	<ul style="list-style-type: none"> ▪ oven, untuk pengoperasian pada suhu 103°C sampai dengan 105°C; ▪ timbangan analitik dengan ketelitian 0,1 mg; ▪ pengaduk magnetik; ▪ pipet volum; ▪ gelas ukur; ▪ cawan aluminium; ▪ cawan porselen/cawan Gooch; ▪ penjepit; ▪ kaca arloji; ▪ pompa vacum. 	<p>terhadap padatan.</p> <ol style="list-style-type: none"> 3. Contoh uji sebaiknya disimpan tidak lebih dari 24 jam. 4. Letakkan kertas saring pada peralatan filtrasi. Pasang vakum dan wadah pencuci dengan air suling berlebih 20 mL. Lanjutkan penyedotan untuk menghilangkan semua sisa air, matikan vakum, dan hentikan pencucian. 5. Pindahkan kertas saring dari peralatan filtrasi ke wadah timbang aluminium. Jika digunakan cawan Gooch dapat langsung dikeringkan. 6. Keringkan dalam oven pada suhu 103°C sampai dengan 105°C selama 1 jam, dinginkan dalam desikator kemudian timbang. 7. Ulangi langkah pada butir c) sampai diperoleh berat konstan atau sampai perubahan berat lebih kecil dari 4% terhadap penimbangan sebelumnya atau lebih kecil dari 0,5 mg. 8. Lakukan penyaringan dengan peralatan vakum. Basahi
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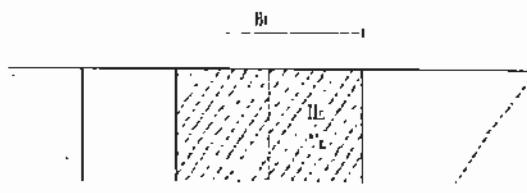
		<p>saringan dengan sedikit air suling.</p> <ol style="list-style-type: none"> 9. Aduk contoh uji dengan pengaduk magnetik untuk memperoleh contoh uji yang lebih homogen. 10. Pipet contoh uji dengan volume tertentu, pada waktu contoh diaduk dengan pengaduk magnetik 11. Cuci kertas saring atau saringan dengan 3×10 mL air suling, biarkan kering sempurna, dan lanjutkan penyaringan dengan vakum selama 3 menit agar diperoleh penyaringan sempurna. Contoh uji dengan padatan terlarut yang tinggi memerlukan pencucian tambahan. 12. Pindahkan kertas saring secara hati-hati dari peralatan penyaring dan pindahkan ke wadah timbang aluminium sebagai penyangga. Jika digunakan cawan Gooch pindahkan cawan dari rangkaian alatnya. 13. Keringkan dalam oven setidaknya selama 1 jam pada
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		<p>suhu 103°C sampai dengan 105°C, dinginkan dalam desikator untuk menyeimbangkan suhu dan timbang.</p> <p>14. Ulangi tahapan pengeringan, pendinginan dalam desikator, dan lakukan penimbangan sampai diperoleh berat konstan atau sampai perubahan berat lebih kecil dari 4% terhadap penimbangan sebelumnya atau lebih kecil dari 0,5 mg.</p>
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Tabel. 2. Prosedur Pengukuran Debit

No	Kegiatan	Alat dan Perlengkapan	Prosedur Pelaksanaan
1	Pengukuran Debit	<ul style="list-style-type: none"> • Current meter dan perlengkapan nya • Pita ukur atau meteran • Alat tulis • Stop watch 	<ol style="list-style-type: none"> 1. Menentukan penampang sungai di bagian sungai yang lurus dan mempunyai aliran sejajar. 2. Menentukan satu penampang sungai dibagian sungai yang lurus dan mempunyai aliran sejajar dengan interval sebesar $\frac{1}{4}$ lebar sungai. 3. Kecepatan aliran penampang tersebut diukur dengan alat ukur kecepatan current meter. 4. Jika kedalaman air (H) lebih dari 1 meter, alat ukur di tempatkan pada dua titik, masing-masing 0,2 H dan 0,8 H, dan hasil pengukurannya adalah : $V = \frac{1}{2}(V_{0,2} + V_{0,8})$ Atau pada 3 titik masing-masing pada 0,2 H, 0,6 H dan 0,8 H dan hasil pengukuran adalah : $V = \frac{1}{3}(V_{0,2} + V_{0,6} + V_{0,8})$ Tetapi jika kedalaman air (H) kurang dari 20 cm maka alat ukut hanya ditempatkan pada titik 0,2 H. 5. Kedalaman sungai menurut penampang diukur dengan meteran. 6. Hitung debit pada masing-masing penampang dihitung dengan menggunakan metode "<i>mean area methode</i>" atau "<i>mid area methode</i>".



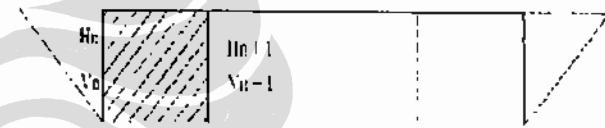
Persamaan debit menjadi sebagai berikut :

$$Q_n = H_n B_n V_n$$

$$n = 1, \dots, n$$

$$Q_p = \sum q_n$$

a. Mid area method



Persamaan debit menjadi sebagai berikut :

$$Q_n = \frac{1}{2} (H_n + H_{n+1})(V_n + V_{n+1}) \cdot \frac{1}{2} B$$

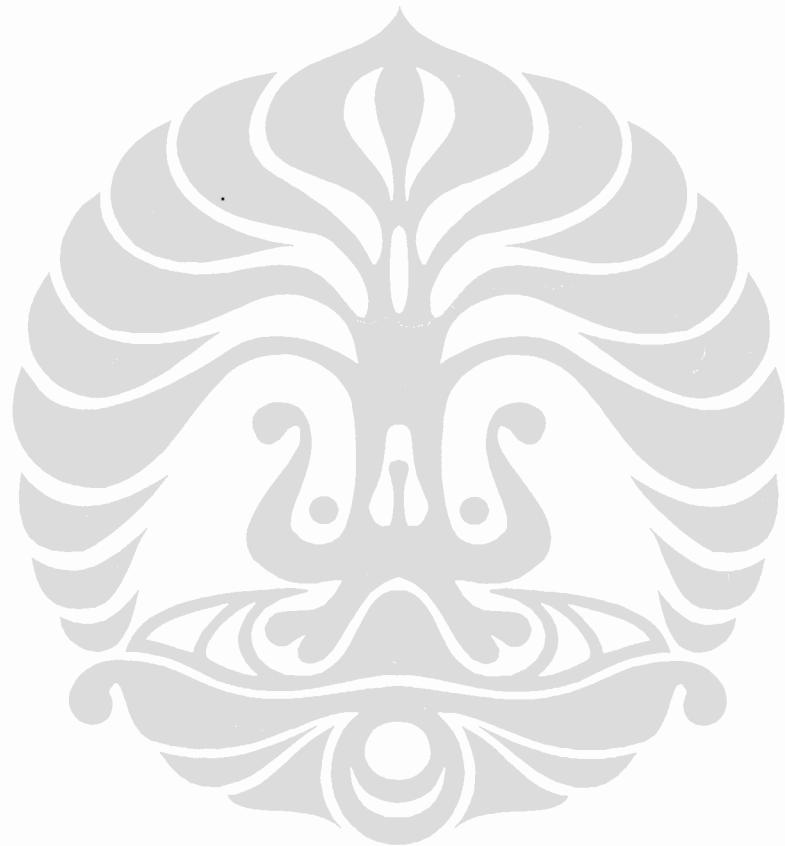
- b. Untuk perbandingan debit di salah satu potongan melintang (Q_p) dapat dihitung dengan rumus :

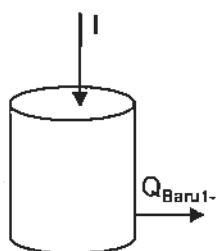
$$Q_p = A_p * V_p$$

$$V_p = \frac{V_1 + V_2 + \dots + V_m}{N}$$

Dimana :

			<p>Q_p = debit sungai pada potongan melintang</p> <p>A_p = luas penampang basah sungai pada potongan melintang</p> <p>V_p = kecepatan aliran sungai pada potongan melintang</p>
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$C_1 = 9.23$
 $C_2 = 12.32$

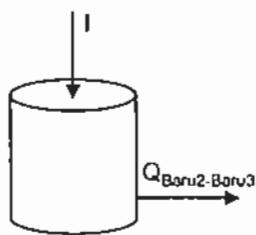
Danau	$C(t)$	W_i	Q_i m^3/hari	V m^3	H m	A m^2	vs m/h	k hari^{-1}	λ_i hari^{-1}
S. Baru1	9.2	0	12092.29	10000	2	5000	0.01	0.1	1.29

initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{dalu}} \text{ g/m}^3 \\ c_1(t) &= 9.2 \text{ g/m}^3 \end{aligned} \quad c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= -\lambda_1 c_1 & k_{11} = f(t, c(t)) &= - \\ dt &= 0.5 \text{ hr} & k_{21} = f(t + 1/2 \Delta t, c(t) + 1) &= - (t + 1/2 \Delta t k_{11}) \\ t &= 0 & k_{31} = f(t + 1/2 \Delta t, c(t) + 1) &= - (t + 1/2 \Delta t k_{21}) \\ c_1(t) &= 9.2 & k_{41} = f(t + \Delta t, c(t) + \Delta t k_1) &= - (t + \Delta t k_{31}) \end{aligned}$$

Δt 0.5	$c_1(t)$	f_{11}		k_{11}	f_{21}		k_{21}	f_{31}		k_{31}	f_{41}		k_{41}	$c_1(t + \Delta t)$
$t = 0$	9.23													9.23
0.5	0.00	9.23	-11.88	0.25	6.26	-8.06	0.25	7.22	-9.29	0.50	4.59	-5.90	4.86	
$(t + \Delta t)$	4.86													
1.000	0.50	4.86	-6.25	0.75	1.73	-2.23	0.75	4.30	-5.54	1.00	2.09	-2.69	2.82	
$(t + \Delta t)$	3.02													
1.5000	1.00	3.02	-3.88	1.25	2.05	-2.63	1.25	2.36	-3.04	1.50	1.50	-1.93	1.59	
$(t + \Delta t)$	1.59													
2.0000	1.50	1.59	-2.04	1.75	1.08	-1.39	1.75	1.24	-1.60	2.00	0.79	-1.02	0.84	
$(t + \Delta t)$	0.84													
2.5000	2.00	0.84	-1.08	2.25	0.57	-0.73	2.25	0.65	-0.84	2.50	0.42	-0.53	0.44	
$(t + \Delta t)$	0.44													
3.0000	2.50	0.44	-0.57	2.50	0.30	-0.38	2.50	0.34	-0.44	3.00	0.44	-0.57	0.21	
$(t + \Delta t)$	0.21													
3.5000	3.00	0.21	-0.27	3.00	0.21	-0.27	3.00	0.14	-0.18	3.50	0.21	-0.27	0.09	
$(t + \Delta t)$	0.09													
4.0000	3.50	0.09	-0.11	3.50	0.09	-0.11	3.50	0.06	-0.08	4.00	0.09	-0.11	0.04	
$(t + \Delta t)$	0.04													
4.5000	4.00	0.04	-0.05	4.00	0.04	-0.05	4.00	0.03	-0.03	4.50	0.04	-0.05	0.02	
$(t + \Delta t)$	0.02													
5.0000	4.50	0.02	-0.02	4.50	0.02	-0.02	4.50	0.01	-0.01	5.00	0.02	-0.02	0.01	



C1 9.23
C2 12.32

Danau	C (t) g/m ³	W _i g/hari	Q _i m ³ /ha	V m ³	H m	A m ²	v _s m/ha	k hari ⁻¹	λ _i hari ⁻¹
S.Baru 2	12.3	0	3381	20000	2	10000	0.01	0.073	0.247

initial condition

$$t = 0$$

$$c(t) = c_{\text{dau}} \text{ g/m}^3$$

$$c_1(t) = 12.3 \text{ g/m}^3 \quad c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady

$$\frac{dc_1}{dt} = f(t, c_1) = -\lambda_1 c_1$$

$$k_{11} = f(t, c_1) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{11})$$

$$k_{21} = f(t + 1/2 \Delta t, c_1) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{21})$$

$$k_{31} = f(t + \Delta t, c_1) = -\lambda_1 c_1 (t + \Delta t k_{31})$$

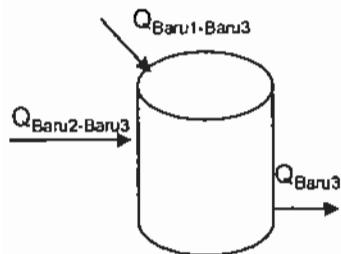
$$\Delta t = 0.5 \text{ hr}$$

$$t = 0$$

$$c_1(t) = 12.32$$

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t + Δt)
t = 0	12.320									12.320
0.5	0.000	12.320	-3.044	0.250	11.559	-2.856	0.250	11.606	-2.868	0.500
(t + Δt)=0,5	10.888									10.888
1.0	0.500	10.888	-2.690	0.750	9.543	-2.358	0.750	10.299	-2.545	1.000
(t + Δt)=1,0	9.649									9.649
1.5	1.000	9.649	-2.384	1.250	9.053	-2.237	1.250	9.090	-2.246	1.500
(t + Δt)=1,5	8.528									8.528
2.0	1.500	8.528	-2.107	1.750	8.001	-1.977	1.750	8.034	-1.985	2.000
(t + Δt)=2,0	7.537									7.537
2.5	2.000	7.537	-1.862	2.250	7.071	-1.747	2.250	7.100	-1.754	2.500
(t + Δt)=2,5	6.661									6.661
3.0	2.500	6.661	-1.646	2.500	6.249	-1.544	2.500	6.275	-1.550	3.000
(t + Δt)=3,0	5.871									5.871
3.5	3.000	5.871	-1.451	3.000	5.871	-1.451	3.000	5.508	-1.361	3.500
(t + Δt)=3,5	5.161									5.161
4.0	3.500	5.161	-1.275	3.500	5.161	-1.275	3.500	4.842	-1.196	4.000
(t + Δt)=4,0	4.536									4.536
4.5	4.000	4.536	-1.121	4.000	4.536	-1.121	4.000	4.256	-1.052	4.500
(t + Δt)=4,5	3.987									3.987
5.0	4.500	3.987	-0.985	4.500	3.987	-0.985	4.500	3.741	-0.924	5.000
(t + Δt)=5,0	3.505									3.505
	5.000	3.505	-0.866	5.000	3.505	-0.866	5.000	3.288	-0.812	0.000
										3.081

PO4 - 3



Danau	C (t) g/m ³	W _i	Q _i m ³ /ha	V m ³	H m	A m ²	v m/ha	k hari ⁻¹	λ ₄ hari ⁻¹
S. Baru 1	9.23	0	12092	10000	2	5000	0.01	0.073	1.287
S. Baru 2	12.32	0	3381.4	20000	2	10000	0.01	0.073	0.247
S. Baru 3	4.24	0	15474	12500	2.5	5000	0.01	0.073	1.315

$$\frac{dc_4}{dt} = W_4/V + \lambda_4 c_4$$

$$dt = 0.5$$

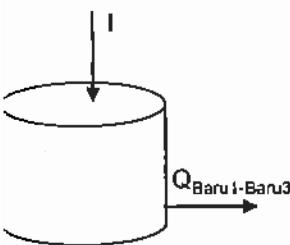
initial condition

$$\begin{aligned} t &= 0 \\ c_4(t) &= c_{\text{danan}} \text{ g/m}^3 \\ c_4(t) &= 4.24 \text{ g/m}^3 \end{aligned}$$

$$\begin{aligned} c_4(t + \Delta t) &= c_4(t) + \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4) \Delta t \\ k_{14} &= f(t, c(t)) = W_3/V + \lambda_4 c_4 \\ k_{24} &= f(t + 1/2 \Delta t, c(t)) = W(1 + 1/2 \lambda_4 c_4) (t + 1/2 \Delta t k_{14}) \\ &\quad + (t + 1/2 + \Delta t k_{14}) \\ k_{34} &= f(t + 1/2 \Delta t, c(t)) = W(1 + 1/2 \lambda_4 c_4) (t + 1/2 \Delta t k_{24}) \\ &\quad + (t + 1/2 + \Delta t k_{24}) \\ k_{43} &= f(t + \Delta t, c(t)) = W(1 + \Delta t \lambda_4 c_4) (t + \Delta t k_{34}) \end{aligned}$$

Δt 0.5	c ₄ (t)	f	k ₁₄	f	k ₂₄	f	k ₃₄	f	k ₄₄	c ₄ (t + Δt)
1 = 0	4.240									4.240
0.5	0.000	4.240	7.669	0.250	6.157	1.428	0.250	4.597	4.643	0.500
(t + Δt)=0,5	5.787									5.787
1.0	0.500	5.787	0.104	0.750	5.813	-3.937	0.750	4.803	0.625	1.000
(t + Δt)= 1,0	4.922									4.922
1.5	1.000	4.922	-1.191	1.250	4.624	-2.074	1.250	4.403	-1.400	1.500
(t + Δt)= 1,5	4.052									4.052
2.0	1.500	4.052	-1.966	1.750	3.561	-2.027	1.750	3.545	-1.802	2.000
(t + Δt)= 2,0	3.090									3.090
2.5	2.000	3.090	-1.779	2.250	2.646	-1.598	2.250	2.691	-1.548	2.500
(t + Δt)= 2,5	2.300									2.300
3.0	2.500	2.300	-1.366	2.750	1.958	-1.158	2.750	2.010	-1.167	3.000
(t + Δt)= 3,0	1.749									1.749
3.5	3.000	1.749	-1.056	3.250	1.485	-0.709	3.250	1.571	-0.965	3.500
(t + Δt)= 3,5	1.347									1.347
4.0	3.500	1.347	-0.791	3.750	1.149	-0.531	3.750	1.214	-0.705	4.000
(t + Δt)= 4,0	1.047									1.047
4.5	4.000	1.047	-0.565	4.250	0.906	-0.379	4.250	0.953	-0.502	4.500
(t + Δt)= 4,5	0.834									0.834
5.0	4.500	0.834	-0.403	4.750	0.733	-0.270	4.750	0.766	-0.362	5.000
(t + Δt)= 5,0	0.681									0.681
5.5	5.000	0.681	-0.295	5.250	0.607	-0.198	5.250	0.632	-0.269	5.500
(t + Δt)= 5,1	0.569									0.569
6.0	5.500	0.569	-0.745	5.750	0.383	-0.495	5.750	0.445	-0.580	6.000
(t + Δt)= 5,2	0.298									0.298
6.5	6.000	0.298	-0.392	6.250	0.200	-0.254	6.250	0.234	-0.302	6.500
(t + Δt)= 5,3	0.157									0.157
7.0	6.500	0.157	-0.211	6.750	0.104	-0.129	6.750	0.125	-0.158	7.000
(t + Δt)= 5,4	0.084									0.084
7.5	7.000	0.084	-0.118	7.250	0.054	-0.063	7.250	0.068	-0.084	7.500
(t + Δt)= 5,5	0.045									0.045
8.0	7.500	0.045	-0.071	7.750	0.028	-0.028	7.750	0.038	-0.045	8.000
(t + Δt)= 5,6	0.026									0.026
8.5	8.000	0.026	-0.047	8.250	0.014	-0.010	8.250	0.023	-0.025	8.500
(t + Δt)= 5,7	0.015									0.015

ammonium



C1 1.46
C2 0.8

Danau	C(t) g/m ³	W _i g/hari	Q _i m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	λ _i hari ⁻¹
S. Baru1	1.46	0	12092	10000	2	5000	0.01	0.183	1.3972

initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{danau}} \quad \text{g/m}^3 \\ c_1(t) &= 1.46 \quad \text{g/m}^3 \end{aligned}$$

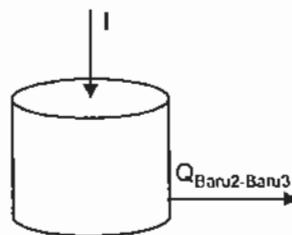
$$c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(t, c_1(t)) \\ &= -\lambda_1 c_1 \\ t &= 0.5 \text{ hr} \\ &= 0 \\ c_1(t) &= 1.46 \end{aligned}$$

$$\begin{aligned} k_{11} &= f(t, c_1(t)) \\ &= -\lambda_1 c_1 \\ k_{21} &= f(t + 1/2 \Delta t, c_1(t) + 1/2 \Delta t k_{11}) \\ &= -\lambda_1 c_1 (t + 1/2 \Delta t k_{11}) \\ k_{31} &= f(t + 1/2 \Delta t, c_1(t) + 1/2 \Delta t k_{21}) \\ &= -\lambda_1 c_1 (t + 1/2 \Delta t k_{21}) \\ k_{41} &= f(t + \Delta t, c_1(t) + \Delta t k_{31}) \\ &= -\lambda_1 c_1 (t + \Delta t k_{31}) \end{aligned}$$

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t + Δt)				
t = 0	1.460													
0.5	0.728	0.000	1.460	-2.040	0.250	0.950	-1.327	0.250	1.128	-1.576	0.500	0.672	-0.939	0.728
(t + Δt)=0,5	0.728													
1.0	0.409	0.500	0.728	-1.017	0.750	0.219	-0.306	0.750	0.651	-0.910	1.000	0.273	-0.381	0.409
(t + Δt)=1,0	0.409													
1.5	0.204	1.000	0.409	-0.571	1.250	0.266	-0.371	1.250	0.316	-0.441	1.500	0.188	-0.263	0.204
(t + Δt)=1,5	0.204													
2.0	0.102	1.500	0.204	-0.285	1.750	0.133	-0.185	1.750	0.157	-0.220	2.000	0.094	-0.131	0.102
(t + Δt)=2,0	0.102													
2.5	0.051	2.000	0.102	-0.142	2.250	0.066	-0.092	2.250	0.078	-0.110	2.500	0.047	-0.065	0.051
(t + Δt)=2,5	0.051													
3.0	0.022	2.500	0.051	-0.071	2.500	0.033	-0.046	2.500	0.039	-0.055	3.000	0.051	-0.071	0.022
(t + Δt)=3,0	0.022													
3.5	0.008	3.000	0.022	-0.031	3.000	0.022	-0.031	3.000	0.014	-0.020	3.500	0.022	-0.031	0.008
(t + Δt)=3,5	0.008													
4.0	0.003	3.500	0.008	-0.012	3.500	0.008	-0.012	3.500	0.005	-0.008	4.000	0.008	-0.012	0.003
(t + Δt)=4,0	0.003													
4.5	0.001	4.000	0.003	-0.005	4.000	0.003	-0.005	4.000	0.002	-0.003	4.500	0.003	-0.005	0.001
(t + Δt)=4,5	0.001													
5.0	0.000	4.500	0.001	-0.002	4.500	0.001	-0.002	4.500	0.001	-0.001	5.000	0.001	-0.002	0.000
(t + Δt)=5,0	0.000													
		5.000	0.000	-0.001	5.000	0.000	-0.001	5.000	0.000	0.000	0.000	0.000	-0.001	0.000

Amonium 2



C1 1.46
C2 0.8

Danau	$C(t)$ g/m ³	W_i	Q_i m ³ /h	V m ³	H m	A m ²	vs m/har	k hari ⁻¹	λ_4 hari ⁻¹
S.Baru 2	0.8	0	3381	20000	2	10000	0.01	0.18	0.36

initial condition

$$t = 0$$

$$c(t) = c_{\text{Danau}} \text{ g/m}^3$$

$$c_i(t) = 0.8 \text{ g/m}^3 \quad c_i(t + \Delta t) = c_i(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady

$$\frac{dc_i}{dt} = f(t, c_i(t)) = -\lambda_1 c_i \quad k_{11} = f(t, c(t)) = -\lambda_1 c_i (t + 1/2 \Delta t k_{11})$$

$$k_{21} = f(t + 1/2 \Delta t, c(t)) = -\lambda_1 c_i (t + 1/2 \Delta t k_{21})$$

$$k_{31} = f(t + \Delta t, c(t)) = -\lambda_1 c_i (t + \Delta t k_{31})$$

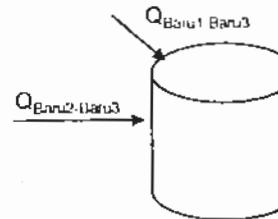
$$k_{41} = f(t + \Delta t, c(t) + \Delta t) = -\lambda_1 c_i (t + \Delta t k_{41}) \quad 0.041667$$

$$\Delta t = 0.5 \text{ hr}$$

$$t = 0$$

$$c_i(t) = 0.8$$

Δt 0.5	$c_i(t)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_i(t + \Delta t)$
$t = 0$	0.8									0.800
0.5	0.000	0.8000	-0.286	0.250	0.729	-0.260	0.250	0.735	-0.262	0.500
$(t + \Delta t) = 0,5$	0.6692									0.669
1.0	0.5	0.6692	-0.239	0.750	0.550	-0.196	0.750	0.620	-0.221	1.000
$(t + \Delta t) = 1,0$	0.5630									0.563
1.5	1.0	0.5630	-0.201	1.250	0.513	-0.183	1.250	0.517	-0.185	1.500
$(t + \Delta t) = 1,5$	0.4710									0.471
2.0	1.5	0.4710	-0.168	1.750	0.429	-0.153	1.750	0.433	-0.155	2.000
$(t + \Delta t) = 2,0$	0.3940									0.394
2.5	2	0.3940	-0.141	2.250	0.359	-0.128	2.250	0.362	-0.129	2.500
$(t + \Delta t) = 2,5$	0.3296									0.329
3.0	2.5	0.3296	-0.118	2.500	0.300	-0.107	2.500	0.303	-0.108	3.000
$(t + \Delta t) = 3,0$	0.2741									0.274
3.5	3.0	0.2741	-0.098	3.000	0.274	-0.098	3.000	0.250	-0.089	3.500
$(t + \Delta t) = 3,5$	0.2266									0.227
4.0	3.5	0.2266	-0.081	3.500	0.227	-0.081	3.500	0.206	-0.074	4.000
$(t + \Delta t) = 4,0$	0.1873									0.187
4.5	4.0	0.1873	-0.067	4.000	0.187	-0.067	4.000	0.171	-0.061	4.500
$(t + \Delta t) = 4,5$	0.1549									0.155
5.0	4.5	0.1549	-0.055	4.500	0.155	-0.055	4.500	0.141	-0.050	5.000
$(t + \Delta t) = 5,0$	0.1281									0.128
5.0	5.0	0.1281	-0.046	5.000	0.128	-0.046	5.000	0.117	-0.042	0.000



Danau	C (l) g/m³	W ₁ g/hari	Q ₁ m³/hari	V m³	II m	A m²	v m/hari	k hari⁻¹	λ ₁ hari⁻¹
S. Baru 1	1.46	0	12092.29	10000	2	5000	0.01	0.183	1.397
S. Baru 2	0.8	0	3381.41	20000	2	10000	0.01	0.183	0.357
S. Baru 3	0.27	0	15473.70	12500	2.5	5000	0.01	0.183	1.425

$$\frac{c_4(t)}{dt} = \frac{W_1/V}{+} + \frac{Q_{14}/V_1}{+} c_{14} - \lambda_4 c_4$$

c_{14}

$$k_{14} = f(l, c(l))$$

$$k_{24} = f(l + 1/2 \Delta t, c(l))$$

$$k_{34} = f(l + 1/2 \Delta t, c(l))$$

$$k_{43} = f(l + 1/2 \Delta t, c(l) + \Delta U)$$

$$c_4(l + \Delta t) = c_4(l) + \frac{1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t}{W_1/V + Q_{14}/V_1 c_{14} + Q_{34}/V_3 c_{34}}$$

$$k_{14} = f(l + 1/2 \Delta t, c(l))$$

$$k_{24} = f(l + 1/2 \Delta t, c(l))$$

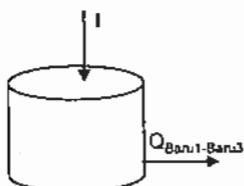
$$k_{34} = f(l + 1/2 \Delta t, c(l))$$

$$k_{43} = f(l + 1/2 \Delta t, c(l) + \Delta U)$$

initial condition

$l = 0$	$c(l) = c_{\text{daran}} \text{ g/m}^3$
$c(l) = 0.27 \text{ g/m}^3$	

Δt 0.5	$c_4(t)$	f	k_{14}	f	k_{24}	f	k_{34}	f	k_{43}	$c_4(t + \Delta t)$
= 0	0.270									0.270
0.5	0.000	0.270	1.516	0.250	0.649	0.347	0.250	0.357	0.980	0.500
$(l + \Delta t) = 0.5$	0.604421712	0.5	0.604	0.132	0.750	0.637	-0.550	0.750	0.467	0.227
$(l + \Delta t) = 1.0$	0.511699738	1.0	0.512	-0.140	1.250	0.477	-0.271	1.250	0.444	-0.163
$(l + \Delta t) = 1.5$	0.402154433	1.5	0.402	-0.247	1.750	0.340	-0.252	1.750	0.339	-0.220
$(l + \Delta t) = 2.0$	0.283192822	2	0.283	-0.214	2.250	0.230	-0.187	2.250	0.237	-0.181
$(l + \Delta t) = 2.5$	0.190542062	2.5	0.191	-0.155	2.750	0.152	-0.126	2.750	0.159	-0.128
$(l + \Delta t) = 3.0$	0.130048882	3	0.130	-0.112	3.250	0.102	-0.072	3.250	0.112	-0.100
$(l + \Delta t) = 3.5$	0.0885552528	3.5	0.089	-0.078	3.750	0.069	-0.050	3.750	0.076	-0.067
$(l + \Delta t) = 4.0$	0.060104767	4	0.060	-0.050	4.250	0.048	-0.032	4.250	0.052	-0.043
$(l + \Delta t) = 4.5$	0.041799942	4.5	0.042	-0.032	4.750	0.034	-0.021	4.750	0.037	-0.027
$(l + \Delta t) = 5.0$	0.030123642	5	0.030	-0.021	5.250	0.025	-0.013	5.250	0.027	-0.018
$(l + \Delta t) = 5.1$	0.022512199	5.5	0.023	-0.032	5.750	0.014	-0.021	5.750	0.017	-0.025
$(l + \Delta t) = 5.2$	0.01107166	6	0.011	-0.016	6.250	0.007	-0.010	6.250	0.009	-0.012
$(l + \Delta t) = 5.3$	0.005445121	6.5	0.005	-0.008	6.750	0.004	-0.005	6.750	0.004	-0.006
$(l + \Delta t) = 5.4$	0.002677949	7	0.003	-0.004	7.250	0.002	-0.002	7.250	0.002	-0.003
$(l + \Delta t) = 5.5$	0.001317035	7.5	0.001	-0.002	7.750	0.001	-0.001	7.750	0.001	-0.002
$(l + \Delta t) = 5.6$	0.000647727	8	0.001	-0.001	8.250	0.000	-0.001	8.250	0.000	-0.001
$(l + \Delta t) = 5.7$	0.000318557									0.000



C1 C2
1677 1455

Danau	C (t) g/m ³	W _i g/hari	Q _i m ³ /hari	V m ³	H m	A m ²	v _S m/hari	k hari ⁻¹	λ _i hari ⁻¹
S. Baru1	1677	0	12082.29	10000	2	5000	0.01	0.123	1.337229

initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{dau}} \quad \text{g/m}^3 \\ c_1(t) &= 1677 \quad \text{g/m}^3 \end{aligned}$$

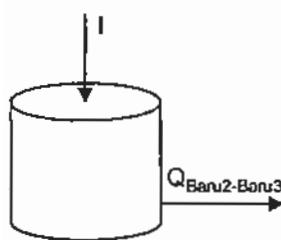
$$c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(l, c_1(t)) = -\lambda_1 c_1 \\ k_{11} &= f(l, c(l)) \\ k_{21} &= f(l + 1/2\Delta t, c(l) + 1/2\Delta t k_{11}) \\ k_{31} &= f(l + 1/2\Delta t, c(l) + 1/2\Delta t k_{21}) \\ k_{41} &= f(l + \Delta t, c(l) + \Delta t k_{31}) \end{aligned}$$

$$\begin{aligned} &= -\lambda_1 c_1(l) \\ &= -\lambda_1 c_1(l + 1/2 \Delta t k_{11}) \\ &= -\lambda_1 c_1(l + 1/2 \Delta t k_{21}) \\ &= -\lambda_1 c_1(l + \Delta t k_{31}) \end{aligned}$$

$$\begin{aligned} dt &= 0.5 \text{ hr} \\ t &= 0 \\ c_1(t) &= 1677 \end{aligned}$$

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t + Δt)
t = 0	1677									1677
0.5	0,000	1677.000	-2242.533	0.250	1116.367	-1492.838	0.250	1303.791	-1743.466	0.500
(l + Δt)=0,5	881.0026707									881.00:
1.0	0.5	881.0026707	-1151.358	0.750	285.324	-381.543	0.750	765.617	-1023.805	1.000
(l + Δt)= 1,0	491.9292378									491.92:
1.5	1.0	491.9292378	-857.822	1.250	327.474	-437.907	1.250	382.452	-511.426	1.500
(l + Δt)= 1,5	252.5655263									252.56:
2.0	1.5	252.5655263	-337.738	1.750	188.131	-224.830	1.750	196.358	-262.576	2.000
(l + Δt)= 2,0	129.6717905									129.67:
2.5	2	129.6717905	-173.401	2.250	88.322	-115.432	2.250	100.814	-134.811	2.500
(l + Δt)= 2,5	66.57588428									66.57:
3.0	2.5	66.57588428	-89.027	2.500	44.319	-59.265	2.500	51.760	-69.215	3.000
(l + Δt)= 3,0	30.32479623									30.32:
3.5	3.0	30.32479623	-40.551	3.000	30.325	-40.551	3.000	20.187	-26.995	3.500
(l + Δt)= 3,5	12.30862442									12.30:
4.0	3.5	12.30862442	-18.459	3.500	12.309	-18.459	3.500	8.194	-10.957	4.000
(l + Δt)= 4,0	4.995985268									4.99:
4.5	4.0	4.995985268	-6.681	4.000	4.996	-6.681	4.000	3.326	-4.447	4.500
(l + Δt)= 4,5	2.027835762									2.02:
5.0	4.5	2.027835762	-2.712	4.500	2.028	-2.712	4.500	1.350	-1.805	5.000
(l + Δt)= 5,0	0.823084468									0.82:
5.0	5.0	0.823084468	-1.101	5.000	0.823	-1.101	5.000	0.548	-0.733	0.000
										0.33-



C1 1677
C2 1455

Danau	C (t) g/m³	W _i g/hari	Q _i m³/hari	V m³	H m	A m²	vs m/h	k hari⁻¹	λ _i hari⁻¹
S.Baru 2	1455	0	3381.4	20000	2	10000	0	0.123	0.2971

initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{dau}} \quad \text{g/m}^3 \\ c_1(t) &= 1455.4 \quad \text{g/m}^3 \end{aligned}$$

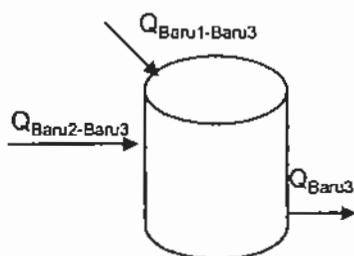
$$c_1(1 + \lambda_i) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(t, c_1) = -\lambda_1 c_1 \\ dt &= 0.5 \text{ hr} \\ t &= 0 \\ c_1(t) &= 1455.4 \end{aligned}$$

$$\begin{aligned} k_{11} &= f(t, c_1) = -\lambda_1 c_1(t) \\ k_{21} &= f(t + 1/2 \Delta t, c_1(t) + 1/2) = -\lambda_1 c_1(t + 1/2 \Delta t k_{11}) \\ k_{31} &= f(t + 1/2 \Delta t, c_1(t) + 1/2) = -\lambda_1 c_1(t + 1/2 \Delta t k_{21}) \\ k_{41} &= f(t + \Delta t, c_1(t) + \Delta t k_{31}) = -\lambda_1 c_1(t + \Delta t k_{31}) \end{aligned}$$

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t + Δt)
t = 0	1455.40									1455.40
0.5	1254.51	0.00	1455.40	-432.36	0.25	1347.31	-400.25	0.25	1355.34	-402.63
(t + Δt)=0,5	1254.51	0.50	1254.51	-372.68	0.75	1068.17	-317.32	0.75	1175.18	-349.11
1.0	1085.65	1.00	1085.65	-322.51	1.25	1005.02	-298.56	1.25	1011.01	-300.34
(t + Δt)= 1,0	1085.65	1.50	935.80	-278.00	1.75	866.30	-257.35	1.75	871.46	-258.88
1.5	935.80	2.00	806.63	-239.63	2.25	746.72	-221.83	2.25	751.17	-223.15
(t + Δt)= 1,5	935.80	2.50	695.29	-206.55	2.50	643.65	-191.21	2.50	647.49	-192.35
2.0	806.63	3.00	596.94	-177.33	3.00	596.94	-177.33	3.00	552.60	-164.16
(t + Δt)= 2,0	806.63	3.50	596.94	-151.64	3.50	510.47	-151.64	3.50	472.56	-140.38
2.5	695.29	4.00	510.47	-129.68	4.00	436.52	-129.68	4.00	404.10	-120.05
(t + Δt)= 2,5	695.29	4.50	436.52	-110.89	4.50	373.29	-110.89	4.50	345.56	-102.66
3.0	596.94	5.00	373.29	-94.83	5.00	319.21	-94.83	5.00	295.51	-87.79
(t + Δt)= 3,0	596.94	5.50	319.21	-79.00	5.50	273.21	-79.00	5.50	253.21	-71.00
3.5	510.47	6.00	273.21	-64.00	6.00	238.21	-64.00	6.00	223.21	-58.00
(t + Δt)= 3,5	510.47	6.50	238.21	-51.00	6.50	203.21	-51.00	6.50	193.21	-46.00
4.0	436.52	7.00	203.21	-40.00	7.00	173.21	-40.00	7.00	163.21	-36.00
(t + Δt)= 4,0	436.52	7.50	173.21	-31.00	7.50	143.21	-31.00	7.50	133.21	-28.00
4.5	373.29	8.00	143.21	-24.00	8.00	113.21	-24.00	8.00	103.21	-22.00
(t + Δt)= 4,5	373.29	8.50	113.21	-18.00	8.50	83.21	-18.00	8.50	73.21	-16.00
5.0	319.21	9.00	83.21	-13.00	9.00	53.21	-13.00	9.00	43.21	-11.00
(t + Δt)= 5,0	319.21	9.50	53.21	-8.00	9.50	23.21	-8.00	9.50	13.21	-7.00

TSS-3



Danau	$C(t)$ g/m ³	W_i g/hari	Q_i m ³ /hari	V m ³	H m	A m ²	v m/h	k hari ⁻¹	λ_i hari ⁻¹
S.Baru 1	1677	0	12092.29	10000	2	5000	0.01	0.123	1.337
S. Baru2	1455	0	3381.408	20000	2	10000	0.01	0.123	0.297
S. Baru3	1248	0	15473.7	12500	2.5	5000	0.01	0.123	1.365

$$\frac{dc_4}{dt} = \frac{W_i}{V} + -\lambda_4 c_4$$

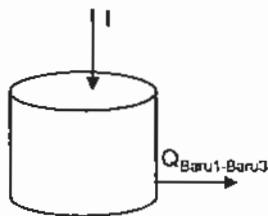
initial condition

$$\begin{aligned} c_4(0) &= 0 \\ c_4(t) &= c_{\text{dau}} \quad \text{g/m}^3 \\ &= 1248 \quad \text{g/m}^3 \end{aligned}$$

$$\begin{aligned} c_4(t + \Delta t) &= c_4(t) + \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4) \Delta t \\ k_{14} &= f(t, c(t)) \\ k_{24} &= f(t + 1/2 \Delta t, c(t)) \\ k_{34} &= f(t + 1/2 \Delta t, c(t)) \\ k_{43} &= f(t + \Delta t, c(t) + \Delta t) \end{aligned}$$

Δt 0.5	$c_4(t)$	f	k_{14}	f	k_{24}	f	k_{34}	f	k_{44}	$c_4(t + \Delta t)$
t = 0	1248.00									1248.00
0.5	1222.26	0.00	1248.00	570.55	0.25	1390.64	-320.34	0.25	1167.91	211.65
(t + Δt) = 1.0	910.01	0.50	1222.26	-415.01	0.75	1118.51	-1001.03	0.75	972.00	-202.19
(t + Δt) = 1.5	671.10	1.00	910.01	-463.66	1.25	794.09	-517.95	1.25	780.52	-431.93
(t + Δt) = 2.0	469.12	1.50	671.10	-452.36	1.75	558.01	-411.85	1.75	568.14	-390.67
(t + Δt) = 2.5	322.30	2.00	469.12	-347.12	2.25	382.34	-291.22	2.25	396.31	-292.02
(t + Δt) = 3.0	227.39	2.50	322.30	-241.85	2.75	261.84	-194.97	2.75	273.56	-201.32
(t + Δt) = 3.5	162.75	3.00	227.39	-172.78	3.25	184.20	-113.82	3.25	198.94	-153.69
(t + Δt) = 4.0	117.77	3.50	162.75	-120.95	3.75	132.52	-79.68	3.75	142.83	-105.15
(t + Δt) = 4.5	87.69	4.00	117.77	-80.90	4.25	97.54	-53.29	4.25	104.45	-70.21
(t + Δt) = 5.0	67.52	4.50	87.69	-54.13	4.75	74.16	-35.66	4.75	78.78	-47.47
(t + Δt) = 5.5	53.59	5.00	67.52	-37.19	5.25	58.22	-24.50	5.25	61.39	-33.17
(t + Δt) = 6.0	41.55	5.50	53.59	-23.15	5.75	35.31	-18.19	5.75	41.55	-56.71
(t + Δt) = 6.5	27.14	6.00	41.55	-13.05	6.25	17.88	-12.41	6.25	21.04	-28.72
(t + Δt) = 7.0	13.75	6.50	27.14	-7.05	6.75	9.06	-12.36	6.75	10.66	-14.55
(t + Δt) = 7.5	6.95	7.00	13.75	-1.77	6.75	4.59	-6.26	6.75	5.40	-7.37
(t + Δt) = 8.0	3.53	7.50	6.96	-9.50	7.25	2.32	-3.17	7.75	2.73	-3.73
(t + Δt) = 8.5	1.79	8.00	3.53	-4.81	7.75	1.18	-1.61	8.25	1.38	-1.89

Amonium



C1 1.46
C2 0.8

Danau	C (t) g/m³	W _i g/hari	Q _i m³/hari	V m³	H m	A m²	v _s m/hari	k hari⁻¹	λ _i hari⁻¹
S. Barul	1.46	0	12092	10000	2	5000	0.01	0	1.2142

initial condition

$$t = 0$$

$$c_i(t) = c_{\text{danau}} \text{ g/m}^3$$

$$c_i(t) = 1.46 \text{ g/m}^3$$

$$c_i(t + \Delta t) = c_i(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady state condition:

$$\frac{dc_i}{dt} = f(t, c_i(t)) = -\lambda_1 c_i$$

$$k_{11} = f(t, c_i(t)) = -\lambda_1 c_i$$

$$k_{21} = f(t + 1/2 \Delta t, c_i(t) + 1/2 \Delta t k_{11}) = -\lambda_1 c_i$$

$$k_{31} = f(t + 1/2 \Delta t, c_i(t) + 1/2 \Delta t k_{21}) = -\lambda_1 c_i$$

$$k_{41} = f(t + \Delta t, c_i(t) + \Delta t k_{31}) = -\lambda_1 c_i$$

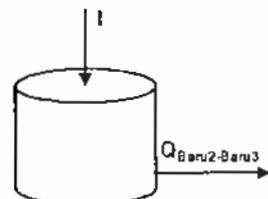
$$dt = 0.5 \text{ hr}$$

$$t = 0$$

$$c_i(t) = 1.46$$

Δt 0.5	c _i (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c _i (t + Δt)
t = 0	1.460									
0.5	0.796	0.000	1.460	-1.773	0.250	1.017	-1.235	0.250	1.151	-1.398
(t + Δt) = 0.5	0.796									0.500
1.0	0.500	0.796	-0.967	0.750	0.313	-0.380	0.750	0.702	-0.852	1.000
(t + Δt) = 1.0	0.473									0.371
1.5	0.258	1.000	0.473	-0.574	1.250	0.329	-0.400	1.250	0.373	-0.453
(t + Δt) = 1.5	0.258									1.500
2.0	0.141	1.500	0.258	-0.313	1.750	0.180	-0.218	1.750	0.204	-0.247
(t + Δt) = 2.0	0.141									2.000
2.5	0.077	2.000	0.141	-0.171	2.250	0.098	-0.119	2.250	0.111	-0.135
(t + Δt) = 2.5	0.077									2.500
3.0	0.038	2.500	0.077	-0.093	2.500	0.053	-0.065	2.500	0.061	-0.074
(t + Δt) = 3.0	0.038									3.000
3.5	0.017	3.000	0.038	-0.046	3.000	0.038	-0.048	3.000	0.027	-0.032
(t + Δt) = 3.5	0.017									3.500
4.0	0.008	3.500	0.017	-0.021	3.500	0.017	-0.021	3.500	0.012	-0.015
(t + Δt) = 4.0	0.008									4.000
4.5	0.004	4.000	0.008	-0.010	4.000	0.008	-0.010	4.000	0.005	-0.007
(t + Δt) = 4.5	0.004									4.500
5.0	0.002	4.500	0.004	-0.004	4.500	0.004	-0.004	4.500	0.002	-0.003
(t + Δt) = 5.0	0.002									5.000

Ammonium 2



Danau	C (t) g/m ³	W _i g/hari	Q _t m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	λ ₄ hari ⁻¹
S.Baru 2	0.8	0	3381.41	15000	2	7500	0.01	0	0.23043

initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{max}} \quad \text{g/m}^3 \\ c_1(t) &= 0.8 \quad \text{g/m}^3 \quad c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t \end{aligned}$$

Steady

$$\begin{array}{lll} \frac{dc_1}{dt} & = f(t, c_1(t)) & = -\lambda_1 c_1 \\ & & k_{21} = f(t + 1/2\Delta t, c_1) + 1/2\Delta t k_{11} \\ & & k_{31} = f(t + 1/2\Delta t, c_1) + 1/2\Delta t k_{21} \\ dt & = 0.5 \text{ hr} & k_{41} = f(t + \Delta t, c_1) + \Delta t k_{31} \\ & & = -\lambda_1 c_1 (t + 1/2 \Delta t k_{11}) \\ & & = -\lambda_1 c_1 (t + 1/2 \Delta t k_{21}) \\ & & = -\lambda_1 c_1 (t + \Delta t k_{31}) \end{array}$$

$$dt = 0.5 \text{ hr} \quad k_{41} = f(1 + \Delta t, c_1) + \Delta t k_{11} = -\lambda_1 c_1 (1 + \Delta t k_{11})$$

$$t = 0$$

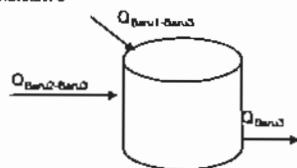
$$c_1(t) = 0.8$$

At	$s_1(t)$
----	----------

at 05

Δt	$c_1(t)$	f_{11}		k_{11}	f_{21}		k_{21}	f_{31}		k_{31}	f_{41}		k_{41}	$c_1(t + \Delta t)$
0.5														
1 = 0	0.80													
0.5	0.71	0.00	0.80	-0.18	0.25	0.75	-0.17	0.25	0.76	-0.17	0.50	0.71	-0.16	0.71
(t + Δt)=0,5	0.71													
1.0	0.64	0.50	0.71	-0.16	0.75	0.63	-0.15	0.75	0.68	-0.16	1.00	0.63	-0.15	0.64
(t + Δt)= 1.0	0.64													
1.5	0.57	1.00	0.64	-0.15	1.25	0.60	-0.14	1.25	0.60	-0.14	1.50	0.57	-0.13	0.57
(t + Δt)= 1,5	0.57													
2.0	0.51	1.50	0.57	-0.13	1.75	0.53	-0.12	1.75	0.54	-0.12	2.00	0.51	-0.12	0.51
(t + Δt)= 2,0	0.51													
2.5	0.45	2.00	0.51	-0.12	2.25	0.48	-0.11	2.25	0.48	-0.11	2.50	0.45	-0.10	0.45
(t + Δt)= 2,5	0.45													
3.0	0.40	2.50	0.45	-0.10	2.50	0.42	-0.10	2.50	0.43	-0.10	3.00	0.45	-0.10	0.40
(t + Δt)= 3,0	0.40													
3.5	0.36	3.00	0.40	-0.09	3.00	0.40	-0.09	3.00	0.38	-0.09	3.50	0.40	-0.09	0.36
(t + Δt)= 3,5	0.36													
4.0	0.32	3.50	0.36	-0.08	3.50	0.36	-0.08	3.50	0.33	-0.08	4.00	0.36	-0.08	0.32
(t + Δt)= 4,0	0.32													
4.5	0.28	4.00	0.32	-0.07	4.00	0.32	-0.07	4.00	0.30	-0.07	4.50	0.32	-0.07	0.28
(t + Δt)= 4,5	0.28													
5.0	0.25	4.50	0.28	-0.06	4.50	0.28	-0.06	4.50	0.26	-0.06	5.00	0.28	-0.06	0.25
(t + Δt)= 5,0	0.25													
		5.00	0.25	-0.06	5.00	0.25	-0.06	5.00	0.23	-0.05	0.00	0.25	-0.06	0.22

Ammonium 3



Diameter	$C(t)$ g/m ³	W_t g/hari	Q_t m ³ /hari	V m ³	R	A m ²	v m/hari	k hari ⁻¹	λ_t hari ⁻¹
S Baru 1	1.40	0	12092.2859	10000	2	5000	0.01	0	1.214
S Baru 2	0.8	0	3381.408	15000	2	7500	0.01	0	0.230
S Baru 3	0.27	0	15473.6978	15750	2.5	7500	0.01	0	0.829

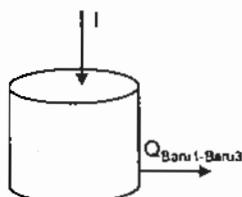
$$\frac{dc}{dt} = \frac{W_t}{V} - Q_1/V c_{1,t} - Q_2/V c_{2,t} - k c_t$$

initial condition

$$c(0) = C_{\text{down}} \quad \text{g/m}^3$$

$$\begin{aligned}
 c_t(t + \Delta t) &= c_t(t) + \frac{1}{V} (k_1 - 2k_2 - 2k_3 + k_4) \Delta t \\
 k_{1,t} &= (t, c(t)) \\
 k_{2,t} &= (t + 1/2\Delta t, c(t) + 1/2\Delta t k_{1,t}) \\
 k_{3,t} &= (t + 1/2\Delta t, c(t) - 1/2\Delta t k_{1,t}) \\
 k_{4,t} &= (t + 1/2\Delta t, c(t) + 1/2\Delta t k_{2,t}) \\
 k_{5,t} &= (t + 1/2\Delta t, c(t) - 1/2\Delta t k_{2,t}) \\
 k_0 &= R \cdot \Delta t \cdot c(t - \Delta t k_{5,t})
 \end{aligned}$$

Δt 0.5	$c_t(t)$	f	$k_{1,t}$	f	$k_{2,t}$	f	$k_{3,t}$	f	$k_{4,t}$	$k_{5,t}$	$c_t(t + \Delta t)$
1 = 0	0.270										
0.5	0.000	0.270	1.722	0.250	0.700	0.619	0.250	0.475	1.169	0.500	0.055
(1 + Δt) = 0.5	0.77581223										0.372
1.0	0.5	0.776	0.481	0.750	0.898	-0.222	0.750	0.720	0.404	1.000	0.978
(1 + Δt) = 1.0	0.82778922										-0.219
1.5	1.0	0.828	0.029	1.250	0.835	-0.159	1.250	0.768	-0.067	1.500	0.794
(1 + Δt) = 1.5	0.77324943										-0.233
2.0	1.5	0.773	-0.201	1.750	0.723	-0.262	1.750	0.708	-0.220	2.000	0.663
(1 + Δt) = 2.0	0.65345782										-0.273
2.5	2	0.653	-0.258	2.250	0.589	-0.262	2.250	0.588	-0.245	2.500	0.531
(1 + Δt) = 2.5	0.52053474										-0.250
3.0	2.5	0.527	-0.242	2.750	0.468	-0.226	2.750	0.470	-0.220	3.000	0.418
(1 + Δt) = 3.0	0.41938978										-0.151
3.5	3	0.419	-0.211	3.250	0.387	-0.187	3.250	0.378	-0.198	3.500	0.322
(1 + Δt) = 3.5	0.33040169										-0.130
4.0	3.5	0.330	-0.173	3.750	0.287	-0.137	3.750	0.298	-0.155	4.000	0.253
(1 + Δt) = 4.0	0.25821015										-0.108
4.5	4	0.258	-0.134	4.250	0.225	-0.106	4.250	0.232	-0.110	4.500	0.189
(1 + Δt) = 4.5	0.20265358										-0.084
5.0	4.5	0.200	-0.101	4.750	0.177	-0.080	4.750	0.183	-0.089	5.000	0.158
(1 + Δt) = 5.0	0.16080377										-0.064
5.5	5	0.161	-0.075	5.250	0.142	-0.060	5.250	0.148	-0.067	5.500	0.127
(1 + Δt) = 5.1	0.12942162										-0.048
6.0	5.5	0.129	-0.107	5.750	0.103	-0.085	5.750	0.108	-0.090	6.000	0.085
(1 + Δt) = 5.2	0.08550612										-0.070
6.5	6	0.086	-0.071	6.250	0.088	-0.056	6.250	0.071	-0.056	6.500	0.058
(1 + Δt) = 5.3	0.05649208										-0.048
7.0	6.5	0.056	-0.047	6.750	0.045	-0.037	6.750	0.047	-0.033	7.000	0.037
(1 + Δt) = 5.4	0.03732313										-0.031
7.5	7	0.037	-0.031	7.250	0.030	-0.025	7.250	0.031	-0.020	7.500	0.024
(1 + Δt) = 5.5	0.0246586										-0.020
8.0	7.5	0.025	-0.020	7.750	0.020	-0.018	7.750	0.021	-0.017	8.000	0.018
(1 + Δt) = 5.6	0.01629141										-0.013
8.5	8	0.016	-0.014	8.250	0.013	-0.011	8.250	0.014	-0.011	8.500	0.011
(1 + Δt) = 5.7	0.01078339										-0.009



C1 1677
C2 1455

Danau	C(t) g/m ³	W _i g/hari	Q _i m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	λ _i hari ⁻¹
S. Baru1	1677	0	12092.3	10000	2	5000	0.01	0	1.214229

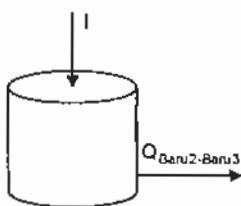
initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{draw}} \text{ g/m}^3 \\ c_1(t) &= 1677 \text{ g/m}^3 \end{aligned}$$

$$c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(t, c_1(t)) = -\lambda_1 c_1 & k_{11} = f(t, c(t)) &= - \\ dt &= 0.5 \text{ hr} & k_{21} = f(t + 1/2\Delta t, c(t) + 1/2\Delta t k) &= -\lambda_1 c_1 (t + 1/2 \Delta t k_{11}) \\ t &= 0 & k_{31} = f(t + 1/2\Delta t, c(t) + 1/2\Delta t k) &= -\lambda_1 c_1 (t + 1/2 \Delta t k_{21}) \\ c_1(t) &= 1677 & k_{41} = f(t + \Delta t, c(t) + \Delta t k_{31}) &= -\lambda_1 c_1 (t + \Delta t k_{31}) \end{aligned}$$

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t + Δt)				
t = 0	1677.0	0.0	1677.0	-2036.3	0.3	1167.9	-1418.1	0.3	1322.5	-1605.8	0.5	874.1	-1061.4	914.9
(t + Δt)=0,5	914.9	0.5	914.9	-1110.9	0.8	359.4	-436.4	0.8	805.8	-978.4	1.0	425.7	-516.9	543.4
1.0	543.4	1.0	543.4	-659.8	1.3	378.5	-459.5	1.3	428.5	-520.3	1.5	283.3	-343.9	296.5
(t + Δt)= 1,0	296.5	1.5	296.5	-360.0	1.8	206.5	-250.7	1.8	233.8	-283.9	2.0	154.5	-187.6	161.7
1.5	161.7	2.0	161.7	-196.4	2.3	112.6	-136.8	2.3	127.5	-154.9	2.5	84.3	-102.4	88.2
(t + Δt)= 1,5	88.2	2.5	88.2	-107.1	2.5	61.4	-74.6	2.5	69.6	-84.5	3.0	48.2	-57.1	43.9
2.0	43.9	3.0	43.9	-53.3	3.0	43.9	-53.3	3.0	30.5	-37.1	3.5	23.9	-33.3	19.9
(t + Δt)= 2,0	19.9	3.5	19.9	-24.2	3.5	19.9	-24.2	3.5	13.9	-16.9	4.0	19.9	-24.2	9.1
2.5	9.1	4.0	9.1	-11.0	4.0	9.1	-11.0	4.0	6.3	-7.7	4.5	9.1	-11.0	4.1
(t + Δt)= 2,5	4.1	4.5	4.1	-5.0	4.5	4.1	-5.0	4.5	2.9	-3.5	5.0	4.1	-5.0	1.9
3.0	1.9	5.0	1.9	-2.3	5.0	1.9	-2.3	5.0	1.3	-1.6	0.0	1.9	-2.3	0.8



C1 9.23
C2 12.32

Danau	C (t) g/m ³	W _t g/hari	Q _t m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	k ₄ hari ⁻¹
S.Baru 2	12.32	0	3381.4	15000	2	7500	0.01	0	0.2304

initial condition

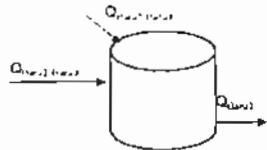
$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{dau}} \quad \text{g/m}^3 \\ c_1(t) &= 12.32 \quad \text{g/m}^3 \end{aligned}$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(t, c_1) = -k_{11} - k_{21} - k_{31} - k_{41} \\ dt &= 0.5 \text{ hr} \\ t &= 0 \\ c_1(t) &= 12.32 \end{aligned}$$

$$\begin{aligned} k_{11} &= f(t, c_1) \\ k_{21} &= f(t + 1/2\Delta t, c(t) + 1/2\Delta t k) \\ k_{31} &= f(t + 1/2\Delta t, c(t) + 1/2\Delta t k) \\ k_{41} &= f(t + \Delta t, c(t) + \Delta t k_{31}) \end{aligned}$$

$$\begin{aligned} &= -\lambda_1 c_1 (t + 1/2 \Delta t k_{11}) \\ &= -\lambda_1 c_1 (t + 1/2 \Delta t k_{21}) \\ &= -\lambda_1 c_1 (t + \Delta t k_{31}) \end{aligned}$$

Δt 0.5	$c_1(t)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_1(t + \Delta t)$
$t = 0$	12.32	0.00	12.32	-2.84	0.25	11.61	-2.68	0.25	11.65	-2.68
$(t + \Delta t) = 0.5$	10.98	0.50	10.98	-2.53	0.75	9.71	-2.24	0.75	10.42	-2.40
$(t + \Delta t) = 1.0$	9.81	1.00	9.81	-2.26	1.25	9.24	-2.13	1.25	9.28	-2.14
$(t + \Delta t) = 1.5$	8.74	1.50	8.74	-2.01	1.75	8.24	-1.90	1.75	8.27	-1.90
$(t + \Delta t) = 2.0$	7.79	2.00	7.79	-1.79	2.25	7.34	-1.69	2.25	7.37	-1.70
$(t + \Delta t) = 2.5$	6.94	2.50	6.94	-1.60	2.50	6.54	-1.51	2.50	6.56	-1.51
$(t + \Delta t) = 3.0$	6.17	3.00	6.17	-1.42	3.00	6.17	-1.42	3.00	5.82	-1.34
$(t + \Delta t) = 3.5$	5.47	3.50	5.47	-1.26	3.50	5.47	-1.26	3.50	5.16	-1.19
$(t + \Delta t) = 4.0$	4.86	4.00	4.86	-1.12	4.00	4.86	-1.12	4.00	4.58	-1.05
$(t + \Delta t) = 4.5$	4.31	4.50	4.31	-0.99	4.50	4.31	-0.99	4.50	4.06	-0.94
$(t + \Delta t) = 5.0$	3.82	5.00	3.82	-0.88	5.00	3.82	-0.88	5.00	3.60	-0.83



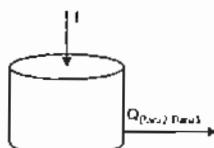
Danar	C (t) km ⁻¹	W _t g/bari	Q _t m ³ /hari	V m ³	H m	A m ²	v m/hari	k bari ⁻¹	k _t bari ⁻¹
S-Batu 1	12.3	0	12097.7099	10000	2	5000	0.01	0	1.214
S-Batu 2	12.32	0	3381.400	15000	2	7500	0.01	0	0.230
S-Batu 3	4.74	0	15472.6979	18750	2.5	7500	0.01	0	0.029

$\frac{d\alpha}{dt}$	τ	W/V	$\times Q_0 V_{\text{initial}}$	$\times Q_0 V_{\text{final}}$	$-k_{\text{rate}}$
$\frac{d\alpha}{dt}$		0.5			
Initial condition					
1	-	0			
$C(t)$	=	C_{initial}		μm^{-3}	
$\alpha(t)$	=	0.74		μm^{-1}	

$c_0(t) = \Delta t$	$c_0(t)$	\times	$1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$
$k_{11} = 10, c_1(t)$	$-$	\times	$-Q_1 V_{11} c_{11}$
$k_{12} = 10, c_1(t)$	$-$	\times	$-Q_2 V_{12} c_{12}$
$k_{13} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{11}$	$-$	\times	$W(t + 1/2 \Delta t)$
$k_{14} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{12}$	$-$	\times	$-1/4 k_1 \quad (t + 1/2 \Delta t) k_{11}$
$k_{15} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{13}$	$-$	\times	$+ Q_1 V_{11} c_{11} \quad (t + 1/2 \Delta t) k_{11}$
$k_{16} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{14}$	$-$	\times	$+ Q_2 V_{12} c_{12} \quad (t + 1/2 \Delta t) k_{12}$
$k_{17} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{15}$	$-$	\times	$+ Q_1 V_{11} c_{11} \quad (t + 1/2 \Delta t) k_{11}$
$k_{18} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{16}$	$-$	\times	$+ Q_2 V_{12} c_{12} \quad (t + 1/2 \Delta t) k_{12}$
$k_{19} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{17}$	$-$	\times	$+ Q_1 V_{11} c_{11} \quad (t + 1/2 \Delta t) k_{11}$
$k_{20} = 10 + 1/2 \Delta t, c_1(t) = 1/2 \Delta t k_{18}$	$-$	\times	$+ Q_2 V_{12} c_{12} \quad (t + 1/2 \Delta t) k_{12}$

Δt	$c_1(t)$	f	k_{14}	I	k_{24}	I	k_{34}	f	k_{44}	$c_1(t + \Delta t)$				
0.5	4.240	0.000	4.240	10.422	0.250	6.046	4.714	0.250	5.418	6.935	0.500	7.707	1.301	7.208330066
$(t + \Delta t) = 0.5$	7.208330067	0.5	7.208	2.586	0.750	7.856	-1.332	0.750	6.725	2.134	1.000	8.275	-1.805	7.305687005
1.0	7.20556701	1.0	7.208	0.011	1.250	7.308	-1.290	1.250	6.983	-0.657	1.500	6.977	-1.805	6.831633092
$(t + \Delta t) = 1.0$	6.831633092	1.5	7.306	-1.590	1.750	6.434	-2.013	1.750	6.328	-1.725	2.000	5.948	-2.057	5.901457215
$(t + \Delta t) = 2.0$	5.90145722	2	5.901	-1.390	2.250	5.404	-2.027	2.250	5.395	-1.900	2.500	4.948	-1.940	4.918249343
$(t + \Delta t) = 2.5$	4.918249343	2.5	4.918	-1.087	2.750	4.848	-1.776	2.750	4.470	-1.736	3.000	4.050	-1.167	4.078267024
$(t + \Delta t) = 3.0$	4.07826702	3	4.078	-1.670	3.250	3.658	-1.331	3.250	3.745	-1.278	3.500	3.795	-1.025	3.326043551
$(t + \Delta t) = 3.5$	3.326043551	3.5	3.348	-1.417	3.750	3.014	-1.124	3.750	3.087	-1.299	4.000	2.719	-0.878	2.772963035
$(t + \Delta t) = 4.0$	2.772963035	4	2.773	-1.141	4.250	2.488	-0.904	4.250	2.547	-1.036	4.500	2.255	-0.711	2.295303446
$(t + \Delta t) = 4.5$	2.295303446	4.5	2.295	-0.903	4.750	2.069	-0.718	4.750	2.116	-0.820	5.000	1.895	-0.543	1.917118228
$(t + \Delta t) = 5.0$	1.917118228	5	1.917	-0.715	5.250	1.738	-0.587	5.250	1.775	-0.651	5.500	1.551	-0.445	1.817317851
$(t + \Delta t) = 5.5$	1.817317851	5.5	1.617	-1.341	5.750	1.582	-1.312	5.750	1.549	-1.318	6.000	1.258	-1.043	0.980338098
$(t + \Delta t) = 6.0$	0.980338098	6	0.980	-0.813	6.250	1.316	-1.421	6.250	1.542	-1.299	6.500	1.020	-1.053	0.372125057
$(t + \Delta t) = 6.5$	0.372125057	6.5	0.372	-0.305	6.750	1.840	-1.576	6.750	1.536	-1.273	7.000	1.290	-1.062	-0.2086420585
$(t + \Delta t) = 7.0$	-0.2086420585	7	-0.205	0.173	7.250	1.962	-1.626	7.250	1.911	-1.253	7.500	1.291	-1.070	-0.783139281
$(t + \Delta t) = 7.5$	-0.783139281	7.5	-0.763	0.633	7.750	2.075	-1.721	7.750	1.882	-1.233	8.000	1.301	-1.079	-1.292615456
$(t + \Delta t) = 8.0$	-1.292615456	8	-1.293	1.072	8.250	2.185	-1.812	8.250	1.464	-1.214	8.500	1.310	-1.096	-1.798180063
$(t + \Delta t) = 8.5$	-1.798180063	8.5	-1.293	1.072	8.250	2.185	-1.812	8.250	1.464	-1.214	8.500	1.310	-1.096	-1.798180063

t	c
0	4240
0.1	720833
0.2	7305567
0.3	6831633
0.4	5901457
0.5	4918269
0.6	4078267
0.7	3368044
0.8	272295
0.9	2295308
1.0	191718
1.1	1617318
1.2	920338
1.3	372125
1.4	-0.20362
1.5	-0.76314
1.6	-29266
1.7	-1784814

C1
C21677
1455

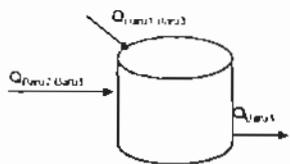
Danau	C (t) g/m³	W _t g/hari	Q _t m³/hari	V m³	H m	A m²	v _s m³/hari	k bar⁻¹	k _t bar⁻¹
S Danau 2	1455.4	0	3381.408	15000	2	7500	0.01	0	0.2434272

initial condition

$$\begin{aligned} I &= 0 \\ c_1(t) &= c_{\text{inital}} = 1455.4 \text{ g/m}^3 \end{aligned}$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= 0 \\ \frac{dc_1}{dt} &= f(t, c_1(t)) = -\lambda_1 c_1 \\ dt &= 0.5 \text{ hr} \\ I &= 0 \\ c_1(t) &= 1455.4 \end{aligned}$$

Δt 0.5	$c_1(0)$	f_{11}	k_{11}	f_{11}	k_{21}	f_{21}	M_{21}	f_{41}	k_{41}	$c_1(t + \Delta t)$
$t = 0$	1455.4	0.000	1455.400	-335.364	0.250	1371.559	-316.045	0.250	1376.389	-317.157
$(t + \Delta t) = 0.5$	1297.01745	0.5	1297.01745	-298.868	0.750	1147.583	-264.434	0.750	1230.909	-283.635
$(t + \Delta t) = 1.0$	1158.58444	1.0	1158.58444	-266.969	1.250	1091.842	-251.590	1.250	1095.687	-252.476
$(t + \Delta t) = 1.5$	1032.50237	1.5	1032.50237	-237.917	1.750	973.023	-224.211	1.750	976.450	-225.001
$(t + \Delta t) = 2.0$	920.14144	2	920.14144	-212.026	2.250	867.135	-199.811	2.250	870.189	-200.515
$(t + \Delta t) = 2.5$	820.0079079	2.5	820.0079079	-188.952	2.500	772.770	-178.067	2.500	775.491	-178.694
$(t + \Delta t) = 3.0$	729.0550483	3.0	729.0550483	-167.994	3.000	729.056	-167.994	3.000	687.057	-158.317
$(t + \Delta t) = 3.5$	646.6714559	3.5	646.6714559	-149.011	3.500	646.671	-149.011	3.500	609.419	-140.427
$(t + \Delta t) = 4.0$	573.596781	4.0	573.596781	-132.172	4.000	573.597	-132.172	4.000	540.554	-124.558
$(t + \Delta t) = 4.5$	508.7796348	4.5	508.7796348	-117.237	4.500	508.780	-117.237	4.500	479.470	-110.483
$(t + \Delta t) = 5.0$	451.2869063	5.0	451.2869063	-103.989	5.000	451.287	-103.989	5.000	425.290	-97.998

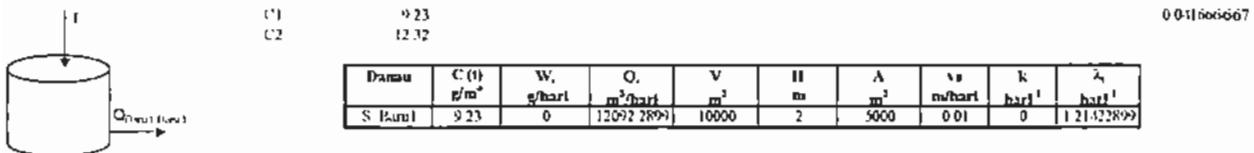


Banau	C(t) g/m³	Wt g/hari	Qt m³/hari	V m³	H m	A m²	v m/hari	k harf'	λt harf'
S Baru 1	1677	0	12092.2899	10000	2	5000	0.01	0	1.214
S Baru 2	1455	0	3301.408	15000	2	7500	0.01	0	0.730
S Baru 3	1248	0	15473.6979	18750	2.5	7500	0.01	0	0.879

$$\begin{aligned}
 \frac{dc}{dt} &= -\frac{W_t}{V} c + \frac{Q_{inlet}}{V} c_{inlet} - \frac{Q_{outlet}}{V} c_{outlet} \\
 \frac{dc}{dt} &= -0.5 c + \frac{Q_{inlet}}{V} c_{inlet} - \frac{Q_{outlet}}{V} c_{outlet} \\
 \text{initial condition} \\
 t &= 0 \\
 c(0) &= 1248 \text{ g/m}^3
 \end{aligned}$$

$$\begin{aligned}
 c_1(t + \Delta t) &= c_1(t) - \frac{W_t}{V} c_1(t) \Delta t + \frac{Q_{inlet}}{V} c_{inlet}(t) \Delta t - \frac{Q_{outlet}}{V} c_{outlet}(t) \Delta t \\
 k_{11} &= (I, c_1(t)) \\
 k_{12} &= f(I + 1/2 \Delta t, c_1(t) + 1/2 \Delta t k_{11}) \\
 k_{13} &= f(I + 1/2 \Delta t, c_1(t) + 1/2 \Delta t k_{12}) \\
 k_{14} &= f(I + \Delta t, c_1(t) + \Delta t k_{13}) \\
 c_2(t) &= c_2(t) - \frac{W_t}{V} c_2(t) \Delta t + \frac{Q_{inlet}}{V} c_{inlet}(t) \Delta t - \frac{Q_{outlet}}{V} c_{outlet}(t) \Delta t \\
 k_{21} &= (I + 1/2 \Delta t, c_2(t)) \\
 k_{22} &= f(I + 1/2 \Delta t, c_2(t) + 1/2 \Delta t k_{21}) \\
 k_{23} &= f(I + 1/2 \Delta t, c_2(t) + 1/2 \Delta t k_{22}) \\
 k_{24} &= f(I + \Delta t, c_2(t) + \Delta t k_{23})
 \end{aligned}$$

Δt	$c_d(t)$	f	k_{11}	f	k_{12}	f	k_{13}	f	k_{14}	f	k_{21}	$c_d(t + \Delta t)$	
0.5	1248.000												
0.5	1248.000	0.000	1248.000	1321.047	0.250	1578.261	412.692	0.250	1351.173	788.959	0.500	1642.480	-12.708
0 + Δt) = 0.5	1567.3015												
1.0	0.5	1567.303	107.265	0.750	1584.110	-620.308	0.750	1402.226	89.021	1.000	1601.814	-553.162	
(0 + Δt) = 1.0	1431.5972												
1.5	1.0	1431.597	-268.868	1.250	1364.380	-427.649	1.250	1324.685	-333.312	1.500	1264.941	-473.733	
(1 + Δt) = 1.5	1242.98709												
2.0	1.5	1242.987	-439.435	1.750	1133.028	-470.584	1.750	1125.246	-430.304	2.000	1027.735	-458.011	
(1 + Δt) = 2.0	1017.95519												
2.5	2	1017.955	-441.155	2.250	907.666	-421.013	2.250	912.702	-408.479	2.500	814.718	-388.850	
(1 + Δt) = 2.5	810.87287												
3.0	2.5	810.873	-380.881	2.750	715.652	-344.955	2.750	724.634	-341.958	3.000	638.894	-739.095	
(1 + Δt) = 3.0	644.72245												
3.5	3	644.722	-317.258	3.250	565.408	-251.486	3.250	587.051	-290.689	3.500	499.378	-196.700	
(1 + Δt) = 3.5	511.527682												
4.0	3.5	511.528	-254.310	3.750	447.848	-201.594	3.750	451.129	-228.237	4.000	397.409	-159.654	
(1 + Δt) = 4.0	405.389022												
4.5	4	405.389	-195.923	4.250	358.408	-155.305	4.250	366.563	-174.490	4.500	318.140	-123.571	
(1 + Δt) = 4.5	323.79743												
5.0	4.5	323.797	-148.847	4.750	298.508	-117.089	4.750	294.300	-132.503	5.000	257.546	-93.907	
(1 + Δt) = 5.0	281.819227												
5.5	5	281.819	-113.125	5.250	233.538	-88.673	5.250	239.401	-101.087	5.500	211.770	-71.214	
(1 + Δt) = 5.1	214.665323												
6.0	5.5	214.665	-178.014	5.750	170.162	-141.109	5.750	179.388	-148.750	6.000	140.285	-116.334	
(1 + Δt) = 5.2	141.824835												
6.5	6	141.825	-117.510	6.250	112.422	-93.228	6.250	118.518	-98.283	6.500	92.684	-78.859	
(1 + Δt) = 5.3	93.7006687												
7.0	6.5	93.701	-77.703	6.750	74.275	-61.594	6.750	78.302	-64.933	7.000	61.234	-50.779	
(1 + Δt) = 5.4	61.9080472												
7.5	7	61.908	-51.336	7.250	49.072	-40.694	7.250	51.703	-42.000	7.500	40.456	-33.549	
(1 + Δt) = 5.5	40.900015												
8.0	7.5	40.900	-33.917	7.750	32.421	-26.885	7.750	34.179	-28.343	8.000	26.728	-22.165	
(1 + Δt) = 5.6	27.0217742												
8.5	8	27.022	-22.408	8.250	21.420	-17.763	8.250	22.581	-18.726	8.500	17.659	-14.644	
(1 + Δt) = 5.7	17.6527142												



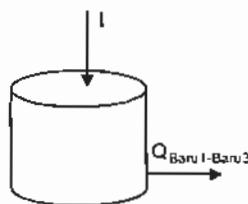
Danau	C (t) g/m ³	W, g/hari	O, m ³ /hari	V m ³	H m	A m ²	N m ³ /hari	k hari ⁻¹	k _i hari ⁻¹
S. Kumb	9.23	0	12092.2899	10000	2	5000	0.01	0	121422899

initial condition

t = 0	c ₁ (t)	c _{1,out} g/m ³	c _{1,r+Δt} g/m ³	c _{1,t}	c _{1,t+Δt}	c _{1,r+Δt}	c _{1,t+Δt}	c _{1,t+Δt}	c _{1,t+Δt}
Steady									
dc ₁ /dt	R(t, c ₁ (t))	-λ ₁ c ₁	k ₁₁ - R(t, c ₁ (t))	-	-	-λ ₁ c ₁ (t)	-	-	-
dt	= 0.5 hr		k ₂₁ - (t + 1/2Δt)c ₁ (t) + 1/2Δtλ ₁₁	-	-	-λ ₁ c ₁ - (t + 1/2Δt)λ ₁₁	-	-	-
t = 0	c ₁ (t)	9.23	k ₃₁ - (t + 1/2Δt)c ₁ (t) + 1/2Δtλ ₂₁	-	-	-λ ₁ c ₁ - (t + 1/2Δt)λ ₂₁	-	-	-
			k ₄₁ - Q(t, c ₁ (t))Δtλ ₁₁	-	-	-λ ₁ c ₁ - (t + Δt)λ ₁₁	-	-	-

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t+Δt)
1 = 0	9.23	0.000	9.230	-11.207	0.250	6.428	-7.805	0.250	7.279	-8.838
0.5	5.04	0.5	5.035	-6.114	0.750	1.978	-2.402	0.750	4.435	-5.385
1.000	0.5	5.035	-6.114	0.750	1.978	-2.402	0.750	4.435	-5.385	1.000
(t + Δt)	3.19	1.000	3.191	-3.875	1.250	2.222	-2.698	1.250	2.516	-3.055
1.5000	1.000	3.191	-3.875	1.250	2.222	-2.698	1.250	2.516	-3.055	1.500
(t + Δt)	1.74	1.000	3.191	-3.875	1.250	2.222	-2.698	1.250	2.516	-3.055
2.0000	1.500	1.500	1.741	-2.314	1.750	1.212	-1.472	1.750	1.373	-1.667
(t + Δt)	0.95	1.500	1.741	-2.314	1.750	1.212	-1.472	1.750	1.373	-1.667
2.5000	2.000	2.000	0.950	-1.153	2.250	0.661	-0.803	2.250	0.749	-0.909
(t + Δt)	0.52	2.000	0.950	-1.153	2.250	0.661	-0.803	2.250	0.749	-0.909
3.0000	2.500	2.500	0.518	-0.629	2.500	0.361	-0.438	2.500	0.409	-0.496
(t + Δt)	0.26	2.500	0.518	-0.629	2.500	0.361	-0.438	2.500	0.409	-0.496
3.5000	3.000	3.000	0.258	-0.313	3.000	0.258	-0.313	3.000	0.179	-0.218
(t + Δt)	0.12	3.000	0.258	-0.313	3.000	0.258	-0.313	3.000	0.179	-0.218
4.0000	3.500	3.500	0.117	-0.162	3.500	0.117	-0.162	3.500	0.081	-0.099
(t + Δt)	0.06	3.500	0.117	-0.162	3.500	0.117	-0.162	3.500	0.081	-0.099
4.5000	4.000	4.000	0.053	-0.065	4.000	0.053	-0.065	4.000	0.037	-0.045
(t + Δt)	0.02	4.000	0.053	-0.065	4.000	0.053	-0.065	4.000	0.037	-0.045
5.0000	4.500	4.500	0.024	-0.029	4.500	0.024	-0.029	4.500	0.017	-0.020
(t + Δt)	0.01	4.500	0.024	-0.029	4.500	0.024	-0.029	4.500	0.017	-0.020
5.5000	5.000	5.000	0.011	-0.013	5.000	0.011	-0.013	5.000	0.008	-0.009

Ammonium



C1 1.46
C2 0.8

Danau	C(t) g/m ³	W _t g/hari	Q _t m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	λ _t hari ⁻¹
S. Baru)	2.72	0	12092	10000	2	5000	0	0	1.2092

initial condition

$$t = 0$$

$$c_1(t) = c_{\text{down}} \quad \text{g/m}^3$$

$$c_1(t) = 2.72 \quad \text{g/m}^3$$

$$c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady state

$$\frac{dc_1}{dt} = f(t, c_1(t)) = -\lambda_1 c_1$$

$$k_{11} = f(t, c_1(t)) = \lambda_1 c_1(t)$$

$$k_{21} = f(t + 1/2\Delta t, c_1(t) + 1/2\Delta t c_1(t)) = -\lambda_1 c_1(t + 1/2\Delta t k_{11})$$

$$k_{31} = f(t + 1/2\Delta t, c_1(t) + 1/2\Delta t c_1(t)) = -\lambda_1 c_1(t + 1/2\Delta t k_{21})$$

$$k_{41} = f(t + \Delta t, c_1(t) + \Delta t k_{31}) = -\lambda_1 c_1(t + \Delta t k_{31})$$

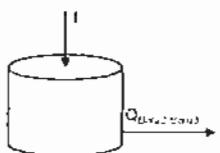
$$\Delta t = 0.5 \text{ hr}$$

$$t = 0$$

$$c_1(t) = 2.72$$

Δt 0.5	c ₁ (t)	f ₁₁	k ₁₁	f ₂₁	k ₂₁	f ₃₁	k ₃₁	f ₄₁	k ₄₁	c ₁ (t + Δt)
1 = 0	2.720									
0.5	0.000	2.720	-3.289	0.250	1.898	-2.295	0.250	2.146	-2.595	0.500
(t + Δt)=0,5	1.488									
1.0	0.500	1.488	-1.799	0.750	0.588	-0.711	0.750	1.310	-1.584	1.000
(t + Δt)=1,0	0.885									
1.5	1.000	0.885	-1.070	1.250	0.617	-0.747	1.250	0.698	-0.845	1.500
(t + Δt)=1,5	0.484									
2.0	1.500	0.484	-0.585	1.750	0.338	-0.408	1.750	0.362	-0.462	2.000
(t + Δt)=2,0	0.265									
2.5	2.000	0.265	-0.320	2.250	0.185	-0.223	2.250	0.209	-0.253	2.500
(t + Δt)=2,5	0.145									
3.0	2.500	0.145	-0.175	2.500	0.101	-0.122	2.500	0.114	-0.138	3.000
(t + Δt)=3,0	0.072									
3.5	3.000	0.072	-0.087	3.000	0.072	-0.087	3.000	0.050	-0.061	3.500
(t + Δt)=3,5	0.033									
4.0	3.500	0.033	-0.040	3.500	0.033	-0.040	3.500	0.023	-0.028	4.000
(t + Δt)=4,0	0.015									
4.5	4.000	0.015	-0.018	4.000	0.015	-0.018	4.000	0.010	-0.013	4.500
(t + Δt)=4,5	0.007									
5.0	4.500	0.007	-0.008	4.500	0.007	-0.008	4.500	0.005	-0.006	5.000
(t + Δt)=5,0	0.003									
	5.000	0.003	-0.004	5.000	0.003	-0.004	5.000	0.002	-0.003	0.000
										0.003
										-0.004
										0.001

Amanah



C1 1.46
C2 0.8

Danau	C (t) g/m³	W, g/hari	Q, m³/hari	V m³	H m	A m²	vs m³/hari	k hari⁻¹	λ₁ hari¹
S Baru 2	2.62	0	3381.408	15000	2	7500	0	0	0.2254272

initial condition

$$\begin{aligned} t &= 0 \\ c(t) &= c_{\text{max}} \quad \text{g/m}^3 \\ c_1(t) &= 2.62 \quad \text{g/m}^3 \end{aligned}$$

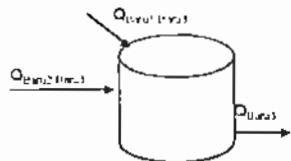
$$c_i(t + \Delta t) = c_i(t) + \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady state

$$\begin{aligned} \frac{dc_1}{dt} &= f(t, c_1(t)) \\ &= -\lambda_1 c_1 - \lambda_2 c_1 (t + 1/2 \Delta t k_{11}) \\ &\quad - \lambda_3 c_1 (t + 1/2 \Delta t k_{21}) \\ &\quad - \lambda_4 c_1 (t + \Delta t k_{31}) \\ &= -\lambda_1 c_1 - \lambda_2 c_1 (t + 1/2 \Delta t k_{11}) \\ &\quad - \lambda_3 c_1 (t + 1/2 \Delta t k_{21}) \\ &\quad - \lambda_4 c_1 (t + \Delta t k_{31}) \end{aligned}$$

$$\begin{aligned} \Delta t &= 0.5 \text{ hr} \\ t &= 0 \\ c_1(t) &= 2.62 \end{aligned}$$

Δt 0.5	$c_1(0)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_1(t + \Delta t)$				
1 = 0	2.62	0.000	7.620	-0.591	0.250	2.472	-0.557	0.250	2.481	-0.559	0.500	2.340	-0.528	2.340725407
0.5	2.340725411	0.5	7.340725411	-0.528	0.750	2.077	-0.468	0.750	2.224	-0.501	1.000	2.090	-0.471	2.095912289
1.0	2.09591229	1.0	2.09591229	-0.472	1.250	1.978	-0.446	1.250	1.984	-0.447	1.500	1.872	-0.422	1.872501964
1.5	1.87250196	1.5	1.87250196	-0.422	1.750	1.767	-0.398	1.750	1.773	-0.400	2.000	1.673	-0.377	1.672905695
2.0	1.6729057	2	1.6729057	-0.377	2.250	1.579	-0.356	2.250	1.584	-0.357	2.500	1.494	-0.337	1.494585063
2.5	1.494585063	2.5	1.49458506	-0.337	2.500	1.410	-0.318	2.500	1.413	-0.319	3.000	1.495	-0.317	1.332275898
3.0	1.332275898	3.0	1.33227589	-0.300	3.000	1.332	-0.300	3.000	1.327	-0.283	3.500	1.332	-0.300	1.184931237
3.5	1.184931237	3.5	1.18493123	-0.267	3.500	1.186	-0.267	3.500	1.118	-0.252	4.000	1.185	-0.267	1.053882336
4.0	1.053882336	4.0	1.05388234	-0.238	4.000	1.054	-0.238	4.000	0.994	-0.224	4.500	1.054	-0.238	0.937326947
4.5	0.937326947	4.5	0.93732695	-0.211	4.500	0.937	-0.211	4.500	0.885	-0.199	5.000	0.937	-0.211	0.833662141
5.0	0.833662141	5.0	0.83366214	-0.183	5.000	0.834	-0.183	5.000	0.787	-0.177	0.000	0.834	-0.183	0.74146227



Danau	C(t) g/m³	W _t g/barl	Q _t m³/barl	V m³	IL m	A m²	v m/barl	k bar⁻¹	λ _t bar⁻¹
S Baru 1	2.72	0	12092.2999	10000	2	5000	0	0	1.209
S Baru 2	2.82	0	2381.408	15000	2	7500	0	0	0.225
S Baru 3	5.90	0	15473.6979	19750	2.5	7500	0	0	0.025

$$\frac{dc}{dt} = -\frac{W_t}{V} c + \frac{Q_t}{V} c_{inj} - \lambda_t c_t$$

$$c_t = 0.5$$

initial condition

$$c(0) = c_{dau}$$

$$c_{inj} = 5.06 \text{ g/m}^3$$

$$c_t(t + \Delta t) = c_t(t) + \frac{1/2 (k_{11} + 2k_{12} + 2k_1 + k_{13}) \Delta t}{W_t/V + Q_t/V c_{inj} - \lambda_t c_t}$$

$$k_{11} = k(t, c(t))$$

$$k_{12} = k(t + 1/2 \Delta t, c(t) + 1/2 \Delta k_{11})$$

$$k_{13} = k(t + 1/2 \Delta t, c(t) + 1/2 \Delta k_{12})$$

$$k_{14} = k(t + 1/2 \Delta t, c(t) + 1/2 \Delta k_{13})$$

$$k_{24} = k(t + \Delta t, c(t) + \Delta k_{14})$$

$$k_{34} = k(t + \Delta t, c(t) + \Delta k_{12})$$

$$k_{44} = k(t + \Delta t, c(t) + \Delta k_{13})$$

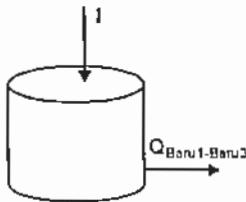
$$W_t = 1/2 (k_{11} + 2k_{12} + 2k_1 + k_{13})$$

$$Q_t = 1/2 (k_{11} + 2k_{12} + 2k_1 + k_{13})$$

$$\lambda_t = 1/2 (k_{11} + 2k_{12} + 2k_1 + k_{13})$$

Δt 0.5	$c_A(t)$	f		k_{14}	f		k_{24}	f		k_{34}	f		k_{44}	$c_A(t + \Delta t)$
1.0	5.960	0.000	5.960	-1.039	0.250	5.700	-1.852	0.250	5.497	-1.382	0.500	5.269	-2.101	5.159357329
(t + Δt)=0.5	5.159357329	0.5	5.158	-3.134	0.750	4.378	-2.432	0.750	4.551	-1.871	1.000	4.324	-2.258	4.0263866523
1.5	4.0263866523	0.5	5.158	-3.134	0.750	4.378	-2.432	0.750	4.551	-1.871	1.000	4.324	-2.258	4.0263866523
(t + Δt)=1.0	4.0263866523	1.0	4.028	-2.807	1.250	3.375	-1.502	1.250	3.628	-1.702	1.500	3.175	-1.638	3.123428527
(t + Δt)=1.5	3.123428527	1.0	4.028	-2.807	1.250	3.375	-1.502	1.250	3.628	-1.702	1.500	3.175	-1.638	3.123428527
2.0	2.37504534	1.5	3.123	-2.138	1.750	2.589	-1.330	1.750	2.781	-1.442	2.000	2.403	-1.300	2.375045339
(t + Δt)=2.0	2.37504534	2	2.375	-1.678	2.250	1.958	-1.036	2.250	2.118	-1.137	2.500	1.807	-0.987	1.791105411
2.5	1.791105411	2	2.375	-1.678	2.250	1.958	-1.036	2.250	2.118	-1.137	2.500	1.807	-0.987	1.791105411
(t + Δt)=2.5	1.791105411	2.5	1.781	-1.284	2.750	1.470	-0.773	2.750	1.598	-0.662	3.000	1.360	-0.611	1.360849525
3.0	1.360849525	2.5	1.781	-1.284	2.750	1.470	-0.773	2.750	1.598	-0.662	3.000	1.360	-0.611	1.360849525
(t + Δt)=3.0	1.360849525	3	1.361	-0.987	3.250	1.114	-0.532	3.250	1.228	-0.688	3.500	1.026	-0.459	1.040214313
3.5	1.040214313	3	1.361	-0.987	3.250	1.114	-0.532	3.250	1.228	-0.688	3.500	1.026	-0.459	1.040214313
(t + Δt)=3.5	1.040214313	3.5	1.040	-0.757	3.750	0.861	-0.395	3.750	0.941	-0.487	4.000	0.782	-0.348	0.799522905
4.0	0.799522905	3.5	1.040	-0.757	3.750	0.861	-0.395	3.750	0.941	-0.487	4.000	0.782	-0.348	0.799522905
(t + Δt)=4.0	0.799522905	4	0.800	-0.579	4.250	0.655	-0.295	4.250	0.728	-0.364	4.500	0.617	-0.254	0.621675303
(t + Δt)=4.5	0.621675303	4.5	0.622	-0.446	4.750	0.510	-0.203	4.750	0.572	-0.267	5.000	0.489	-0.184	0.491471377
5.0	0.491471377	4.5	0.622	-0.446	4.750	0.510	-0.203	4.750	0.572	-0.267	5.000	0.489	-0.184	0.491471377
(t + Δt)=5.0	0.491471377	5	0.481	-0.348	5.250	0.405	-0.142	5.250	0.458	-0.198	5.500	0.393	-0.133	0.395017689
(t + Δt)=5.1	0.395017689	5.5	0.395	-0.328	5.750	0.314	-0.259	5.750	0.330	-0.273	6.000	0.259	-0.214	0.261501343
6.0	0.261501343	5.5	0.395	-0.328	5.750	0.314	-0.259	5.750	0.330	-0.273	6.000	0.259	-0.214	0.261501343
(t + Δt)=5.2	0.261501343	6	0.262	-0.216	6.250	0.208	-0.171	6.250	0.219	-0.180	6.500	0.171	-0.141	0.173110646
6.5	0.173110646	6	0.262	-0.216	6.250	0.208	-0.171	6.250	0.219	-0.180	6.500	0.171	-0.141	0.173110646
(t + Δt)=6.5	0.173110646	6.5	0.173	-0.143	6.750	0.137	-0.113	6.750	0.145	-0.119	7.000	0.113	-0.094	0.114601073
7.0	0.114601073	7	0.115	-0.086	7.250	0.091	-0.075	7.250	0.096	-0.079	7.500	0.075	-0.062	0.075865804
(t + Δt)=7.4	0.075865804	7.5	0.078	-0.083	7.750	0.060	-0.050	7.750	0.063	-0.052	8.000	0.050	-0.041	0.050223092
8.0	0.050223092	8	0.050	-0.041	8.250	0.040	-0.033	8.250	0.042	-0.035	8.500	0.033	-0.027	0.03324764
(t + Δt)=8.5	0.03324764	8.5	0.050	-0.041	8.250	0.040	-0.033	8.250	0.042	-0.035	8.500	0.033	-0.027	0.03324764

Ammonium



C1 1.46
C2 0.8

Danau	$C(t)$ g/m ³	W_t g/hari	Q_t m ³ /hari	V m ³	H m	A m ²	vs m/har	k hari ⁻¹	λ_t hari ⁻¹
S. Baru1	2.62	0	12092	10000	2	5000	0.01	0	1.2142

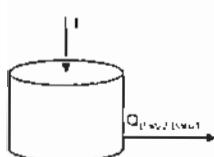
initial condition

$$t = 0 \\ c(t) = c_{\text{dauu}} \text{ g/m}^3 \\ c_1(t) = 2.62 \text{ g/m}^3 \\ c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(c_1) = -\lambda_1 c_1 \\ &\quad k_{11} = f(t, c(t)) = -\lambda_1 c_1 \\ &\quad k_{21} = f(t + 1/2\Delta t, c(t) + 1/2\Delta t, c_1(t)) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{11}) \\ &\quad k_{31} = f(t + 1/2\Delta t, c(t) + 1/2\Delta t, c_1(t)) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{21}) \\ &\quad k_{41} = f(t + \Delta t, c(t) + \Delta t k_{31}, c_1(t)) = -\lambda_1 c_1 (t + \Delta t k_{31}) \end{aligned}$$

$$\Delta t = 0.5 \text{ hr} \\ t = 0 \\ c_1(t) = 2.62$$

Δt 0.5	$c_1(t)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_1(t + \Delta t)$
t = 0	2.620									
0.5	0.000	2.620	-3.181	0.250	1.825	-2.216	0.250	2.066	-2.509	0.500
(t + Δt)=0,5	1.429									
1.0	0.500	1.429	-1.736	0.750	0.562	-0.682	0.750	1.259	-1.529	1.000
(t + Δt)= 1,0	0.849									
1.5	1.000	0.849	-1.031	1.250	0.591	-0.718	1.250	0.670	-0.813	1.500
(t + Δt)= 1,5	0.463									
2.0	1.500	0.463	-0.562	1.750	0.323	-0.392	1.750	0.365	-0.443	2.000
(t + Δt)= 2,0	0.253									
2.5	2.000	0.253	-0.307	2.250	0.176	-0.214	2.250	0.199	-0.242	2.500
(t + Δt)= 2,5	0.138									
3.0	2.500	0.138	-0.167	2.500	0.096	-0.117	2.500	0.109	-0.132	3.000
(t + Δt)= 3,0	0.069									
3.5	3.000	0.069	-0.083	3.000	0.069	-0.063	3.000	0.048	-0.058	3.500
(t + Δt)= 3,5	0.031									
4.0	3.500	0.031	-0.038	3.500	0.031	-0.038	3.500	0.022	-0.026	4.000
(t + Δt)= 4,0	0.014									
4.5	4.000	0.014	-0.017	4.000	0.014	-0.017	4.000	0.010	-0.012	4.500
(t + Δt)= 4,5	0.006									
5.0	4.500	0.006	-0.008	4.500	0.006	-0.008	4.500	0.004	-0.005	5.000
(t + Δt)= 5,0	0.003									
	5.000	0.003	-0.004	5.000	0.003	-0.004	5.000	0.002	-0.002	0.000



C1 1677
C2 1455

Danau	C (n) g/m³	W, m³/harl	O, m³/harl	V m³	H m	A m²	vB m/harl	k harl⁻¹	k _t harl⁻¹
S Baru 2	1455.4	0	3381.408	15000	2	7500	0.01	0	0.2304272

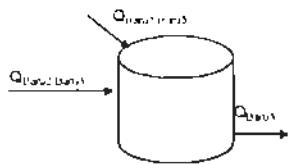
initial condition

$$\begin{aligned} t &= 0 \\ c_1(0) &= c_{1,\text{init}} \quad \text{g/m}^3 \\ c_1(t) &= 1455.4 \quad \text{g/m}^3 \end{aligned}$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(t, c_1(t)) \\ \frac{dc_1}{dt} &= -\lambda_1 c_1 \\ &= k_{11} - f(t, c_1(t)) \\ &= k_{11} - f(t, 1/2\Delta t, c(t)+1/2\Delta t k_{11}) \\ &= k_{11} - f(t+1/2\Delta t, c(t)+1/2\Delta t k_{11}) \\ &= k_{11} - f(t+\Delta t, c(t)+\Delta t k_{11}) \end{aligned}$$

$$\begin{aligned} \Delta t &= 0.5 \text{ hr} \\ t &= 0 \\ c_1(t) &= 1455.4 \end{aligned}$$

$\frac{\Delta t}{0.5}$	$c_1(0)$	f_{11}		k_{11}	f_{11}		k_{11}	f_{11}		k_{11}	f_{11}		k_{11}	$c_1(t+\Delta t)$
$t=0$	1455.4	0.000	1455.400	-335.364	0.250	1371.559	-316.045	0.250	1376.389	-317.157	0.300	1296.821	-298.823	1297.017455
$(t+\Delta t)=0.5$	1297.017455	0.5	1297.01745	-298.868	0.750	1147.583	-264.434	0.750	1230.909	-283.635	1.000	1155.200	-266.190	1158.584436
$(t+\Delta t)=1.0$	1158.584436	1.0	1158.58444	-266.969	1.250	1091.842	-251.590	1.250	1095.687	-252.476	1.500	1032.346	-237.881	1032.502568
$(t+\Delta t)=1.5$	1032.50257	1.5	1032.50257	-237.917	1.750	973.023	-224.211	1.750	976.450	-225.001	2.000	920.002	-211.994	920.1411404
$(t+\Delta t)=2.0$	920.14114	2	920.14114	-212.026	2.250	867.135	-199.811	2.250	870.189	-200.515	2.500	819.884	-188.924	820.0079079
$(t+\Delta t)=2.5$	820.0079079	2.5	820.007908	-188.952	2.500	772.770	-178.067	2.500	775.491	-178.694	3.000	620.008	-188.952	729.0556463
$(t+\Delta t)=3.0$	729.0556463	3.0	729.055646	-167.994	3.000	729.056	-167.994	3.000	687.057	-158.317	3.500	729.058	-167.994	646.6714559
$(t+\Delta t)=3.5$	646.6714559	3.5	646.671456	-149.011	3.500	648.971	-149.011	3.500	609.419	-140.427	4.000	648.671	-149.011	573.596781
$(t+\Delta t)=4.0$	573.596781	4.0	573.596781	-132.172	4.000	573.597	-132.172	4.000	540.554	-124.558	4.500	573.597	-132.172	508.7796348
$(t+\Delta t)=4.5$	508.7796348	4.5	508.779635	-117.237	4.500	508.780	-117.237	4.500	479.470	-110.483	5.000	508.780	-117.237	451.28e9063
$(t+\Delta t)=5.0$	451.28e9063	5.0	451.28e906	-103.989	5.000	451.297	-103.989	5.000	425.290	-97.998	6.000	451.287	-103.989	400.2909273



Danau	C(t) g/m³	W _t g/hari	Q _t m³/hari	V m³	H m	A m²	x m/hari	k hari⁻¹	λ _t hari⁻¹
S.Batu 1	1677	0	12092.2899	10000	2	5000	0.01	0	0.214
S.Batu2	1455.4	0	3381.408	15000	2	7500	0.01	0	0.230
S.Batu3	1248	0	15473.6979	18750	2.5	7500	0.01	0	0.029

$$\frac{dc}{dt} = \frac{W_t}{V} + Q_{in}/V - Q_{out}/V - k c$$

Initial condition

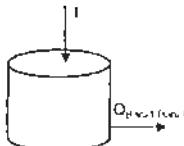
$$c(0) = 0$$

$$c_a(t) = c(0) + \int_0^t c(t) dt$$

$$\begin{aligned}
 & c_a(t + \Delta t) = c_a(t) + \frac{W_t}{V} (k_1 + k_2 + k_3 + k_4) \Delta t \\
 & k_1 = h_1 \cdot \ln(V_{1,a}) \\
 & k_2 = h_1 \cdot \ln(V_{2,a}) \\
 & k_3 = h_1 \cdot \ln(V_{3,a}) \\
 & k_4 = h_1 \cdot \ln(V_{4,a}) \\
 & V_{1,a} = V(1 + 1/2 \Delta t) c(t) + 1/2 \Delta t k_1 \\
 & V_{2,a} = V(1 + 1/2 \Delta t) c(t) + 1/2 \Delta t k_2 \\
 & V_{3,a} = V(1 + 1/2 \Delta t) c(t) + 1/2 \Delta t k_3 \\
 & V_{4,a} = V(1 + 1/2 \Delta t) c(t) + 1/2 \Delta t k_4
 \end{aligned}$$

Δt	$c_a(t)$	f	k_{1a}	f	k_{2a}	f	k_{3a}	f	k_{4a}	$c_a(t + \Delta t)$
0.5	1248.000	0.000	1248.000	1321.042	0.250	1578.261	412.602	0.250	1351.173	788.959
(t + Δt)=0.5	1557.30315	0.5	1557.303	107.265	0.750	1584.119	-620.308	0.750	1402.226	89.021
1.0	1431.5972	1.0	1431.597	-268.868	1.250	1384.380	-477.649	1.250	1324.605	-333.312
(t + Δt)=1.0	1431.5972	1.0	1431.597	-268.868	1.250	1384.380	-477.649	1.250	1324.605	-333.312
1.5	1242.88708	1.5	1242.887	-439.435	1.750	1133.028	-470.564	1.750	1125.248	-430.304
(t + Δt)=1.5	1242.88708	1.5	1242.887	-439.435	1.750	1133.028	-470.564	1.750	1125.248	-430.304
2.0	1017.95510	2.0	1017.955	-441.155	2.250	907.866	-421.013	2.250	912.702	-408.479
(t + Δt)=2.0	1017.95510	2.0	1017.955	-441.155	2.250	907.866	-421.013	2.250	912.702	-408.479
2.5	810.872627	2.5	810.873	-380.881	2.750	715.652	-344.955	2.750	724.834	-341.958
(t + Δt)=2.5	810.872627	2.5	810.873	-380.881	2.750	715.652	-344.955	2.750	724.834	-341.958
3.0	644.72245	3	644.722	-317.258	3.250	565.408	-251.496	3.250	581.851	-250.689
(t + Δt)=3.5	511.577602	3.5	511.528	-254.318	3.750	447.048	-201.504	3.750	451.129	-229.237
4.0	405.380022	3.5	511.528	-254.318	3.750	447.048	-201.504	3.750	451.129	-229.237
(t + Δt)=4.0	405.380022	4	405.389	-195.923	4.250	358.408	-155.305	4.250	368.563	-174.498
4.5	323.78743	4	405.389	-195.923	4.250	358.408	-155.305	4.250	368.563	-174.498
(t + Δt)=4.5	323.78743	4.5	323.797	-148.847	4.750	296.588	-117.989	4.750	294.300	-132.503
5.0	261.010227	4.5	323.797	-148.847	4.750	296.588	-117.989	4.750	294.300	-132.503
(t + Δt)=5.0	261.010227	5	261.019	-113.125	5.250	233.538	-89.673	5.250	239.401	-105.081
5.5	214.685323	5	261.019	-113.125	5.250	233.538	-89.673	5.250	239.401	-105.081
(t + Δt)=5.5	214.685323	5.5	214.665	-178.014	5.750	170.162	-141.109	5.750	179.389	-148.760
6.0	141.624835	5.5	214.665	-178.014	5.750	170.162	-141.109	5.750	179.389	-148.760
(t + Δt)=6.0	141.624835	6	141.625	-117.610	6.250	112.422	-93.228	6.250	118.518	-98.263
6.5	93.700667	6	141.625	-117.610	6.250	112.422	-93.228	6.250	118.518	-98.263
(t + Δt)=6.5	93.700667	6.5	93.701	-77.703	6.750	74.275	-61.594	6.750	78.302	-64.903
7.0	61.9060472	6.5	93.701	-77.703	6.750	74.275	-61.594	6.750	78.302	-64.903
(t + Δt)=7.0	61.9060472	7	61.906	-51.338	7.250	40.072	-40.694	7.250	51.733	-42.900
7.5	40.800015	7	61.906	-51.338	7.250	40.072	-40.694	7.250	51.733	-42.900
(t + Δt)=7.5	40.800015	7.5	40.900	-33.917	7.750	32.421	-26.885	7.750	34.179	-28.343
8.0	27.0217742	7.5	40.900	-33.917	7.750	32.421	-26.885	7.750	34.179	-28.343
(t + Δt)=8.0	27.0217742	8	27.022	-22.408	8.250	21.420	-17.763	8.250	22.581	-18.726
8.5	17.0527142	8	27.022	-22.408	8.250	21.420	-17.763	8.250	22.581	-18.726
(t + Δt)=8.5	17.0527142	8.5	17.053	-11.736	8.750	11.420	-11.420	8.750	17.655	-14.644

C1 9.23
C2 12.32
0.031666667



Bahan	C (t) g/m ³	W _t m ³ /barl	Q _t m ³ /barl	V m ³	H m	A m ²	v _t m/barl	k barl ⁻¹	k _t barl ⁻¹
S. Banul	9.21	0	12692.2899	16000	2	5000	0.01	0	121422899

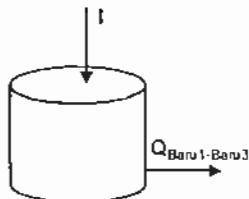
Initial condition:

$$t = 0 \\ c(t) = c_{\text{initial}} \quad \mu\text{m}^{-3} \\ c_i(t) = 9.23 \quad \mu\text{m}^{-3} \\ c_i(t + \Delta t) = c_i(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{array}{llllll} \text{Steady} & & k_{11} = f(t, c(t)) & & -\lambda_1 c_i(t) & \\ \frac{dc_i}{dt} & f(t, c_i(t)) & -\lambda_1 c_i & k_{21} = f(t + 1/2 \Delta t, c(t) + 1/2 \Delta t k_{11}) & -\lambda_1 c_i & (t + 1/2 \Delta t) k_{11} \\ dt & 0.5 \text{ s} & k_{31} = f(t + 1/2 \Delta t, c(t) + 1/2 \Delta t k_{21}) & -\lambda_1 c_i & -\lambda_1 c_i & (t + 1/2 \Delta t) k_{21} \\ t & 0 & k_{41} = f(t + \Delta t, c(t) + \Delta t k_{11}) & -\lambda_1 c_i & -\lambda_1 c_i & (t + \Delta t) k_{11} \end{array}$$

Δt 0.5	$c_i(t)$	f_{11}		k_{11}	f_{21}		k_{21}	f_{31}		k_{31}	f_{41}		k_{41}	$c_i(t + \Delta t)$
1 → 0	9.23	0.000	9.230	-11.207	0.250	6.428	-7.805	0.250	7.279	-8.838	0.500	4.811	-5.842	5.035
0.5	5.04	0.000	9.230	-11.207	0.250	6.428	-7.805	0.250	7.279	-8.838	0.500	4.811	-5.842	5.035
(t + Δt)	5.04	0.5	5.035	-6.114	0.750	1.978	-2.402	0.750	4.435	-5.383	1.000	2.343	-2.845	2.991
1.000	3.19	0.5	5.035	-6.114	0.750	1.978	-2.402	0.750	4.435	-5.383	1.000	2.343	-2.845	2.991
(t + Δt)	3.19	1.000	3.191	-3.875	1.250	2.222	-2.698	1.250	2.516	-3.055	1.500	1.663	-2.070	1.741
1.500	1.74	1.000	3.191	-3.875	1.250	2.222	-2.698	1.250	2.516	-3.055	1.500	1.663	-2.070	1.741
(t + Δt)	1.74	2.000	1.741	-2.114	1.750	1.212	-1.472	1.750	1.373	-1.667	2.000	0.902	-1.102	0.950
2.000	0.95	2.000	1.741	-2.114	1.750	1.212	-1.472	1.750	1.373	-1.667	2.000	0.902	-1.102	0.950
(t + Δt)	0.95	2.000	0.950	-1.153	2.250	0.661	-0.803	2.250	0.749	-0.909	2.500	0.495	-0.601	0.518
2.500	0.52	2.000	0.950	-1.153	2.250	0.661	-0.803	2.250	0.749	-0.909	2.500	0.495	-0.601	0.518
(t + Δt)	0.52	2.500	0.518	-0.629	2.500	0.361	-0.438	2.500	0.409	-0.496	3.000	0.518	-0.629	0.258
3.000	0.26	2.500	0.518	-0.629	2.500	0.361	-0.438	2.500	0.409	-0.496	3.000	0.518	-0.629	0.258
(t + Δt)	0.26	3.000	0.258	-0.313	3.000	0.258	-0.313	3.000	0.179	-0.218	3.500	0.258	-0.313	0.117
3.500	0.12	3.000	0.258	-0.313	3.000	0.258	-0.313	3.000	0.179	-0.218	3.500	0.258	-0.313	0.117
(t + Δt)	0.12	3.500	0.117	-0.142	3.500	0.117	-0.142	3.500	0.081	-0.099	4.000	0.117	-0.142	0.053
4.000	0.05	3.500	0.117	-0.142	3.500	0.117	-0.142	3.500	0.081	-0.099	4.000	0.117	-0.142	0.053
(t + Δt)	0.05	4.000	0.053	-0.065	4.000	0.053	-0.065	4.000	0.037	-0.045	4.500	0.053	-0.065	0.024
4.500	0.02	4.000	0.053	-0.065	4.000	0.053	-0.065	4.000	0.037	-0.045	4.500	0.053	-0.065	0.024
(t + Δt)	0.02	4.500	0.024	-0.029	4.500	0.024	-0.029	4.500	0.017	-0.020	5.000	0.024	-0.029	0.011
5.000	0.01	4.500	0.024	-0.029	4.500	0.024	-0.029	4.500	0.017	-0.020	5.000	0.024	-0.029	0.011
(t + Δt)	0.01	5.000	0.011	-0.013	5.000	0.011	-0.013	5.000	0.008	-0.009	5.500	0.011	-0.013	0.005

Ammonium



C1 1.46
C2 0.8

Danau	C (t) g/m ³	W _i g/hari	Q _i m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	λ ₄ hari ⁻¹
S. Baru1	2.72	0	12092	10000	2	5000	0	0	1.2092

initial condition

$$t = 0$$

$$c_i(t) = c_{\text{dew}} \text{ g/m}^3$$

$$c_i(t) = 2.72 \text{ g/m}^3$$

$$c_i(t + \Delta t) = c_i(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady

$$\frac{dc_i}{dt} = f(t, c_i(t))$$

$$c_i(t) = -\lambda_1 c_1$$

$$dt = 0.5 \text{ hr}$$

$$t = 0$$

$$c_i(t) = 2.72$$

$$k_{1i} = f(t, c_i(t)) = -\lambda_1 c_i(t)$$

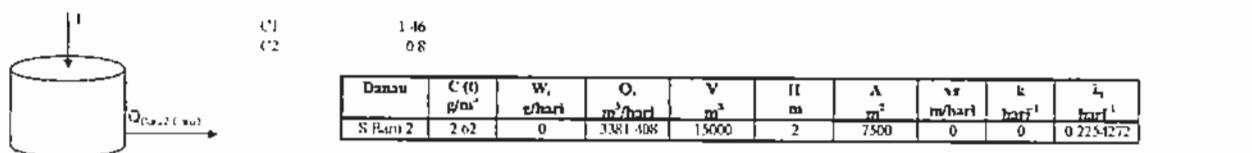
$$k_{2i} = f(t + 1/2\Delta t, c_i(t) + 1/2\Delta t) = -\lambda_1 c_i(t + 1/2 \Delta t k_{1i})$$

$$k_{3i} = f(t + 1/2\Delta t, c_i(t) + 1/2\Delta t) = -\lambda_1 c_i(t + 1/2 \Delta t k_{2i})$$

$$k_{4i} = f(t + \Delta t, c_i(t) + \Delta t k_{3i}) = -\lambda_1 c_i(t + \Delta t k_{3i})$$

Δt 0.5	$c_i(t)$	f_{1i}		k_{1i}	f_{2i}		k_{2i}	f_{3i}		k_{3i}	f_{4i}		k_{4i}	$c_i(t + \Delta t)$
$t = 0$	2.720													
0.5	0.000	2.720	-3.289	0.250	1.698	-2.295	0.250	2.146	-2.595	0.500	1.422	-1.720	1.488	
$(t + \Delta t) = 0.5$	1.488													
1.0	0.500	1.488	-1.799	0.750	0.588	-0.711	0.750	1.310	-1.584	1.000	0.696	-0.841	0.885	
$(t + \Delta t) = 1.0$	0.885													
1.5	1.000	0.885	-1.070	1.250	0.617	-0.747	1.250	0.698	-0.845	1.500	0.463	-0.560	0.484	
$(t + \Delta t) = 1.5$	0.484													
2.0	1.500	0.484	-0.585	1.750	0.338	-0.408	1.750	0.382	-0.462	2.000	0.253	-0.306	0.265	
$(t + \Delta t) = 2.0$	0.265													
2.5	2.000	0.265	-0.320	2.250	0.185	-0.223	2.250	0.209	-0.253	2.500	0.138	-0.167	0.145	
$(t + \Delta t) = 2.5$	0.145													
3.0	2.500	0.145	-0.175	2.500	0.101	-0.122	2.500	0.114	-0.138	3.000	0.145	-0.175	0.072	
$(t + \Delta t) = 3.0$	0.072													
3.5	3.000	0.072	-0.087	3.000	0.072	-0.087	3.000	0.050	-0.061	3.500	0.072	-0.087	0.033	
$(t + \Delta t) = 3.5$	0.033													
4.0	3.500	0.033	-0.040	3.500	0.033	-0.040	3.500	0.023	-0.028	4.000	0.033	-0.040	0.015	
$(t + \Delta t) = 4.0$	0.015													
4.5	4.000	0.015	-0.018	4.000	0.015	-0.018	4.000	0.010	-0.013	4.500	0.015	-0.018	0.007	
$(t + \Delta t) = 4.5$	0.007													
5.0	4.500	0.007	-0.008	4.500	0.007	-0.008	4.500	0.005	-0.006	5.000	0.007	-0.008	0.003	
$(t + \Delta t) = 5.0$	0.003													
	5.000	0.003	-0.004	5.000	0.003	-0.004	5.000	0.002	-0.003	0.000	0.003	-0.004	0.001	

Annular



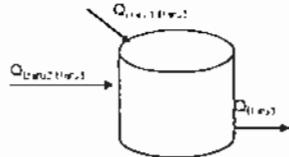
initial condition

$$\begin{aligned} t &= 0 \\ c_1(t) &= c_{1,\text{ini}} \quad \text{g/m}^3 \\ c_1(t) &= 2.62 \quad \text{g/m}^3 \end{aligned}$$

$$c_1(t + \Delta t) = c_1(t) - \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= f(t, c_1(t)) \quad \text{= } -\lambda_1 c_1 \\ dt &= 0.5 \text{ hr} \quad \text{= } -\lambda_1 c_1 - (t + 1/2 \Delta t) k_{11} \\ c_1(t) &= 2.62 \quad \text{= } -\lambda_1 c_1 - (t + 1/2 \Delta t) k_{11} \end{aligned}$$

Δt 0.5	$c_1(t)$	f_{11}	k_{11}	f_{12}	k_{21}	f_{23}	k_{31}	f_{41}	k_{41}	$c_1(t + \Delta t)$
t = 0	2.62	0.000	2.620	-0.591	0.250	2.472	-0.557	0.250	2.481	-0.559
(t + Δt) = 0.5	2.34072541			-0.528	0.750	2.077	-0.468	0.750	2.224	-0.501
1.0	2.09591229			-0.472	1.250	1.978	-0.446	1.250	1.984	-0.447
(t + Δt) = 1.5	1.87250196			-0.422	1.750	1.767	-0.398	1.750	1.773	-0.400
(t + Δt) = 2.0	1.6729057			-0.377	2.250	1.579	-0.356	2.250	1.584	-0.357
(t + Δt) = 2.5	1.494585083			-0.337	2.500	1.410	-0.318	2.500	1.415	-0.319
(t + Δt) = 3.0	1.332275898			-0.300	3.000	1.332	-0.300	3.000	1.257	-0.300
(t + Δt) = 3.5	1.184931237			-0.267	3.500	1.185	-0.267	3.500	1.118	-0.252
(t + Δt) = 4.0	1.053882336			-0.238	4.000	1.054	-0.238	4.000	0.991	-0.224
(t + Δt) = 4.5	0.937326947			-0.211	4.500	0.937	-0.211	4.500	0.885	-0.199
(t + Δt) = 5.0	0.833662141			-0.188	5.000	0.834	-0.188	5.000	0.787	-0.177



Danau	C(t) g/m³	W _t t/m³	Q _t m³/t/m³	V m³	H m	A m²	r m/t/m³	k t/m³	λ _t t/m³
S Baru 1	2.72	0	12092.2899	10000	2	5000	0	0	1.209
S Baru 2	2.62	0	1361.408	15000	2	7500	0	0	0.725
S Baru 3	5.98	0	15473.6979	18750	2.5	7500	0	0	0.875

$$\frac{dV}{dt} = \frac{W_t}{V} + Q_{inlet} - Q_{outlet} - k_1 C_t$$

$$dt = 0.5$$

Initial condition:

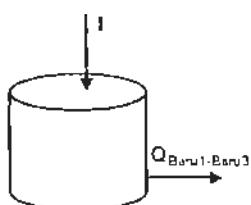
$$C(0) = 0$$

$$C_{inlet} = 5.98 \text{ g/m}^3$$

$$\begin{aligned}
 & C_t(t + \Delta t) = C_t(t) + \frac{W_t}{V} \Delta t + Q_{inlet} \Delta t - k_1 C_t(t) \\
 & k_{11} = k_1, \quad C_{inlet} \\
 & k_{12} = k_1 + 1/2\Delta t, \quad C(t) \\
 & k_{13} = k_1 + 1/2\Delta t, \quad C(t + \Delta t) \\
 & k_{14} = k_1 + 1/2\Delta t, \quad C(t + 1/2\Delta t) \\
 & k_{15} = k_1 + 1/2\Delta t, \quad C(t + \Delta t) \\
 & k_{16} = k_1 + 1/2\Delta t, \quad C(t + 3/2\Delta t) \\
 & k_{17} = k_1 + 1/2\Delta t, \quad C(t + 2\Delta t) \\
 & k_{18} = k_1 + 1/2\Delta t, \quad C(t + 5/2\Delta t) \\
 & k_{19} = k_1 + 1/2\Delta t, \quad C(t + 3\Delta t) \\
 & k_{20} = k_1 + 1/2\Delta t, \quad C(t + 7/2\Delta t) \\
 & k_{21} = k_1 + 1/2\Delta t, \quad C(t + 4\Delta t) \\
 & k_{22} = k_1 + 1/2\Delta t, \quad C(t + 9/2\Delta t) \\
 & k_{23} = k_1 + 1/2\Delta t, \quad C(t + 5\Delta t) \\
 & k_{24} = k_1 + 1/2\Delta t, \quad C(t + 11/2\Delta t) \\
 & k_{25} = k_1 + 1/2\Delta t, \quad C(t + 6\Delta t) \\
 & k_{26} = k_1 + 1/2\Delta t, \quad C(t + 13/2\Delta t) \\
 & k_{27} = k_1 + 1/2\Delta t, \quad C(t + 7\Delta t) \\
 & k_{28} = k_1 + 1/2\Delta t, \quad C(t + 15/2\Delta t) \\
 & k_{29} = k_1 + 1/2\Delta t, \quad C(t + 8\Delta t) \\
 & k_{30} = k_1 + 1/2\Delta t, \quad C(t + 17/2\Delta t) \\
 & k_{31} = k_1 + 1/2\Delta t, \quad C(t + 9\Delta t) \\
 & k_{32} = k_1 + 1/2\Delta t, \quad C(t + 19/2\Delta t) \\
 & k_{33} = k_1 + 1/2\Delta t, \quad C(t + 10\Delta t) \\
 & k_{34} = k_1 + 1/2\Delta t, \quad C(t + 21/2\Delta t) \\
 & k_{35} = k_1 + 1/2\Delta t, \quad C(t + 11\Delta t) \\
 & k_{36} = k_1 + 1/2\Delta t, \quad C(t + 23/2\Delta t) \\
 & k_{37} = k_1 + 1/2\Delta t, \quad C(t + 12\Delta t) \\
 & k_{38} = k_1 + 1/2\Delta t, \quad C(t + 25/2\Delta t) \\
 & k_{39} = k_1 + 1/2\Delta t, \quad C(t + 13\Delta t) \\
 & k_{40} = k_1 + 1/2\Delta t, \quad C(t + 27/2\Delta t) \\
 & k_{41} = k_1 + 1/2\Delta t, \quad C(t + 14\Delta t) \\
 & k_{42} = k_1 + 1/2\Delta t, \quad C(t + 29/2\Delta t) \\
 & k_{43} = k_1 + 1/2\Delta t, \quad C(t + 15\Delta t) \\
 & k_{44} = k_1 + 1/2\Delta t, \quad C(t + 31/2\Delta t) \\
 & C_{inlet} = 5.98 \text{ g/m}^3
 \end{aligned}$$

Δt 0.5	$C_t(t)$	f	k_{14}	f	k_{24}	f	k_{34}	f	k_{44}	$C_t(t + \Delta t)$				
t = 0	5.960	0.000	5.960	-1.039	0.250	5.700	-1.852	0.250	5.497	-1.282	0.500	5.269	-2.101	5.159357328
(t + Δt)=0.5	5.15935733	0.5	5.159	-3.134	0.750	4.378	-2.432	0.750	4.551	-1.671	1.000	4.324	-2.258	4.026388623
1.0	4.02638862	0.5	5.159	-3.134	0.750	4.378	-1.592	1.250	3.629	-1.702	1.500	3.175	-1.639	3.123428527
1.5	3.12342853	1.0	4.028	-2.607	1.250	3.378	-1.330	1.750	2.791	-1.442	2.000	2.403	-1.300	2.375045339
(t + Δt)= 1.5	2.37504534	1.5	3.123	-2.138	1.750	2.588	-1.035	2.250	2.115	-1.137	2.500	1.807	-0.987	1.791185411
2.0	1.79118541	2	2.375	-1.678	2.250	1.958	-0.773	2.750	1.598	-0.662	3.000	1.380	-0.811	1.360849525
(t + Δt)= 2.5	1.36084952	2.5	1.791	-1.284	2.750	1.470	-0.773	2.750	1.598	-0.662	3.000	1.380	-0.811	1.360849525
3.0	1.04021431	3	1.361	-0.987	3.250	1.114	-0.532	3.250	1.228	-0.668	3.500	1.076	-0.459	1.040214313
(t + Δt)= 3.5	0.94147138	3.5	1.040	-0.757	3.750	0.851	-0.365	3.750	0.941	-0.497	4.000	0.782	-0.348	0.709572905
4.0	0.7995229	4.0	0.940	-0.579	4.250	0.655	-0.285	4.250	0.728	-0.364	4.500	0.617	-0.284	0.621075303
(t + Δt)= 4.5	0.6210753	4.5	0.800	-0.418	4.750	0.510	-0.202	4.750	0.572	-0.267	5.000	0.489	-0.164	0.491471377
5.0	0.49147138	5.0	0.622	-0.448	4.750	0.510	-0.202	4.750	0.572	-0.267	5.000	0.489	-0.164	0.491471377
(t + Δt)= 5.0	0.49147138	5	0.491	-0.348	5.250	0.405	-0.142	5.250	0.458	-0.198	5.500	0.393	-0.133	0.395017689
5.5	0.39501769	5.5	0.395	-0.326	5.750	0.314	-0.258	5.750	0.330	-0.273	6.000	0.298	-0.214	0.261501343
(t + Δt)= 5.2	0.26150134	6	0.262	-0.218	6.250	0.208	-0.171	6.250	0.219	-0.180	6.500	0.171	-0.141	0.173113546
6.0	0.17311355	6.5	0.173	-0.143	6.750	0.137	-0.113	6.750	0.145	-0.119	7.000	0.113	-0.094	0.114601073
(t + Δt)= 6.3	0.11460107	7	0.115	-0.085	7.250	0.081	-0.075	7.250	0.098	-0.079	7.500	0.075	-0.062	0.073885804
7.0	0.0758858	7.5	0.076	-0.063	7.750	0.060	-0.050	7.750	0.063	-0.052	8.000	0.050	-0.041	0.050223092
(t + Δt)= 7.6	0.05022309	8	0.050	-0.041	8.250	0.040	-0.033	8.250	0.042	-0.035	8.500	0.033	-0.027	0.03324784
(t + Δt)= 7.7	0.03324784													

Ammonium



C1 1.46
C2 0.8

Danau	C (0) g/m ³	W _t g/hari	Q _t m ³ /hari	V m ³	H m	A m ²	vs m/hari	k hari ⁻¹	k _d hari ⁻¹
S. Baru1	2.62	0	12092	10000	2	5000	0.01	0	1.2142

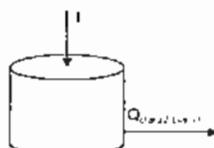
initial condition

$$t = 0 \\ c(t) = c_{\text{deau}} \text{ g/m}^3 \\ c_1(t) = 2.62 \text{ g/m}^3 \\ c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$\begin{aligned} \text{Steady} \\ \frac{dc_1}{dt} &= -f(L) = -\lambda_1 c_1 & k_{11} = f(t, c(t)) &= -\lambda_1 c_1(t) \\ c_1(t) &= & k_{21} = f(t + 1/2\Delta t, c(t) + 1/2\Delta t) &= -\lambda_1 c_1(t + 1/2\Delta t k_{11}) \\ && k_{31} = f(t + 1/2\Delta t, c(t) + 1/2\Delta t) &= -\lambda_1 c_1(t + 1/2\Delta t k_{21}) \\ dt &= 0.5 \text{ hr} & k_{41} = f(t + \Delta t, c(t) + \Delta t k_{31}) &= -\lambda_1 c_1(t + \Delta t k_{31}) \\ t &= 0 \\ c_1(t) &= 2.62 \end{aligned}$$

Δt 0.5	$c_1(t)$	f_{11}		k_{11}	f_{21}		k_{21}	f_{31}		k_{31}	f_{41}		k_{41}	$c_1(t + \Delta t)$
t = 0	2.620													
0.5	1.429	0.000	2.620	-3.181	0.250	1.825	-2.216	0.250	2.066	-2.509	0.500	1.366	-1.658	1.429
(t + Δt)= 0,5	1.429													
1.0	0.849	0.500	1.429	-1.736	0.750	0.562	-0.682	0.750	1.259	-1.529	1.000	0.665	-0.808	0.849
(t + Δt)= 1,0	0.849													
1.5	0.463	1.000	0.849	-1.031	1.250	0.591	-0.718	1.250	0.670	-0.813	1.500	0.443	-0.537	0.463
(t + Δt)= 1,5	0.463													
2.0	0.253	1.500	0.463	-0.562	1.750	0.323	-0.392	1.750	0.365	-0.443	2.000	0.241	-0.293	0.253
(t + Δt)= 2,0	0.253													
2.5	0.138	2.000	0.253	-0.307	2.250	0.176	-0.214	2.250	0.199	-0.242	2.500	0.132	-0.160	0.138
(t + Δt)= 2,5	0.138													
3.0	0.069	2.500	0.138	-0.167	2.500	0.096	-0.117	2.500	0.109	-0.132	3.000	0.138	-0.167	0.069
(t + Δt)= 3,0	0.069													
3.5	0.031	3.000	0.069	-0.083	3.000	0.069	-0.083	3.000	0.048	-0.058	3.500	0.069	-0.083	0.031
(t + Δt)= 3,5	0.031													
4.0	0.014	3.500	0.031	-0.038	3.500	0.031	-0.038	3.500	0.022	-0.026	4.000	0.031	-0.038	0.014
(t + Δt)= 4,0	0.014													
4.5	0.006	4.000	0.014	-0.017	4.000	0.014	-0.017	4.000	0.010	-0.012	4.500	0.014	-0.017	0.006
(t + Δt)= 4,5	0.006													
5.0	0.003	4.500	0.006	-0.008	4.500	0.006	-0.008	4.500	0.004	-0.005	5.000	0.006	-0.008	0.003
(t + Δt)= 5,0	0.003													
5.5	0.001	5.000	0.003	-0.004	5.000	0.003	-0.004	5.000	0.002	-0.002	0.000	0.003	-0.004	0.001

Ammonium

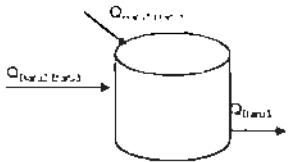


Danau	C (0) g/m³	W _i g/hari	Q _i m³/hari	V m³	H m	A m²	γ _g m³/hari	k hari⁻¹	λ _i hari⁻¹
S Baru 2	2.48	0	3381.408	15000	2	7500	0	0	0.2253272

initial condition

$$\begin{aligned}
 t &= 0 \\
 c_i(t) &= 0 \\
 c_{i,0} &= 2.48 \text{ g/m}^3 \\
 c_i(t) &= c_{i,0} + k_{11}c_1(t) + k_{21}c_2(t) + k_{31}c_3(t) + k_{41}c_4(t) \\
 \dot{c}_i(t) &= -k_{11}c_1(t) - k_{21}c_2(t) - k_{31}c_3(t) - k_{41}c_4(t) \\
 \text{Steady state} & \quad c_i(t) = 0 \\
 \dot{c}_i(t) &= 0 \\
 \Delta t &= 0.5 \text{ hr} \\
 t &= 0 \\
 c_i(t) &= 2.48
 \end{aligned}$$

Δt 0.5	$c_1(0)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_1(t+\Delta t)$
1.0	2.48	0.000	2.480	-0.559	0.250	2.340	-0.528	0.250	2.348	-0.529
0.5	2.21564848	0.5	2.21564848	-0.499	0.750	1.966	-0.443	0.750	2.105	-0.474
(1 + Δt) = 1.0	1.98391698			-0.447	1.250	1.872	-0.422	1.250	1.878	-0.423
1.5	1.77244461	1.0	1.98391698	-0.400	1.750	1.673	-0.377	1.750	1.678	-0.378
(1 + Δt) = 1.5	1.77244461	1.5	1.77244461	-0.357	2.250	1.494	-0.337	2.250	1.499	-0.338
2.0	1.58351379	2	1.58351379	-0.337	2.250	1.494	-0.337	2.250	1.499	-0.338
(1 + Δt) = 2.0	1.58351379	2.5	1.58351379	-0.319	2.500	1.335	-0.301	2.500	1.339	-0.302
3.0	1.414721739	3	1.414721739	-0.284	3.000	1.261	-0.284	3.000	1.190	-0.268
(1 + Δt) = 3.0	1.414721739	3.5	1.414721739	-0.253	3.500	1.122	-0.253	3.500	1.058	-0.239
4.0	1.121614301	4	1.121614301	-0.225	4.000	0.998	-0.225	4.000	0.941	-0.212
(1 + Δt) = 4.0	1.121614301	4.5	1.121614301	-0.200	4.500	0.887	-0.200	4.500	0.837	-0.189
5.0	0.887240774	5	0.887240774	-0.178	5.000	0.789	-0.178	5.000	0.745	-0.168
(1 + Δt) = 5.0	0.887240774	5.5	0.887240774	-0.158	5.500	0.700	-0.158	5.500	0.662	-0.150
6.0	0.789115309	6	0.789115309	-0.140	6.000	0.625	-0.140	6.000	0.593	-0.140
(1 + Δt) = 6.0	0.789115309	6.5	0.789115309	-0.125	6.500	0.556	-0.125	6.500	0.527	-0.135
7.0	0.701812149	7	0.701812149	-0.112	7.000	0.500	-0.112	7.000	0.480	-0.125
(1 + Δt) = 7.0	0.701812149	7.5	0.701812149	-0.100	7.500	0.455	-0.100	7.500	0.425	-0.115
8.0	0.636526352	8	0.636526352	-0.090	8.000	0.416	-0.090	8.000	0.390	-0.105
(1 + Δt) = 8.0	0.636526352	8.5	0.636526352	-0.080	8.500	0.382	-0.080	8.500	0.357	-0.095
9.0	0.58351379	9	0.58351379	-0.072	9.000	0.353	-0.072	9.000	0.330	-0.085
(1 + Δt) = 9.0	0.58351379	9.5	0.58351379	-0.065	9.500	0.328	-0.065	9.500	0.305	-0.075
10.0	0.542857143	10	0.542857143	-0.058	10.000	0.305	-0.058	10.000	0.280	-0.065
(1 + Δt) = 10.0	0.542857143	10.5	0.542857143	-0.052	10.500	0.285	-0.052	10.500	0.260	-0.055
11.0	0.513513513	11	0.513513513	-0.046	11.000	0.267	-0.046	11.000	0.240	-0.045
(1 + Δt) = 11.0	0.513513513	11.5	0.513513513	-0.040	11.500	0.251	-0.040	11.500	0.220	-0.040
12.0	0.490000000	12	0.490000000	-0.034	12.000	0.236	-0.034	12.000	0.200	-0.034
(1 + Δt) = 12.0	0.490000000	12.5	0.490000000	-0.029	12.500	0.223	-0.029	12.500	0.180	-0.029
13.0	0.470000000	13	0.470000000	-0.024	13.000	0.211	-0.024	13.000	0.160	-0.024
(1 + Δt) = 13.0	0.470000000	13.5	0.470000000	-0.020	13.500	0.200	-0.020	13.500	0.140	-0.020
14.0	0.453513513	14	0.453513513	-0.016	14.000	0.190	-0.016	14.000	0.120	-0.016
(1 + Δt) = 14.0	0.453513513	14.5	0.453513513	-0.012	14.500	0.181	-0.012	14.500	0.100	-0.012
15.0	0.440000000	15	0.440000000	-0.009	15.000	0.173	-0.009	15.000	0.080	-0.009
(1 + Δt) = 15.0	0.440000000	15.5	0.440000000	-0.006	15.500	0.165	-0.006	15.500	0.060	-0.006
16.0	0.430000000	16	0.430000000	-0.004	16.000	0.158	-0.004	16.000	0.040	-0.004
(1 + Δt) = 16.0	0.430000000	16.5	0.430000000	-0.002	16.500	0.152	-0.002	16.500	0.020	-0.002
17.0	0.422857143	17	0.422857143	-0.001	17.000	0.146	-0.001	17.000	0.010	-0.001
(1 + Δt) = 17.0	0.422857143	17.5	0.422857143	0.000	17.500	0.141	0.000	17.500	0.005	0.000
18.0	0.417500000	18	0.417500000	0.000	18.000	0.136	0.000	18.000	0.000	0.000
(1 + Δt) = 18.0	0.417500000	18.5	0.417500000	0.000	18.500	0.132	0.000	18.500	0.000	0.000
19.0	0.414000000	19	0.414000000	0.000	19.000	0.128	0.000	19.000	0.000	0.000
(1 + Δt) = 19.0	0.414000000	19.5	0.414000000	0.000	19.500	0.125	0.000	19.500	0.000	0.000
20.0	0.412000000	20	0.412000000	0.000	20.000	0.122	0.000	20.000	0.000	0.000
(1 + Δt) = 20.0	0.412000000	20.5	0.412000000	0.000	20.500	0.120	0.000	20.500	0.000	0.000
21.0	0.411000000	21	0.411000000	0.000	21.000	0.118	0.000	21.000	0.000	0.000
(1 + Δt) = 21.0	0.411000000	21.5	0.411000000	0.000	21.500	0.116	0.000	21.500	0.000	0.000
22.0	0.411000000	22	0.411000000	0.000	22.000	0.114	0.000	22.000	0.000	0.000
(1 + Δt) = 22.0	0.411000000	22.5	0.411000000	0.000	22.500	0.112	0.000	22.500	0.000	0.000
23.0	0.411000000	23	0.411000000	0.000	23.000	0.110	0.000	23.000	0.000	0.000
(1 + Δt) = 23.0	0.411000000	23.5	0.411000000	0.000	23.500	0.108	0.000	23.500	0.000	0.000
24.0	0.411000000	24	0.411000000	0.000	24.000	0.106	0.000	24.000	0.000	0.000
(1 + Δt) = 24.0	0.411000000	24.5	0.411000000	0.000	24.500	0.104	0.000	24.500	0.000	0.000
25.0	0.411000000	25	0.411000000	0.000	25.000	0.102	0.000	25.000	0.000	0.000
(1 + Δt) = 25.0	0.411000000	25.5	0.411000000	0.000	25.500	0.100	0.000	25.500	0.000	0.000
26.0	0.411000000	26	0.411000000	0.000	26.000	0.098	0.000	26.000	0.000	0.000
(1 + Δt) = 26.0	0.411000000	26.5	0.411000000	0.000	26.500	0.096	0.000	26.500	0.000	0.000
27.0	0.411000000	27	0.411000000	0.000	27.000	0.094	0.000	27.000	0.000	0.000
(1 + Δt) = 27.0	0.411000000	27.5	0.411000000	0.000	27.500	0.092	0.000	27.500	0.000	0.000
28.0	0.411000000	28	0.411000000	0.000	28.000	0.090	0.000	28.000	0.000	0.000
(1 + Δt) = 28.0	0.411000000	28.5	0.411000000	0.000	28.500	0.088	0.000	28.500	0.000	0.000
29.0	0.411000000	29	0.411000000	0.000	29.000	0.086	0.000	29.000	0.000	0.000
(1 + Δt) = 29.0	0.411000000	29.5	0.411000000	0.000	29.500	0.084	0.000	29.500	0.000	0.000
30.0	0.411000000	30	0.411000000	0.000	30.000	0.082	0.000	30.000	0.000	0.000
(1 + Δt) = 30.0	0.411000000	30.5	0.411000000	0.000	30.500	0.080	0.000	30.500	0.000	0.000
31.0	0.411000000	31	0.411000000	0.000	31.000	0.078	0.000	31.000	0.000	0.000
(1 + Δt) = 31.0	0.411000000	31.5	0.411000000	0.000	31.500	0.076	0.000	31.500	0.000	0.000
32.0	0.411000000	32	0.411000000	0.000	32.000	0.074	0.000	32.000	0.000	0.000
(1 + Δt) = 32.0	0.411000000	32.5	0.411000000	0.000	32.500	0.072	0.000	32.500	0.000	0.000
33.0	0.411000000	33	0.411000000	0.000	33.000	0.070	0.000	33.000	0.000	0.000
(1 + Δt) = 33.0	0.411000000	33.5	0.411000000	0.000	33.500	0.068	0.000	33.500	0.000	0.000
34.0	0.411000000	34	0.411000000	0.000	34.000	0.066	0.000	34.000	0.000	0.000
(1 + Δt) = 34.0	0.411000000	34.5	0.411000000	0.000	34.500	0.064	0.000	34.500	0.000	0.000
35.0	0.411000000	35	0.411000000	0.000	35.000	0.062	0.000	35.000	0.000	0.000
(1 + Δt) = 35.0	0.411000000	35.5	0.411000000	0.000	35.500	0.060	0.000	35.500	0.000	0.000
36.0	0.411000000	36	0.411000000	0.000	36.000	0.058	0.000	36.000	0.000	0.000
(1 + Δt) = 36.0	0.411000000	36.5	0.411000000	0.000	36.500	0.056	0.000	36.500	0.000	0.000
37.0	0.411000000	37	0.411000000	0.000	37.000	0.054	0.000	37.000	0.000	0.000
(1 + Δt) = 37.0	0.411000000	37.5	0.411000000	0.000	37.500					



Danau	C (t) g/m³	W _t g/hari	Q _t m³/hari	V m³	B m	A m²	v m/hari	k hari⁻¹	k _f hari⁻¹
S Baru 1	2.62	0	12092.2899	10000	2	5000	0	0	1.209
S Baru 2	2.48	0	3381.408	15000	2	7500	0	0	0.225
S Baru 3	2	0	15473.6979	19750	2.5	7500	0	0	0.825

$$\frac{dc_i}{dt} = \frac{W_t V}{dt} + Q_{in}V_{c_{in}} - Q_{out}V_{c_{out}} - k_i c_i$$

initial condition
 $c_i(0) = c_{i,0}$

$$c_i(t + \Delta t) = c_i(t) + \frac{W_t V}{dt} + Q_{in}V_{c_{in}} - Q_{out}V_{c_{out}} - k_i c_i$$

$$k_{in} = f(t, c_i(t))$$

$$k_{out} = f(t + 1/2\Delta t, c_i(t) + 1/2\Delta t k_i)$$

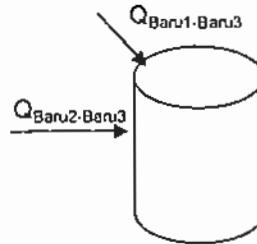
$$k_{in} = f(t + 1/2\Delta t, c_i(t) + 1/2\Delta t k_i)$$

$$k_{out} = f(t + 1/2\Delta t, c_i(t) + 1/2\Delta t k_i)$$

$$k_{in} = f(t + \Delta t, c_i(t) + \Delta t k_i)$$

$$k_{out} = f(t + \Delta t, c_i(t) + \Delta t k_i)$$

Δt 0.5	$c_i(t)$	f	k_{in}	f	k_{out}	f	k_{in}	f	k_{out}	$c_i(t + \Delta t)$
1 = 0	2.000	0.000	2.000	2.077	0.250	2.519	0.655	0.250	2.164	1.242
(t + Δt)= 0.5	2.48821570	0.5	2.488	-0.930	0.750	2.256	-0.739	0.750	2.303	0.098
1.0	2.23325784	0.5	2.488	-0.930	0.750	2.256	-0.739	0.750	2.303	1.000
(t + Δt)= 1.0	1.91893298	1.0	2.233	-1.127	1.250	1.951	-0.473	1.250	2.115	-0.512
1.5	1.56248155	1.5	1.917	-1.142	1.750	1.631	-0.579	1.750	1.772	-0.642
(t + Δt)= 1.5	1.24291018	2	1.562	-1.005	2.250	1.311	-0.533	2.250	1.429	-0.601
2.0	0.98934313	2.5	1.243	-0.831	2.750	1.035	-0.437	2.750	1.134	-0.502
(t + Δt)= 2.0	0.78729052	3	0.989	-0.680	3.250	0.819	-0.309	3.250	0.912	-0.477
2.5	0.62642087	3.5	0.787	-0.549	3.750	0.650	-0.245	3.750	0.726	-0.334
(t + Δt)= 2.5	0.50262683	4	0.626	-0.430	4.250	0.517	-0.165	4.250	0.580	-0.255
3.0	0.40807188	4.5	0.503	-0.347	4.750	0.416	-0.135	4.750	0.469	-0.193
(t + Δt)= 3.0	0.33843481	5	0.406	-0.279	5.250	0.339	-0.098	5.250	0.384	-0.148
3.5	0.2227194	5.5	0.336	-0.278	5.750	0.267	-0.020	5.750	0.281	-0.132
(t + Δt)= 3.5	0.14744003	6	0.223	-0.184	6.250	0.177	-0.148	6.250	0.186	-0.154
4.0	0.09780517	6.5	0.147	-0.127	6.750	0.117	-0.097	6.750	0.123	-0.102
(t + Δt)= 4.0	0.06481453	7	0.098	-0.081	7.250	0.077	-0.064	7.250	0.082	-0.087
4.5	0.04277476	7.5	0.065	-0.053	7.750	0.051	-0.042	7.750	0.054	-0.045
(t + Δt)= 4.5	0.02801685	8	0.043	-0.035	8.250	0.034	-0.028	8.250	0.036	-0.030
5.0										0.028
(t + Δt)= 5.0										0.023
5.5										0.023
(t + Δt)= 5.5										0.023
6.0										0.023
(t + Δt)= 6.0										0.023
6.5										0.023
(t + Δt)= 6.5										0.023
7.0										0.023
(t + Δt)= 7.0										0.023
7.5										0.023
(t + Δt)= 7.5										0.023
8.0										0.023
(t + Δt)= 8.0										0.023
8.5										0.023
(t + Δt)= 8.5										0.023
9.0										0.023
(t + Δt)= 9.0										0.023
9.5										0.023
(t + Δt)= 9.5										0.023
10.0										0.023
(t + Δt)= 10.0										0.023



Danau	$C(t)$ g/m^3	W_1	Q_1 m^3/hari	V m^3	H m	A m^2	v m/hari	k hari^{-1}	λ_4 hari^{-1}
S. Baru 1	2.72	0	12092.29	10000	2	5000	0.01	0.197	1.406
S. Baru 2	2.62	0	3381.41	20000	2	10000	0.01	0.197	0.366
S. Baru 3	5.96	0	15473.70	12500	2.5	5000	0.01	0.197	1.435

$$\frac{dc_4}{dt} = W_4/V + Q_{14}/V_1 c_{14} + Q_{34}/V_3 c_{34} - \lambda_4 c_4$$

$$\Delta t = 0.5$$

initial condition

$$\begin{aligned} t &= 0 \\ c_4(t) &= c_{\text{dalu}} \quad \text{g/m}^3 \\ c_4(0) &= 5.96 \quad \text{g/m}^3 \end{aligned}$$

$$c_4(t + \Delta t) = c_4(t) + \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$= W_4/V + Q_{14}/V_1 c_{14} + Q_{34}/V_3 c_{34} - \lambda_4 c_4$$

$$k_{14} = f(t, c(t))$$

$$k_{24} = f(t + 1/2 \Delta t, c(t) + \frac{1}{2} (W_4/V + Q_{14}/V_1 c_{14} - \lambda_4 c_4))$$

$$+ Q_{34}/V_3 c_{34}$$

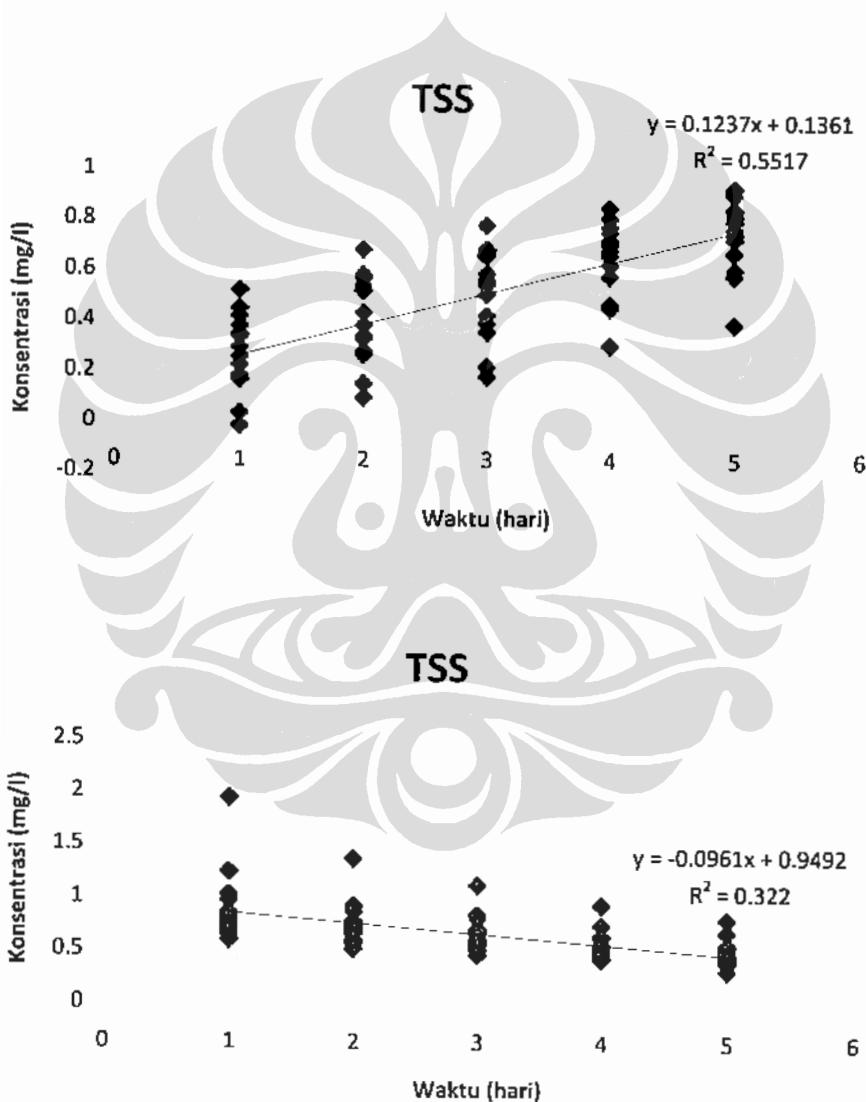
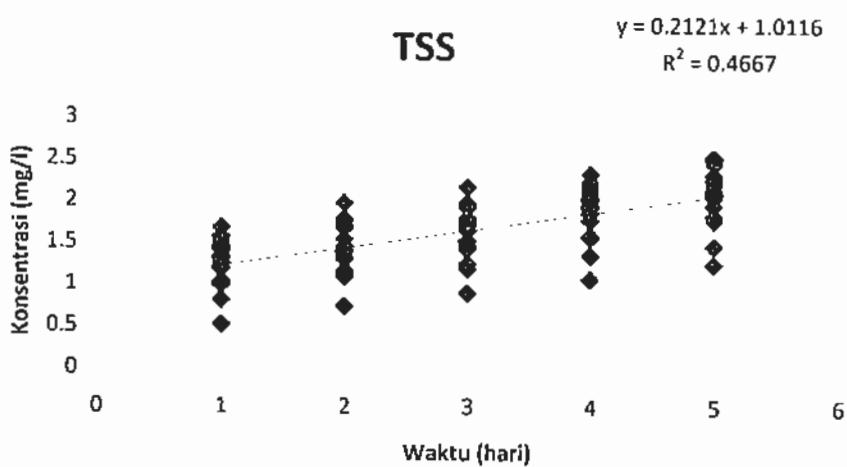
$$Q_{14}/V_1 c$$

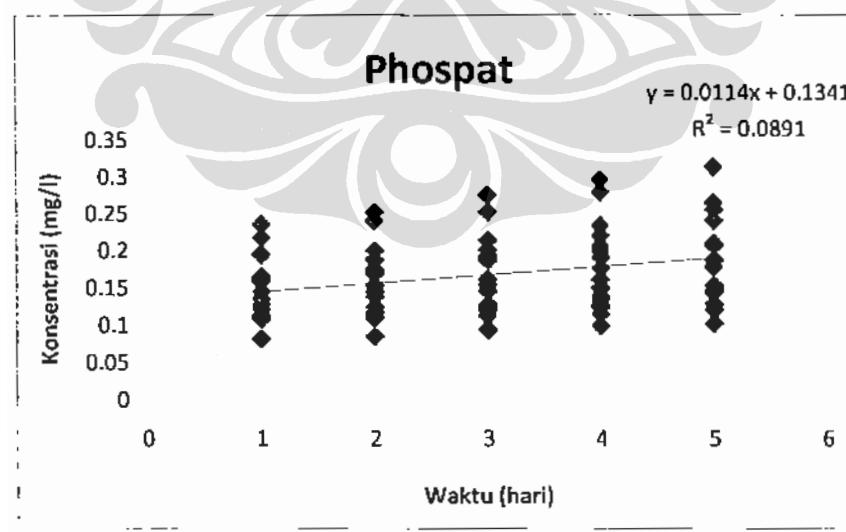
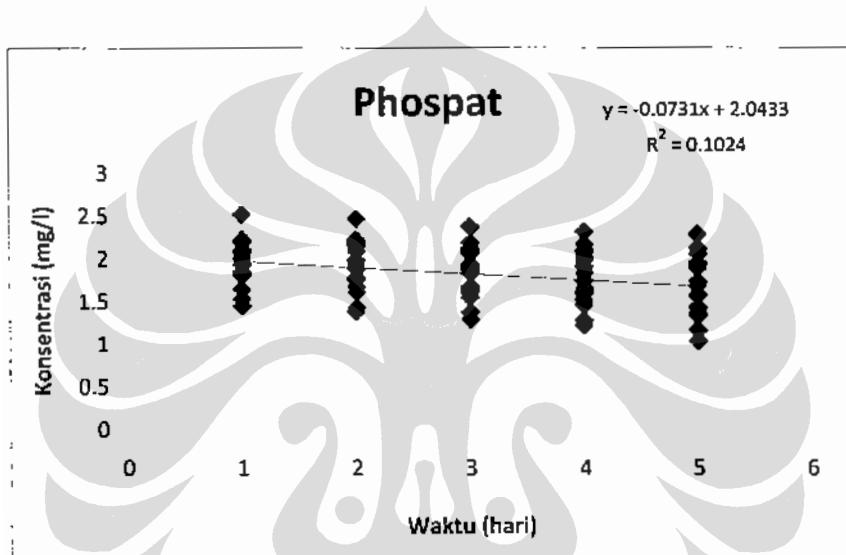
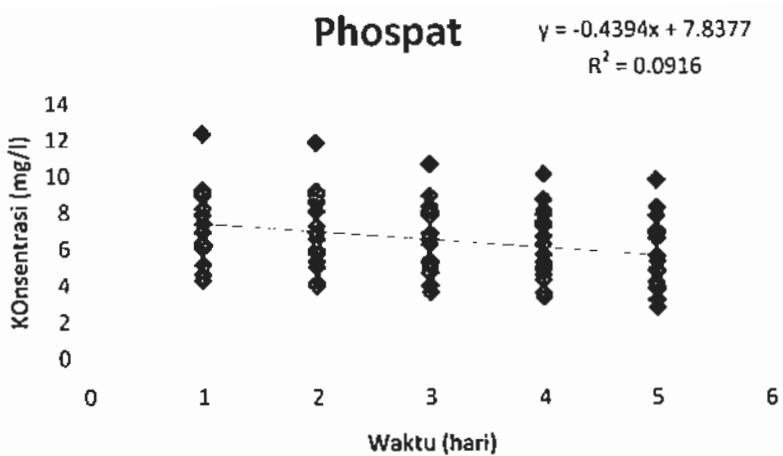
$$k_{34} = f(t + 1/2 \Delta t, c(t) + \frac{1}{2} (W_4/V + Q_{14}/V_1 c_{14} - \lambda_4 c_4))$$

$$+ (t + 1/2 \Delta t k_{24}) - (t + 1/2 \Delta t k_{14})$$

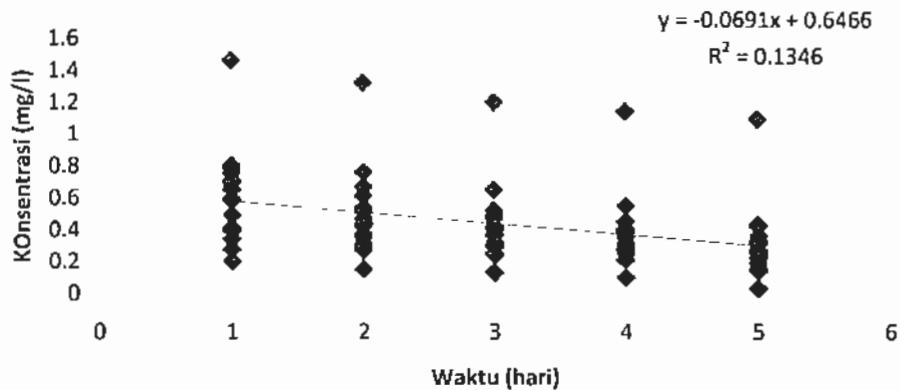
$$k_{43} = f(t + \Delta t, c(t) + \Delta t) = W_4/V + Q_{14}/V_1 c_{14} - \lambda_4 c_4 - (t + \Delta t k_{34})$$

Δt	$c_4(t)$	f	k_{14}	f	k_{24}	f	k_{34}	f	k_{43}	f	k_{44}	$c_4(t + \Delta t)$
0.5												
t = 0	5.96											
0.5	3.83	0.00	5.96	-5.71	0.25	4.53	-3.89	0.25	4.99	-4.22	0.50	3.85
(t + Δt) = 0.5	3.83	0.50	3.83	-4.50	0.75	2.70	-2.94	0.75	3.09	-2.63	1.00	2.51
1.0	2.30	1.00	2.30	-2.71	1.25	1.62	-1.37	1.25	1.96	-1.80	1.50	1.40
(t + Δt) = 1.0	2.30	1.44	1.44	-1.74	1.75	1.00	-0.82	1.75	1.23	-1.15	2.00	-1.31
1.5	1.44	1.50	1.44	-1.74	1.75	1.00	-0.82	1.75	1.23	-1.15	2.00	0.86
(t + Δt) = 1.5	1.44	0.90	0.90	-1.10	2.25	0.62	-0.46	2.25	0.79	-0.71	2.50	-0.78
2.0	0.90	2.00	0.90	-1.10	2.25	0.62	-0.46	2.25	0.79	-0.71	2.50	0.54
(t + Δt) = 2.0	0.90	0.57	0.57	-0.71	2.75	0.40	-0.24	2.75	0.51	-0.44	3.00	-0.46
2.5	0.57	2.50	0.57	-0.71	2.75	0.40	-0.24	2.75	0.51	-0.44	3.00	0.57
(t + Δt) = 2.5	0.57	0.39	0.39	-0.48	3.25	0.27	-0.13	3.25	0.36	-0.29	3.50	0.24
3.0	0.39	3.00	0.39	-0.48	3.25	0.27	-0.13	3.25	0.36	-0.29	3.50	-0.09
(t + Δt) = 3.0	0.39	0.27	0.27	-0.34	3.75	0.19	-0.07	3.75	0.25	-0.19	4.00	0.27
3.5	0.27	3.50	0.27	-0.34	3.75	0.19	-0.07	3.75	0.25	-0.19	4.00	0.18
(t + Δt) = 3.5	0.27	0.19	0.19	-0.24	4.25	0.13	-0.03	4.25	0.19	-0.12	4.50	-0.05
4.0	0.19	4.00	0.19	-0.24	4.25	0.13	-0.03	4.25	0.19	-0.12	4.50	0.19
(t + Δt) = 4.0	0.19	0.15	0.15	-0.18	4.75	0.10	0.00	4.75	0.15	-0.08	5.00	0.13
4.5	0.15	4.50	0.15	-0.18	4.75	0.10	0.00	4.75	0.15	-0.08	5.00	-0.03
(t + Δt) = 4.5	0.15	0.12	0.12	-0.15	5.25	0.08	0.01	5.25	0.12	-0.06	5.50	0.15
5.0	0.12	5.00	0.12	-0.15	5.25	0.08	0.01	5.25	0.12	-0.06	5.50	0.12
(t + Δt) = 5.0	0.12											0.10

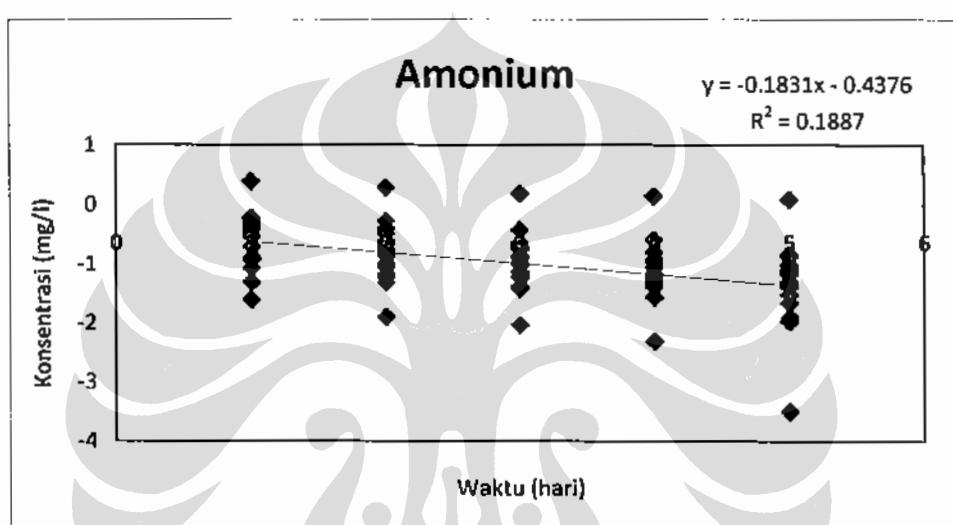




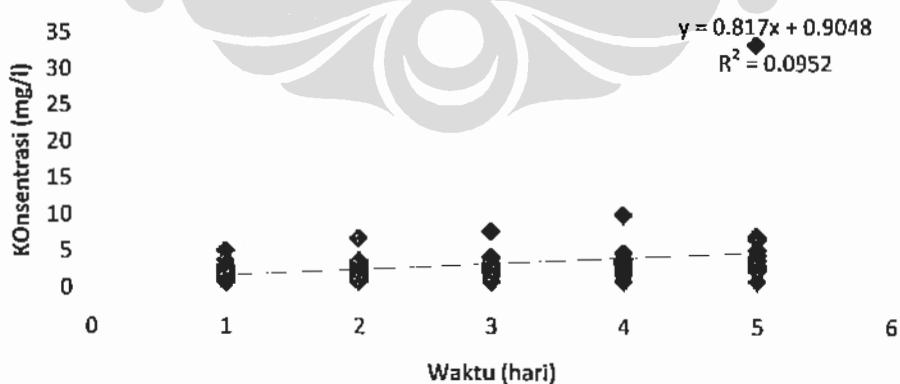
Amonium



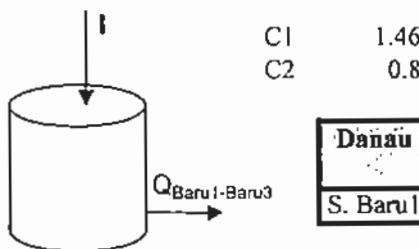
Amonium



Amonium



DO - 1



Danau	$C(t)$ g/m ³	W_f	Q_i m ³ /hari	V m ³	H m	A m ²	vs m/h	k hari ⁻¹	λ_i hari ⁻¹
S. Baru1	2.7	0	12092.29	10000	2	5000	0	0.2	1.411

initial condition

$$t = 0$$

$$c(t) = c_{\text{danan}} \text{ g/m}^3$$

$$c_1(t) = 2.7 \text{ g/m}^3$$

$$c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

$$= -$$

$$\text{Steady } k_{11} = f(t, c(t)) \quad \lambda_1 c_1(t)$$

$$\frac{dc_1}{dt} = -\lambda_1 c_1 \quad k_{21} = f(t + 1/2 \Delta t, c(t) + 1) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{11})$$

$$k_{31} = f(t + 1/2 \Delta t, c(t) + 1) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{21})$$

$$k_{41} = f(t + \Delta t, c(t) + \Delta t k_3) = -\lambda_1 c_1 (t + \Delta t k_{31})$$

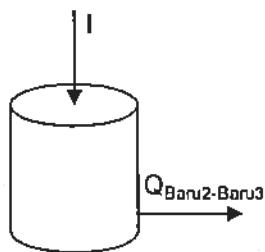
$$\Delta t = 0.5 \text{ hr}$$

$$t = 0$$

$$c_1(t) = 2.7$$

$\Delta t = 0.5$	$c_1(t)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_1(t + \Delta t)$
$t = 0$	2.72									
0.5	0.00	2.72	-3.84	0.25	1.76	-2.48	0.25	2.10	-2.96	0.50
($t + \Delta t$) = 0.5	1.35	0.50	1.35	-1.90	0.75	0.40	-0.56	0.75	1.21	-1.70
1.0	0.50	1.35	-1.90	0.75	0.40	-0.56	0.75	1.21	-1.70	1.00
($t + \Delta t$) = 1.0	0.75	1.00	0.75	-1.06	1.25	0.49	-0.69	1.25	0.58	-0.82
1.5	1.00	0.75	-1.06	1.25	0.49	-0.69	1.25	0.58	-0.82	1.50
($t + \Delta t$) = 1.5	0.37	0.37	-0.53	1.75	0.24	-0.34	1.75	0.29	-0.41	2.00
2.0	1.50	0.37	-0.53	1.75	0.24	-0.34	1.75	0.29	-0.41	0.17
($t + \Delta t$) = 2.0	0.18	2.00	0.18	-0.26	2.25	0.12	-0.17	2.25	0.14	-0.24
2.5	2.00	0.18	-0.26	2.25	0.12	-0.17	2.25	0.14	-0.20	2.50
($t + \Delta t$) = 2.5	0.09	2.50	0.09	-0.13	2.50	0.06	-0.08	2.50	0.07	-0.10
3.0	2.50	0.09	-0.13	2.50	0.06	-0.08	2.50	0.07	-0.10	3.00
($t + \Delta t$) = 3.0	0.04	3.00	0.04	-0.06	3.00	0.04	-0.06	3.00	0.03	-0.04
3.5	3.00	0.04	-0.06	3.00	0.04	-0.06	3.00	0.03	-0.04	3.50
($t + \Delta t$) = 3.5	0.01	3.50	0.01	-0.02	3.50	0.01	-0.02	3.50	0.01	-0.06
4.0	3.50	0.01	-0.02	3.50	0.01	-0.02	3.50	0.01	-0.01	4.00
($t + \Delta t$) = 4.0	0.01	4.00	0.01	-0.01	4.00	0.01	-0.01	4.00	0.01	-0.02
4.5	4.00	0.01	-0.01	4.00	0.01	-0.01	4.00	0.00	-0.01	4.50
($t + \Delta t$) = 4.5	0.00	4.50	0.00	0.00	4.50	0.00	0.00	4.50	0.01	-0.01
5.0	4.50	0.00	0.00	4.50	0.00	0.00	4.50	0.00	0.00	0.00
($t + \Delta t$) = 5.0	0.00	5.00	0.00	0.00	5.00	0.00	0.00	5.00	0.00	0.00

DO - 2



Danau	C(t) g/m ³	W _i m ³ /hari	c _d O _d m ³	V _i m ³	H _i m	A _i m ²	ws m ³ /ha	sk _s hari	T _{si} hari
S.Baru 2	2.62	0	3381.41	20000	2	10000	0.01	0.2	0.371

initial condition

$$t = 0$$

$$c(t) = c_{dansu} \text{ g/m}^3$$

$$c_1(t) = 2.6 \text{ g/m}^3$$

$$c_1(t + \Delta t) = c_1(t) + 1/6 (k_1 + 2k_2 + 2k_3 + k_4) \Delta t$$

Steady

$$\frac{dc_1}{dt} = -\lambda_1 c_1 \quad k_{11} = f(t, c(t)) = -$$

$$k_{21} = f(t+1/2\Delta t, c(t)+1/2\Delta t k_{11}) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{11})$$

$$k_{31} = f(t+1/2\Delta t, c(t)+1/2\Delta t k_{21}) = -\lambda_1 c_1 (t + 1/2 \Delta t k_{21})$$

$$k_{41} = f(t+\Delta t, c(t)+\Delta t k_{31}) = -\lambda_1 c_1 (t + \Delta t k_{31})$$

$$\Delta t = 0.5 \text{ hr}$$

$$t = 0$$

$$c_1(t) = 2.6$$

Δt 0.5	$c_1(t)$	f_{11}	k_{11}	f_{21}	k_{21}	f_{31}	k_{31}	f_{41}	k_{41}	$c_1(t + \Delta t)$				
t = 0	2.62	0.00	-2.62	0.97	0.25	2.86	-1.06	0.25	2.35	-0.87	0.50	2.18	-0.81	2.31
(t + Δt)=0,5	2.31	0.50	-2.31	0.86	0.75	2.74	-1.02	0.75	2.06	-0.76	1.00	1.93	-0.72	2.03
1.0	2.03	1.00	-2.03	0.75	1.25	2.21	-0.82	1.25	1.82	-0.68	1.50	1.69	-0.63	1.79
(t + Δt)= 1,0	2.03	1.00	-2.03	0.75	1.25	2.21	-0.82	1.25	1.82	-0.68	1.50	1.69	-0.63	1.79
1.5	1.79	1.50	-1.79	0.66	1.75	1.95	-0.72	1.75	1.61	-0.60	2.00	1.49	-0.55	1.58
(t + Δt)= 1,5	1.79	1.50	-1.79	0.66	1.75	1.95	-0.72	1.75	1.61	-0.60	2.00	1.49	-0.55	1.58
2.0	1.58	2.00	-1.58	0.58	2.25	1.72	-0.64	2.25	1.42	-0.53	2.50	1.31	-0.49	1.39
(t + Δt)= 2,0	1.58	2.00	-1.58	0.58	2.25	1.72	-0.64	2.25	1.42	-0.53	2.50	1.31	-0.49	1.39
2.5	1.39	2.50	-1.39	0.52	2.50	1.52	-0.56	2.50	1.25	-0.46	3.00	1.39	-0.52	1.22
(t + Δt)= 2,5	1.39	2.50	-1.39	0.52	2.50	1.52	-0.56	2.50	1.25	-0.46	3.00	1.39	-0.52	1.22
3.0	1.22	3.00	-1.22	0.45	3.00	1.22	-0.45	3.00	1.11	-0.41	3.50	1.22	-0.45	1.08
(t + Δt)= 3,0	1.22	3.00	-1.22	0.45	3.00	1.22	-0.45	3.00	1.11	-0.41	3.50	1.22	-0.45	1.08
3.5	1.08	3.50	-1.08	0.40	3.50	1.08	-0.40	3.50	0.98	-0.36	4.00	1.08	-0.40	0.95
(t + Δt)= 3,5	1.08	3.50	-1.08	0.40	3.50	1.08	-0.40	3.50	0.98	-0.36	4.00	1.08	-0.40	0.95
4.0	0.95	4.00	-0.95	0.35	4.00	0.95	-0.35	4.00	0.86	-0.32	4.50	0.95	-0.35	0.84
(t + Δt)= 4,0	0.95	4.00	-0.95	0.35	4.00	0.95	-0.35	4.00	0.86	-0.32	4.50	0.95	-0.35	0.84
4.5	0.84	4.50	-0.84	0.31	4.50	0.84	-0.31	4.50	0.76	-0.28	5.00	0.84	-0.31	0.74
(t + Δt)= 4,5	0.84	4.50	-0.84	0.31	4.50	0.84	-0.31	4.50	0.76	-0.28	5.00	0.84	-0.31	0.74
5.0	0.74	5.00	-0.74	0.27	5.00	0.74	-0.27	5.00	0.67	-0.25	0.00	0.74	-0.27	0.65
(t + Δt)= 5,0	0.74	5.00	-0.74	0.27	5.00	0.74	-0.27	5.00	0.67	-0.25	0.00	0.74	-0.27	0.65